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AN EXACT TEST FOR THE SEQUENTIAL ANALYSIS OF VARIANCE.(U)  
AUG 79 R W MILLER N00014-77-C-0438

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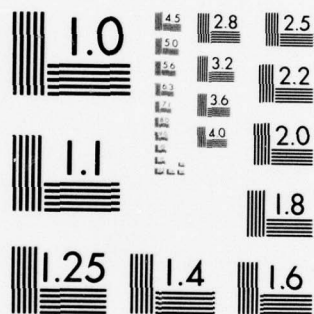
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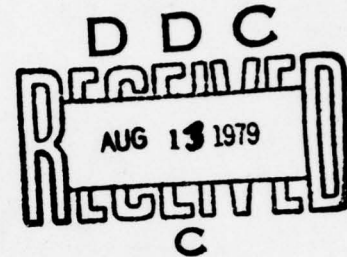


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6 AN EXACT TEST  
FOR THE  
SEQUENTIAL ANALYSIS OF VARIANCE\*

by

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\* This monograph contains the first two chapters  
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## CHAPTER 1

### SEQUENTIAL FIXED EFFECTS

#### ONE-WAY ANALYSIS

#### OF VARIANCE

#### 1.0 INTRODUCTION

This first chapter of the thesis will consider both the fixed and sequential analysis of variance tests. For the fixed sample test the discussions consist of the statistical model, the optimum properties of the test, and the operating characteristic (OC) function. Each of these concepts is important for the consideration of the sequential analysis of variance test.

The sequential analysis of variance test (termed SANOVA) is first discussed from a historical perspective. Further discussions consist of the experimental procedure, the test statistic, and the test statistic decision rule or regions. The OC and average sample number (ASN) functions are also defined. These functions are extremely helpful for designing SANOVA tests.

## 1.1 ONE-WAY FIXED EFFECTS ANALYSIS OF VARIANCE

Analysis of variance, a term introduced into statistics by R.A. Fisher (1918, 1925, 1935), is a statistical technique for analyzing measurements depending upon several kinds of effects operating simultaneously. In general, this technique consists of a body of tests of hypotheses, methods of estimation, etc., using statistics which are linear combinations of sums of squares of linear functions of the observed measurements. The simplest case in which analysis of variance is applied, is the one-way classification, in which the observations depend upon only one factor.

In the one-way layout, a population is stratified into  $m$  subpopulations according to some characteristic or factor and  $n_i$  independent observations are taken from each of  $k$  of the  $m$  subpopulations ( $i = 1, \dots, k$ ). Let the  $j$ th observation from population  $i$  be denoted by  $x_{ij}$  where  $i = 1, \dots, k$  and  $j = 1, \dots, n_i$ . Given that population  $i$  has mean  $\mu + \sigma_i$  and standard deviation  $\sigma_i$ , the statistical model employed in the one-way layout is

$$x_{ij} = \mu + \sigma + e_{ij}, \quad i = 1, \dots, k; \quad j = 1, \dots, n_i$$

with the parameters  $\delta_1, \dots, \delta_k$  satisfying the following condition

$$n_1\delta_1 + \dots + n_k\delta_k = 0$$

The parameter  $\delta_i$  is referred to as the differential effect due to the factor at level  $i$ .

The usual hypothesis of interest is whether  $\delta_1 = \delta_2 = \dots = \delta_k = 0$ , which is equivalent to the hypothesis of the equality of the  $k$  means. The analysis of the effect of the factor depends upon whether  $k < m$  or  $k = m$ . Eisenhardt (1947) was the first to differentiate between the two situations. He used the terms Model I or a fixed effects model as the case where the sample consists of all groups in the population, i.e.,  $k = m$ , and Model II or a random effects model as the case where the interest is in the population from which the sample came, i.e.,  $k < m$ . This thesis will be concerned with only fixed-effects one-way analysis of variance.

The analysis of variance technique requires several assumptions. Specifically, it is assumed that the observations from each of the subpopulations are random variables distributed normally with mean  $\mu + \delta_i$  and standard deviation  $\sigma = \sigma_i$  for all  $i$ . In other words, the model may be expressed as

$$x_{ij} = \mu + \delta_i + e_{ij} \quad i = 1, \dots, k; j = 1, \dots, n$$

$$x_{ij} \sim N(\mu + \delta_i, \sigma)$$

$$e_{ij} \sim N(0, \sigma)$$

and

$$\text{cov}(x_{ij}, x_{lm}) = 0.$$

With this model the hypotheses

$H_0: \mu_1 = \mu_2 = \dots \mu_k$  vs.  $H_1$ : not all means equal  
can be tested with the following statistic

$$F_{\text{cal}} = \frac{\sum_{i=1}^k n_i (\bar{x}_i - \bar{\bar{x}})^2 / (k-1)}{\sum_{i=1}^k \sum_{j=1}^{n_i} (x_{ij} - \bar{x}_i)^2 / (N-k)}$$

where

$$N = \sum_{i=1}^k n_i$$

$$\bar{x}_i = \frac{1}{n_i} \sum_{j=1}^{n_i} x_{ij}$$

$$\bar{\bar{x}} = \frac{1}{N} \sum_{i=1}^k \sum_{j=1}^{n_i} x_{ij}$$

This statistic can be shown (Kempthorne, 1952) to be distributed as a noncentral F variate with  $(k-1, N-k)$  degrees of freedom and noncentrality parameter  $\bar{n}\lambda$ , where

$$\lambda = \frac{\sum_{i=1}^k \delta_i^2 n_i}{\sigma^2} = \frac{\sum_{i=1}^k (\mu_i - \bar{\mu})^2 n_i}{\sigma^2} \quad \text{with} \quad \bar{\mu} = \frac{1}{k} \sum_{i=1}^k \mu_i$$

$$\text{and} \quad \bar{n} = \frac{1}{k} \sum_{j=1}^k n_i$$

The density function of a noncentral F variate with  $v_1, v_2$  degrees of freedom and noncentrality parameter  $\lambda$  is given by:

$$f_{v_1, v_2, \lambda}(x) = \frac{e^{-\frac{1}{2}\lambda} v_1^{\frac{1}{2}v_1} v_2^{\frac{1}{2}v_2} x^{\frac{1}{2}v_1-1}}{B(\frac{1}{2}v_1, \frac{1}{2}v_2) (v_2 + v_1 x)^{\frac{1}{2}(v_1+v_2)}} \sum_{j=0}^{\infty} \left[ \frac{\frac{1}{2}\lambda v_1 x}{v_2 + v_1 x} \right]^j \frac{\Gamma\{\frac{1}{2}(2j + v_1 + v_2)\}}{j! \Gamma(\frac{1}{2}v_2) \Gamma\{\frac{1}{2}(2j + v_1)\}}$$

(Johnson and Kotz, 1970).

(1.1.1)

If the null hypothesis is true, the distribution of  $F_{cal}$  is a central F distribution with  $k-1, N-k$  degrees of freedom. Hence, if the hypothesis is rejected whenever  $F_{cal}$  is greater than the  $100(1-\alpha)\%$  point of this distribution, that is

$$F_{cal} > F_{k-1, N-k, 1-\alpha}^*$$

then the significance level of the test will be  $\alpha$ .

The operating characteristic curve of the test, that is, the probability of accepting  $H_0$  is given by  $\Pr\{F_{cal} \leq F_{k-1, N-k, 1-\alpha}^*\}$ . Since  $F_{cal} \sim F_{k-1, N-k, \bar{n}\xi}$  the OC of the test is characterized by the parameter  $\xi = \bar{n}\lambda$ , i.e.

$$OC(\lambda) = \Pr\{F_{k-1, N-k, \xi} \leq F_{k-1, N-k, 1-\alpha}^*\}$$

Several sets of tables and curves have been prepared from which the OC curve for selected tests can be obtained (Tang 1938, Pearson and Hartley 1951, Lehmer 1944, Fox 1956, Fix 1949). Most of these tables are entered with a different parameter than  $\xi$ . Appendix A contains a

computer program which will calculate the OC curve (as a function of  $\lambda$ ) for any given test.

Originally ANOVA was derived from a distributional point of view, but the F-test has been found to possess several optimum properties. Hsu (1941) showed that the F-test is UMP amongst all tests of size  $\alpha$  whose power depends upon  $\lambda$ , and Wald (1942a) proved that the F-test is best when one is interested uniformly in all alternatives, as expressed by uniform weighting on spheres. As far as ANOVA is concerned it is immaterial whether the value of  $\lambda$  is built up by a number of small contributions or a single large one. Situations where instead the main emphasis is on detection of large deviations should not use ANOVA since the test is no longer optimum in these cases.

## 1.2 SEQUENTIAL ONE-WAY FIXED EFFECTS ANALYSIS OF VARIANCE

Wald (1947) first presented, and systematically studied, the sequential test of a simple hypothesis against a simple alternative. Let  $H_0$  denote the hypothesis that the population density is  $f_0(x)$ , and  $H_1$  the hypothesis that it is  $f_1(x)$ . Constants  $A$  and  $B$  are chosen ( $A > B$ ), and after each observation in a sequence the corresponding likelihood ratio is computed:

$$\Lambda_n = \frac{f_1(x_1) \cdot f_1(x_2) \cdots f_1(x_n)}{f_0(x_1) \cdot f_0(x_2) \cdots f_0(x_n)}$$

The procedure is then as follows: reject  $H_0$  if  $\Lambda'_n \geq A$ , accept  $H_0$  if  $\Lambda_n \leq B$ , and obtain another observation if  $B < \Lambda_n < A$ .  $A$  and  $B$  are chosen so as to make the probabilities of Type-I and Type-II errors equal to  $\alpha$  and  $\beta$  respectively.

Exact values of  $A$  and  $B$  are difficult to obtain.

However, Wald (1947) proved that for small values of  $\alpha$  and  $\beta$

$$A \sim \frac{1 - \beta}{\alpha} \quad \text{and} \quad B \sim \frac{\beta}{1 - \alpha}$$

Since the hypothesis about the equality of  $K$  normal population means with common unknown variance is a composite multiparameter hypothesis with a nuisance parameter, Wald's theory of the sequential probability ratio test cannot be directly applied. To deal with problems such as these, Wald introduced the method of weight functions which, through the notion of a prior distribution for unknown parameters, essentially reduced the basic problem to test hypotheses in one parameter families. A difficulty with this procedure is the choice of the weight function. Cox (1952) devised a unified method under which sequential tests can be obtained for composite hypotheses. The basic idea behind Cox's procedure is to consider a sequence formed by transforming the original observations, the transformation chosen so that the new sequence depends upon a single parameter. Although the distribution of the transformed values  $\{T_n\}$  depends upon only a single para-

meter  $\theta$ , the sequence  $\{T_n\}$  may not be independent. Cox gave conditions under which the following factorization is possible

$$f(T_1, T_2, \dots, T_n) = f(T_n | \theta) f(T_2, \dots, T_n)$$

where  $f(T_2, \dots, T_n)$  does not depend upon  $\theta$ . When this factorization is possible a sequential test can be developed to make a decision about this single parameter  $\theta$ , using only the transformed values  $\{T_n\}$ . The test for discriminating between the hypotheses

$$H_0: \theta = \theta_0 \quad \text{vs.} \quad H_1: \theta = \theta_1$$

can now be constructed by considering the following ratio

$$\Lambda_n = \frac{f(T_n | \theta_1)}{f(T_n | \theta_0)}.$$

Johnson (1953) applied Cox's method to the following one-way fixed effects analysis of variance problem. An experiment is carried out in stages, and at each stage a fixed number  $r_i$ , for  $i = 1, \dots, k$ , of observations are taken from each group. Denote the  $j$ th observation on the  $i$ th group at the  $n$ th stage by  $X_{ijn}$ .

Let

$$SSB_n = n \sum_{i=1}^k r_i (\bar{X}_i - \bar{\bar{X}})^2$$

and

$$SSW_n = \sum_{i=1}^k \sum_{j=1}^{r_i} \sum_{s=1}^n (X_{ijs} - \bar{X}_i)^2$$

with

$$\bar{X}_i = \frac{1}{nr_i} \sum_{j=1}^{r_i} \sum_{s=1}^n X_{ijs}$$

$$\bar{X} = \frac{1}{N} \sum_{i=1}^k \sum_{j=1}^{n_i} \sum_{s=1}^r X_{ijs}$$

$$N = n \sum_{i=1}^k r_i$$

and

$$F_n = \frac{SSB_n / (k-1)}{SSW_n / (N-k)} \quad (1.2.1)$$

The distribution of the sequence  $\{F_n\}$  depends only upon the noncentrality parameter  $\lambda$ . Applying Cox's theorem, a sequential test for discriminating between the hypotheses

$$H_0: \lambda = \lambda_0 \quad \text{vs.} \quad H_1: \lambda = \lambda_1, \quad \lambda_1 > \lambda_0 \quad (1.2.2)$$

for a given  $\alpha$  and  $\beta$  is specified by the decision rule

$$\begin{aligned} \text{Accept } H_0 & \text{ if } \frac{f(F_n | \lambda_1)}{f(F_n | \lambda_0)} < \frac{\beta}{1-\alpha} \\ \text{Reject } H_0 & \text{ if } \frac{f(F_n | \lambda_1)}{f(F_n | \lambda_0)} \geq \frac{1-\beta}{\alpha} \end{aligned}$$

otherwise continue to the next stage. (1.2.3)

An equivalent test was derived by Hoel (1955) using Wald's method of weight functions. The weight function Hoel employed was a generalization of that used for Wald's sequential t-test.

The same sequential test (i.e., the test statistic of (1.2.1) and decision rule (1.2.3) of the hypotheses (1.2.2) has also been by Hall, Wijsman and Ghosh (1965). Their derivation involved applying the principle of invariance. They showed that test statistic of equation (1.2.1) is unchanged by any of the following transformations:

$$(i) \quad X'_{ijn} = CX_{ijn} \quad C > 0$$

$$(ii) \quad X'_{ijn} = X_{ijn} + C$$

(iii) an orthogonal transformation

Also, they were able to prove that the sequential test was UMP for testing the hypotheses  $H_0: \lambda \leq \lambda_0$  vs.  $H_1: \lambda \geq \lambda_1$ , by showing that the density  $f(F_n | \lambda)$  possessed a monotone likelihood ratio (Lehman (1959)).

In addition, they proved that the vector of statistics  $T_n = \{\bar{X}_1, \bar{X}_2, \dots, SSW_n\}$  was a transitive sufficient sequence. This finding is of importance in later chapters of the thesis.

As previously explained, the sequential test is carried out in stages, where at each stage a fixed number  $r_i$ , for  $i = 1, \dots, k$ , of observations are taken from each group. Throughout the remainder of this thesis it will be assumed that at the first stage two observations from each group will be taken (this is so the statistic  $SSB_1$  will not be zero on

the first stage). Each subsequent stage will result in one observation from each group being taken (i.e.,  $r_i = 1$  for all  $i$ ). All future discussions will pertain to this particular testing situation.

As in the fixed sample test, the density of the statistic  $F_{nj} (F_n | \lambda)$ , is that of a noncentral  $F$  variate and is given in equation (1.1.1). Therefore, the decision rule of equation (1.2.3) requires calculating the ratio of two noncentral  $F$  densities. For specified values of  $\alpha$ ,  $\beta$ ,  $\lambda_0$  and  $\lambda_1$  the decision rule can be reexpressed as:

$$\text{accept } H_0 \text{ if } \Lambda_n \leq \frac{\beta}{1-\alpha}$$

$$\text{reject } H_0 \text{ if } \Lambda_n \geq \frac{1-\beta}{\alpha}$$

continue otherwise

where

$$\Lambda = R(F_n) = \frac{e^{-\frac{n}{2}(\lambda_1 - \lambda_0)} M\left[\frac{N-1}{2}, \frac{K-1}{2}, \frac{\lambda_0(K-1)F_n}{2(K(n-1) + (K-1)F_n)}\right]}{M\left[\frac{N-1}{2}, \frac{K-1}{2}, \frac{\lambda_1(K-1)F_n}{2(K(n-1) + (K-1)F_n)}\right]}$$

and  $M(x, y, u)$ , known as the confluent hypergeometric function is defined as

$$M(x, y, u) = \sum_{t=0}^{\infty} \frac{\Gamma(y) \Gamma(x+t)}{\Gamma(x) \Gamma(y+t)} \frac{u^t}{t!}$$

Since the above decision rule is a function of the statistic,  $F_n$ , the equations may be solved to obtain a decision rule in terms of that statistic. That is, two

critical values of the statistic may be found;  $F_n^A$  and  $F_n^R$  such that  $R(F_n^A) = \beta/(1-\alpha)$  and  $R(F_n^R) = (1-\beta)/\alpha$ . When these critical values have been calculated for all stages,  $F_n^A$  and  $F_n^R$ ,  $n = 2, \dots, m_0$ ; the sequential test can then be conducted by comparing the statistic,  $F_n$ , of equation (1.2.1) against these critical values. In summary, at every stage  $n$  the following decision rule is applied:

$$\begin{aligned} \text{accept } H_0 & \text{ if } F_n \leq F_n^A \\ \text{reject } H_0 & \text{ if } F_n \geq F_n^R \\ \text{continue} & \text{ if } F_n^A < F_n < F_n^R \end{aligned}$$

The test is usually performed using the somewhat simpler statistic

$$V_n = \frac{SSB_n}{SSW_n}.$$

The relationship between the two statistics  $F_n$  and  $V_n$  is simply

$$\frac{(N-K)V_n}{(K-1)} = F_n.$$

Conducting the test with the statistic  $V_n$  requires transforming the critical region as well (e.g.,  $V_n^A = (K-1)F_n^A/(N-K)$ ).

Tables of the critical values have been prepared for selected values of  $\alpha$ ,  $\beta$ ,  $K$ ,  $\lambda_0$  and  $\lambda_1$  by Ray (1956) and B.K. Ghosh, et al. (1967). However, these tables are in terms of the test statistic  $G_n = V_n/K$ . Appendix B of this thesis contains a computer program which calculates the critical values of  $V_n$ ;  $V_n^A$  and  $V_n^R$ , for specified values of  $\alpha$ ,  $\beta$ ,  $K$ ,  $\lambda_0$ , and  $\lambda_1$ .

As with all statistical tests, one important property of the test described above is the Operating Characteristic Curve. The OC curve for the above test is strictly a function of  $\lambda$ , and is given by

$$OC(\lambda^*) = \Pr \{ \text{accepting } H_0: \lambda = \lambda_0 \text{ if } \lambda = \lambda^* \}$$

Wald developed an approximation for the OC curve of a sequential probability ratio test of  $f(X, \theta_0)$  against  $f(X, \theta_1)$  provided the equation

$$E_{\theta} \{ [f(X, \theta_1)/f(X, \theta_0)]^h \} = 1$$

has a nonzero solution  $h = h(\theta)$ , and the  $\{X_i\}$  are i.i.d. However, since the above test is conducted on the transformed sequence  $\{V_i\}$  which are not independent, Wald's approximation is not valid. Bhate (1955) developed a conjectural formula, similar to Wald's approximation for the OC curve, when the  $\{X_i\}$  are not independent. Ghosh (1970) suggests that substituting the sequence  $\{V_i\}$  into Bhate's formula may yield a useful approximation to the OC curve. The result of this substitution yields the following approximation to the OC curve.

If  $h_i(\lambda)$  is a nonzero solution of the equation

$$\frac{f_i(V_i | V_1, \dots, V_{i-1}; \lambda_1)}{f_i(V_i | V_1, \dots, V_{i-1}; \lambda_0)}^{h_i} dF(V_i | V_1, \dots, V_{i-1}; \lambda) = 1$$

and  $h_i(\lambda) \approx h(\lambda)$  for all  $i \geq 1$ , that is  $h_i(\lambda)$  varies very little with  $i$  for a given  $\lambda$ , then

$$OC(\lambda) \approx \frac{e^{Ah(\lambda)} - 1}{e^{Ah(\lambda)} - e^{Bh(\lambda)}}.$$

Where

$$A \approx \ln \frac{1-\beta}{\alpha} \qquad B \approx \ln \frac{\beta}{1-\alpha}$$

The crucial point in the use of the conjecture lies in the verification of  $h_i(\theta) \approx h(\theta)$  for various values of  $i$ . Also it must be noted that this approximation is only valid for infinite Wald regions.

The only other alternative, to date, for obtaining the OC curve for this type of test is to employ Monte Carlo techniques.

Also of interest in a sequential test is the Average Sample Number function. For the above test the ASN function will be defined as:

$$ASN(\lambda^*) = \text{Expected number of stages until a decision is reached if } \lambda = \lambda^*.$$

As with the OC curve, Wald's approximation to the ASN, is not valid due to the dependence of the  $\{V_i\}$  sequence. No general formula (exact or approximate) for the ASN for composite hypotheses exists, but Bhate (1955) has developed

a conjectural formula along the same lines as that for the OC curve. Ray (1956) has applied Bhate's conjectural formula to the one-way fixed effect analysis of variance test, and obtained expressions for  $\lambda = \lambda_0, \lambda_1$ . Again, as with the OC curve this procedure is valid only for open Wald regions.

Since the regions are open, it is possible to progress through a large number of stages before a decision is reached. The number of stages will always be finite, however (Johnson, 1953). One way of assuming termination within a reasonable amount of time is to truncate the test. Truncation involves altering the Wald regions so that by some stage  $m_0$  a decision can be made.

This thesis will be concerned with developing procedures to obtain the ASN function and OC curve for a SANOVA test with any given set of truncated regions. The following chapter contains a derivation of SANOVA for the case  $k = 2$  by the Direct Method of Sequential Analysis (Aroian, 1968).

### 1.3 CONCLUSION

This chapter has served to introduce the SANOVA test. This thesis will pertain to obtaining the OC and ASN functions of such a test. Currently, only approximations exist, such as that of Bhate (1959), considered in this chapter. The next chapter will derive the first exact procedure for obtaining the OC and ASN of a  $k=2$  SANOVA test.

## 2.0 INTRODUCTION

The major advantage to performing an analysis of variance sequentially is the possible reduction in sample size over that required for the fixed sample test. Since the sample size is not predetermined in a SANOVA test, the experimenter would like to be assured that the sequential test can offer an equally discriminating test with smaller sample size than the corresponding fixed sample test. As previously discussed, such assurance can be obtained by examining the OC and ASN curves of the sequential test.

In this chapter an exact procedure is developed for obtaining the OC and ASN curves of a SANOVA test. This procedure is the first which yields exact results and is versatile enough so as to be used for tests with general regions. It is hoped that the procedure will be an invaluable tool for designing SANOVA tests.

In a SANOVA test the decision of acceptance can be made at any stage  $i$ ,  $i = 2, \dots, m_0$ . Thus, the probability of accepting the null hypothesis must be calculated as the sum of the probabilities of accepting at each

state,  $P_A^i$ ; i.e.  $OC = \sum_{i=2}^{m_0} P_A^i$ . Of course, these

probabilities will depend upon the state of nature  $\lambda$ .

Unlike the fixed sample test, these probabilities cannot be obtained by simply integrating the distribution of the test statistic. One must remember that in sequential analysis the statistic at stage  $i$  only exists when the statistics at all previous stages have had values within the continuation region, i.e.,  $F_A^j < F_j < F_R^j$ ,  $j = 2, \dots, i-1$ . Thus, the distribution of the test statistic at stage  $i$  is not a true probability distribution since its total probability content is not 1 (rather  $P_C^{i-1}$ ). Were this distribution known it could be integrated to obtain  $P_A^i$ . Unfortunately this distribution cannot be obtained analytically.

However, the procedure developed in this chapter obtains a "truncated" density at stage  $i-1$ . Rather than utilizing the density of the test statistic  $F_i$ , this procedure utilizes the joint density of the sufficient statistics at stage  $i$  (i.e. each of the  $K$  sample means and the pooled estimate of the variance). From this joint density the density of  $F_i$  can be obtained which then can be integrated to yield  $P_A^i$ .

The joint density at stage  $i$  is obtained from the joint density at stage  $i-1$  by applying Aroian's direct method of sequential analysis. This consists of determining the mapping of points at stage  $i-1$  to those at

stage  $i$  (where a point represents a value of the vector of sufficient statistics). This mapping describes how the statistics at stage  $i-1$  are changed by the new observations to yield statistics at stage  $i$ . Thus for any given point,  $A$ , at stage  $i$ , there is a region of points,  $P$ , at stage  $i-1$  which can be mapped into it.

Due to the nature of a sequential test, some points in  $P$  may result in a decision being made at stage  $i-1$ . If so, the point can not be mapped into  $A$ , since the test would terminate at stage  $i-1$ . Thus, for a sequential test the region of points,  $H$ , which can be mapped into  $A$  must include only those points in  $P$  which lie in the continuation region at stage  $i-1$ . Ultimately, this restriction will yield the desired "truncated" density for stage  $i$  (i.e., the total probability content is  $P_C^{i-1}$ ).

As previously mentioned the statistics at stage  $i$  are transformations of the statistics at stage  $i-1$  and the new observations taken at stage  $i$ . Suppose that the required number of sufficient statistics is  $n$ , and that the number of new observations taken at any stage is  $K$  (assuming one observation from each population would imply a test for the equality of  $K$  means). The above transformation would then be a transformation of  $n + k$  random variables (the statistics at stage  $i$  and the  $K$  new

observations) to  $n$  random variables (the statistics at stage  $i$ ). Since the dimensionality of the two sets of random variables is not the same,  $K$  surplus random variables must be introduced. These  $K$  surplus variables will be judiciously selected functions of the statistics at stage  $i-1$  and new observations. This introduction of surplus random variables makes the transformation from an  $n + K$  dimensional space (the statistics at stage  $i-1$  and  $K$  new observations) to an  $n+K$  dimensional space (the statistics at stage  $i$  and  $K$  surplus variables). The joint density of the statistics at stage  $i$  and  $K$  surplus variables can be found by calculus. The procedure is essentially equivalent to transforming variables in multiple integrals.

Finally, the desired density (of the joint distribution of the statistics at stage  $i$ ) is obtained by performing a multiple integration of the joint density of the statistics at stage  $i$  and  $K$  surplus variables. The region of integration will be over all points contained in the set of points  $H$ .

The above discussion has given a brief outline of the "exact" procedure developed in this chapter of the thesis. The following sections describe the procedure in greater detail.

## 2.1 THE DIRECT METHOD OF SEQUENTIAL ANALYSIS

Aroian developed a general theory for obtaining the properties of a sequential test exactly (Aroian, 1968).

To determine the properties (usually only the OC curve) for a fixed sample test one needs to know the distribution of the test statistic for a given sample size  $n$  for different values of the parameter being tested. For example, in the fixed sample analysis of variance test where  $n$  observations are taken from each of  $k$  groups, the test statistic

$$F_{\text{cal}} = \frac{\sum_{i=1}^k (\bar{X}_i - \bar{\bar{X}})^2 / (k-1)}{\sum_{i=1}^k \sum_{j=1}^n (X_{ij} - \bar{X}_i)^2 / (N-k)}$$

is distributed as a noncentral  $F$  variate with  $[k-1, N-k]$  degrees of freedom and noncentrality parameter  $\xi = r\lambda$ . The OC curve for a given value of the parameter,  $\xi$ , is then obtained by integrating this distribution over the acceptance region. For fixed sample ANOVA

$$OC(\xi) = \int_{\text{Acceptance region}} f_{k-1, N-k, \xi}(F_{\text{cal}}) dF_{\text{cal}}$$

where  $f_{v_1, v_2, \xi}(x)$  is the noncentral  $F$  density function.

The direct method recognizes as its primary principle that observations are taken in stages in sequential testing, and that for this reason a way must be found to calculate the distribution of the test statistic  $T_n$ , at stage  $n$ . In most cases  $T_n$  is not independent of  $T_1, T_2, \dots, T_{n-1}$ , so that the marginal distribution of  $T_n$  must be obtained by integrating the joint distribution, i.e.,

$$h_n(T_n) = \int \cdots \int_I h(T_1, T_2, \dots, T_{n-1}) dT_1 dT_2 \cdots dT_{n-1}$$

Since a sequential test is terminated whenever any  $T_m \leq T_m^A$  or  $T_m \geq T_m^R$ ; it is not possible to have a value of  $T_n$  if any  $T_i \leq T_i^A$  or  $T_i \geq T_i^R$   $i=2, \dots, n-1$ . Therefore, the direct method considers only the truncated distribution  $f_n(T_n)$ , where

$$f_n(t) = \Pr\{T_2^A < T_2 < T_2^R, T_3^A < T_3 < T_3^R, \dots, T_{n-1}^A < T_{n-1} < T_{n-1}^R, T_n = t\}.$$

Mathematically  $f_n$  is not a true "density" function since  $\int f_n \neq 1$ , but will still be referred to as a density.

When  $T_n$  is dependent upon  $T_{n-1}$  in the following manner

$$T_n = g_1(T_{n-1}) + g_2(X_{(n)})$$

with  $X_{(n)}$  representing the new observation at stage  $n$ ,  $g_1$  and  $g_2$

arbitrary functions,  $f_n(T_n)$  can be obtained from  $f_n(T_{n-1})$ . Bahadur generalized the dependence by introducing the notion of a transitive sequence of statistics (Bahadur, 1954). A transitive sufficient sequence  $\{T_n\}$  is a sequence such that for every  $n > 1$  the conditional distribution of  $T_{n+1}$ , given the set of observations up to stage  $n$ , is identical to the conditional distribution of  $T_{n+1}$ , given  $T_n$ . So, in general, whenever  $T_n$  is transitive sufficient,  $f_n(T_n)$  can be obtained from  $f_{n-1}(T_{n-1})$ .

Instead of obtaining  $f_n(T_n)$  via integration of a joint distribution, the direct method obtains  $f_n(T_n)$  directly from  $f_{n-1}(T_{n-1})$ , due to the transitivity of  $T_n$ .

At each stage  $n$ , the direct method calculates the probability of accepting  $H_0$ ,  $P_A^n$ , and the probability of rejecting  $H_0$ ,  $P_R^n$ , by integrating  $f_n(T_n)$  over the appropriate regions. In mathematical terms,

$$P_A^n = \int_{T_n \leq T_n} f_n(T_n) dT_n$$

$$P_R^n = \int_{T_n \geq T_n} f_n(T_n) dT_n.$$

These probabilities depend upon the state of nature  $\theta$ , since the distribution of  $T_n$  depends upon the parameter  $\theta$ . So for any given  $\theta$ , the OC and ASN curves may be calculated as:

$$OC(\theta) = \sum_{i=2}^{m_0} P_A^i$$

$$ASN(\theta) = \sum_{i=2}^{m_0} i(P_A^i + P_R^i) = 1 + \sum_{i=1}^m P_C^i$$

where  $m_0$  is the truncation point of the sequential test.

Usually the density  $f_n(T_n)$  cannot be obtained from  $f_{n-1}(T_{n-1})$  analytically, so that the procedure must be performed numerically. In numerical terms  $f_n(T_n)$  represents a "grid" of  $T_n$  values calculated for each  $n$  from a "grid" of  $T_{n-1}$  values.

The direct method has been used in a variety of applications, including tests for the mean of a normal distribution with the standard deviation known (Aroian and Robison, 1969) and unknown (Schmee, 1974), and tests of the standard deviation of a normal distribution with mean known and unknown (Aroian, Gorge, Goss and Robison, 1975).

The following section contains a discussion of the application of the direct method to SANOVA.

## 2.2 APPLICATION OF THE DIRECT METHOD TO SANOVA

SANOVA is based on the statistic

$$V_n = n \sum_{i=1}^k (\bar{X}_{i(n)} - \bar{\bar{X}}_{(n)})^2 / \sum_{i=1}^k \sum_{j=1}^n (X_{ij} - \bar{X}_{i(n)})^2.$$

In order to solve this problem by the direct method a transitive, sufficient sequence  $\{T_n\}$  must be used. The sequence  $\{V_n\}$  is not transitive, so one must use the multidimensional transitive sequence

$$\{T_n\} = \{X_{1(n)}, X_{2(n)}, \dots, X_{k(n)}, S_{(n)}^2\}$$

where

$$X_{i(n)} = \sum_{j=1}^n X_{ij}$$

and

$$S_{(n)}^2 = \sum_{i=1}^k \sum_{j=1}^n \left[ X_{ij} - \frac{X_{i(n)}}{n} \right]^2$$

(Hall, Wijsman, Ghosh, 1965). Similarly, one must now work with the joint distribution  $f_n(X_{1(n)}, X_{2(n)}, \dots, X_{k(n)}, S_{(n)}^2)$ . From this distribution  $P_A^n$  and  $P_R^n$  can be obtained by a  $k+1$  dimensional integration,

$$P^n = \iiint_A \dots \int f_n(X_{1(n)}, X_{2(n)}, \dots, S_{(n)}^2) dX_{1(n)} \dots dS_{(n)}^2$$

where  $A$  is the region in  $k+1$  space such that

$$V_n = \sum_{i=1}^k \left\{ x_{i(n)} - \left[ \frac{x_{1(n)} + \dots + x_{k(n)}}{k} \right] \right\} / s^2_{(n)} \leq V_n^L$$

and

$$P_R^n = \int \dots \int_R f_n(x_{1(n)}, \dots, x_{k(n)}, s^2_{(n)}) dx_{1(n)} \dots ds^2_{(n)}$$

where  $R$  is the region such that  $V_n \geq V_n^u$ .

The problem lies in obtaining  $f_n(T_n)$ . If the first stage at which a decision can be made is  $n_1 \geq 2$ , then since  $x_{1(n_1)}, x_{2(n_1)}, \dots, x_{k(n_1)}$ , and  $s^2_{(n_1)}$  are all independent

$$\begin{aligned} f_{n_1}(T_{n_1}) &= f_{n_1}(x_{1(n_1)}, x_{2(n_1)}, \dots, x_{k(n_1)}, s^2_{(n_1)}) \\ &= \phi \left[ \frac{x_{1(n_1)} - n_1 \mu_1}{\sigma} \right] \cdot \phi \left[ \frac{x_{2(n_1)} - n_1 \mu_2}{\sigma} \right] \dots \phi \left[ \frac{x_{k(n_1)} - n_1 \mu_2}{\sigma} \right] \end{aligned}$$

$$\sigma^2 f_{\chi^2_{k(n_1)-1}}(s^2_{(n_1)})$$

where

$$\phi(x) = \frac{1}{\sqrt{2\pi}} e^{-\frac{1}{2}x^2}$$

is the standard normal density function and

$$f_{\chi^2_v}(x) = \frac{x^{v/2-1} e^{-x/2}}{2^{v/2} \Gamma(v/2)}, \quad x \geq 0$$

is the  $\chi^2$  density function with  $v$  degrees of freedom. Since the power of the SANOVA test depends only upon  $\lambda$ , the density  $f_{n_1}(T_{n_1})$  for given  $\lambda$  can be calculated by assuming  $\mu_1 = \mu_2 = \dots = \mu_k$ ,  $\sigma = 1$  and

$$\mu_k = \sqrt{\frac{\lambda^*}{k-1}}.$$

The probabilities  $P_A^{n_1}$  and  $P_R^{n_1}$  need not be obtained by integration of  $f_{n_1}(T_{n_1})$  since the distribution of  $V_{n_1}$  is known to be related to the noncentral F-distribution;

$$\frac{k(n_1-1)}{(k-1)} V_{n_1} \sim F_{k-1, k(n_1-1)}(n_1 \lambda^*). \quad \text{Therefore}$$

$$P_A^{n_1} = \int_0^{\frac{k(n_1-1)}{(k-1)} V_{n_1}^A} f_{k-1, k(n_1-1), n_1 \lambda^*}(x) dx$$

and

$$P_R^{n_1} = \int_{\frac{k(n_1-1)}{(k-1)} V_{n_1}^R}^{\infty} f_{k-1, k(n_1-1), n_1 \lambda^*}(x) dx$$

These integrals are evaluated by the methods discussed in Appendix A.

To determine  $f_{n_1+1}(T_{n_1+1})$  the direct method will be applied. Since  $\{T_n\}$  is transitive,  $f_{n_1+1}(T_{n_1+1})$  can be obtained directly from  $f_{n_1}(T_{n_1})$ . Suppose the following relationships exist between the elements of  $T_{n_1+1}$  and  $T_{n_1}$ ;

$$\begin{aligned} x_{1(n_1+1)} &= g_{11}(x_{1(n_1)}) + g_{21}(x_{(n_1+1)}) \\ &\vdots \\ x_{k(n_1+1)} &= g_{1k}(x_{k(n_1)}) + g_{2k}(x_{(n_1+1)}) \\ s^2_{(n_1+1)} &= g_{1k+1}(s^2_{(n_1)}) + g_{2k+1}(x_{(n_1+1)}) \end{aligned}$$

where  $g_{1i}$  and  $g_{2i}, i=1, \dots, k+1$  are arbitrary functions, and  $x_{(n_1+1)}$  is the vector of new observations from stage  $n_1+1$ . The statistic  $T_{n_1+1}$  defines a transformation which maps points in the  $2k+1$  dimensional space of  $T_{n_1}, x_{(n_1+1)}$  to the  $k+1$  dimensional space of  $T_{n_1+1}$ . To make the transformation from a  $2k+1$  space to a  $k+1$  space, the following additional variables will be defined

$$\begin{aligned} E_{1(n_1+1)} &= g_{2\ k+2}(x_{(n_1+1)}) \\ &\vdots \\ E_{k(n_1+1)} &= g_{2\ 2k+1}(x_{(n_1+1)}) \end{aligned} \quad : \quad E_{n_1+1}$$

where the functions  $g_{2i}, i=k+2, \dots, 2k+1$  are arbitrary functions. Since the transformation is now  $2k+1$  to  $2k+1$ , the joint distribution of  $X_{1(n_1+1)}, \dots, E_{k(n_1+1)}$  can be obtained. From this distribution the joint marginal distribution of  $X_{1(n_1+1)}, \dots, S^2_{(n_1+1)}$  will be obtained by integrating out  $E_{1(n_1+1)}, \dots, E_{k(n_1+1)}$ . To obtain the joint distribution of  $T_{n_1+1}$  and  $E_{n_1+1}$ , one must first obtain the joint distribution of  $T_{n_1}$  and  $X_{(n_1+1)}$ . Since  $X_{(n_1+1)}$  is independent of  $T_{n_1}$ , the joint distribution is simply the product of the respective densities; i.e.

$$g(X_{1(n_1)}, \dots, S^2_{(n_1)}, X_{(n_1+1)}) = f_{n_1}(X_{1(n_1)}, \dots, S^2_{(n_1)}) \cdot f(X_{(n_1+1)})$$

Then under certain conditions (which for this general discussion will be assumed to be true, but are dependent upon the functions  $g_{1i}$  and  $g_{2i}$ ) the joint distribution of  $T_{n_1+1}$  and  $E_{n_1+1}$  is given by

$$f(T_{n_1+1}, E_{n_1+1}) = g(u_1(T_{n_1}, X_{(n_1+1)}), \dots, u_{2k+1}(T_{n_1}, X_{(n_1+1)})) |J|$$

where  $u_i(T_{n_1}, X_{(n_1+1)}), i=1, \dots, 2k+1$  is the set of inverse transformations and  $|J|$  is the Jacobian for the transformation. As previously mentioned the density of  $f_{n_1}(T_{n_1+1})$  can now be obtained as follows

$$f_{n_1}(T_{n_1+1}) = \iiint_{R^*} \dots \int f(T_{n_1+1}, E_{n_1+1}) dE_{1(n_1+1)} \dots dE_{k(n_1+1)} \cdot$$

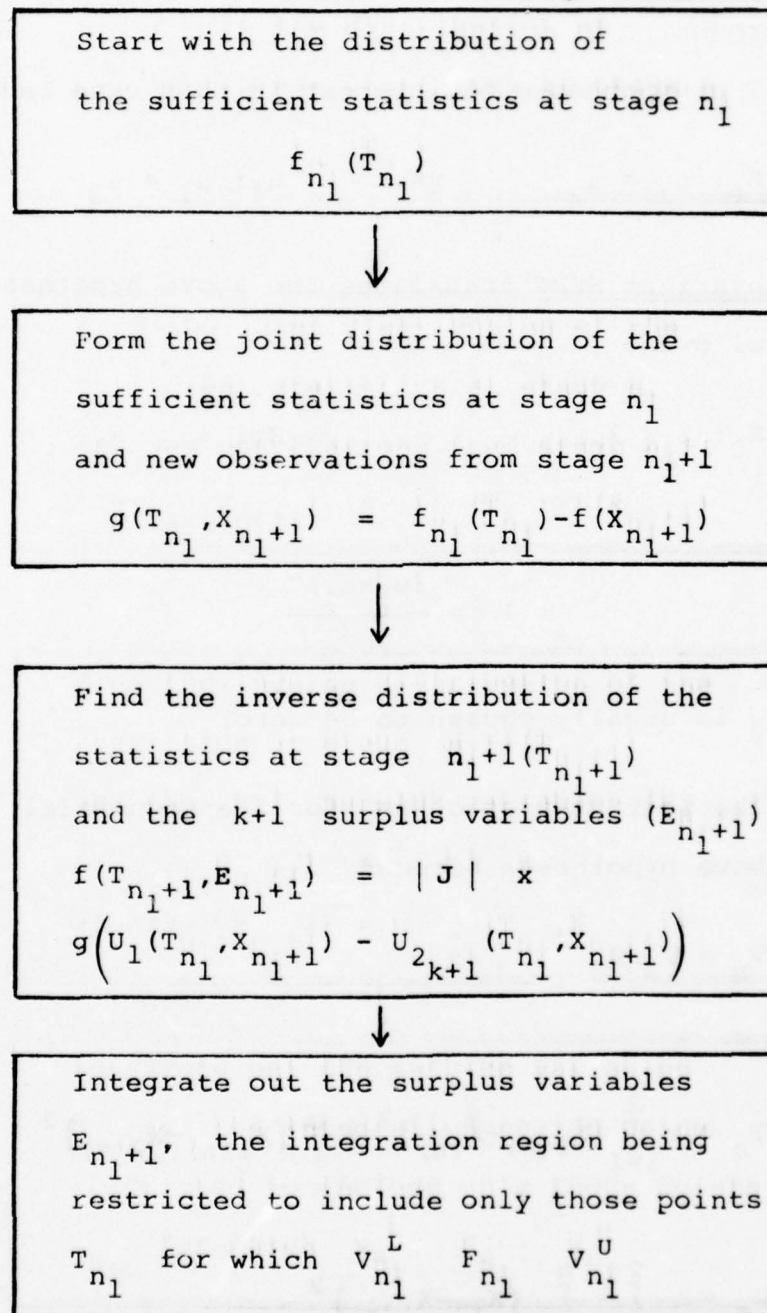
where  $R^*$  represents the integration region in  $k$  space.

The direct method restricts the set of points  $T_{n_1}, X_{(n_1+1)}$  to be mapped into  $T_{n_1+1}$ , to include only those points for which  $V_{n_1}^L < V_{n_1} < V_{n_1}^u$ . This entire procedure can be represented diagrammatically as shown in Figure 1.

The following section contains a complete derivation of the direct method procedure to obtain  $f_n(T_n)$  from  $f_{n-1}(T_{n-1})$  for the special case  $k=2$ . This discussion will specify the functions  $g_{1i}, g_{2i}, u_i$  and derive the integration region  $R^*$ .

FIGURE 1

## The Direct Method Logic



2.3 DERIVATION FOR THE CASE  $k = 2$ 

This section will derive a procedure for obtaining the properties of a SANOVA test for the special case when  $k=2$ , groups.

The hypotheses of interest in this case become:

$$H_0: \mu_1 = \mu_2 \quad \text{vs.} \quad H_1: \mu_1 \neq \mu_2$$

The invariant SPRT translates the above hypotheses into the following

$$H_0: \lambda \leq \lambda_0 \quad H_1: \lambda \geq \lambda_1$$

where

$$\lambda = \frac{(\mu_1 - \mu_2)^2}{2\sigma^2}$$

and  $\lambda_0$  is usually chosen to be zero.

The test statistic used for the sequential test of the above hypotheses becomes

$$V_n = T_n / D_n$$

where

$$T_n = n \sum_{i=1}^2 (\bar{X}_{i(n)} - \bar{\bar{X}}_{(n)})^2 = \frac{n}{2} [x_{1(n)} - x_{2(n)}]^2$$

and

$$D_n = \sum_{i=1}^2 \sum_{j=1}^n (x_{ij} - x_{i(n)})^2.$$

To conduct such a test requires the specification of the following quantities: the null hypothesis,  $\lambda_0$ ; the alternative hypothesis,  $\lambda_1$ ; and a set of regions  $V_A^i, V_R^i, i=1, \dots, m_0$  ( $m_0$  being the test truncation point). The regions may be any type (Wald or modified Wald) that specify: accept  $H_0$  if at any  $i$ ,  $V_i \leq V_A^i$  and reject  $H_0$  if  $V_i \geq V_R^i$ ; otherwise continue sampling. The properties of such a test consist of the OC and ASN curves as functions of  $\lambda$ ; i.e.,  $OC(\lambda)$ , and  $ASN(\lambda)$ ,  $\lambda_0 \leq \lambda \leq \lambda_1$ .

The direct method involves calculating for a given  $\lambda^*$ ,  $f_n(T_n)$  at each stage  $n$ , from which the probabilities  $P_A^n$  and  $P_R^n$  are obtained. Once the quantities  $P_A^i, P_R^i, i=1, \dots, m_0$  have been calculated, the points  $OC(\lambda^*)$  and  $ASN(\lambda^*)$  may be obtained. The following discussion will pertain to obtaining  $P_A^i, P_R^i$  and thus the OC and ASN for a given state of nature  $\lambda = \lambda^*$ . Unfortunately, the statistic  $V_n$  is not transitive, and in order to conserve all the necessary information, one must resort to a transitive sufficient sequence, such as  $\{T_n\} = \{W_n, Q_n, R_n\}$  where

$$\begin{aligned} W_n &= \sum_{j=1}^n x_{1j} \\ Q_n &= \sum_{j=1}^n x_{2j} \\ R_n &= \sum_{i=1}^n \sum_{j=1}^n x_{1j}^2. \end{aligned}$$

The reduction from  $T_n \rightarrow V_n$  is performed at each stage in the following manner

$$V_n = \frac{[W_n - Q_n]^2}{2[nR_n - W_n^2 - Q_n^2]} \quad (2.3.1)$$

The direct method involves calculating, for every stage  $n$ , the joint density  $f_n(W_n, Q_n, R_n)$ .

Suppose the first stage at which a decision can be made is  $n_1 \geq 2$ . The density of  $f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1})$  is obtained as follows:

Let

$$W_{n_1} = n_1 X$$

$$Q_{n_1} = n_1 Y$$

$$R_{n_1} = D_{n_1} + n_1 X^2 + n_1 Y^2$$

where

$$X = \bar{X}_{1(n_1)}$$

$$Y = \bar{X}_{2(n_1)}$$

$$D = \sum_{j=1}^2 \sum_{i=1}^{n_1} (X_{ij} - \bar{X}_{i(n_1)})^2.$$

Since the quantities  $X, Y, D$  are all independent, their joint distribution is given by:

$$f(X, Y, D) = \left[ \chi^2_{2(n_1-1)}(D_{n_1}) \cdot \sigma^2 \right] \phi \left[ \frac{\bar{X}_1(n_1) - \mu_1}{\sigma/\sqrt{n_1}} \right] \cdot \phi \left[ \frac{\bar{X}_2(n_1) - \mu_2}{\sigma/\sqrt{n_1}} \right].$$

Since this procedure is being used to find the properties of the test when  $\lambda = \lambda^*$ , and the test is invariant with respect to  $\lambda$ , we can let  $\mu_1 = 0$ ,  $\sigma = 1$ , and

$$\mu_2 = \sqrt{\lambda^*}.$$

So this density may be expressed as

$$f(X, Y, D_{n_1}) = \chi^2_{2(n_1-1)}(D_{n_1}) \cdot \phi(\sqrt{n_1} \bar{X}_1(n_1)) \cdot \phi(\sqrt{n_1} (X_{2(n_1)} - \sqrt{\lambda^*})).$$

From this density we can determine the joint distribution of  $W_{n_1}, Q_{n_1}, R_{n_1}$ . The set of inverse transformations is given by

$$X = \frac{1}{n_1} W_{n_1}$$

$$Y = \frac{1}{n_1} Q_{n_1}$$

$$D = R_{n_1} - \frac{1}{n_1} W_{n_1}^2 - \frac{1}{n_1} Q_{n_1}^2$$

which has a Jacobian

$$J = \begin{vmatrix} \frac{1}{n_1} & 0 & 0 \\ 0 & \frac{1}{n_1} & 0 \\ -\frac{2}{n_1} W_{n_1} & -\frac{2}{n_1} Q_{n_1} & 1 \end{vmatrix} = \frac{1}{n_1^2}$$

Since this transformation is one-to-one

$$f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1}) = \left(\frac{1}{n_1}\right)^{2(n_1-1)} \left[ R_{n_1} - \frac{1}{n_1} W_{n_1}^2 - \frac{1}{n_1} Q_{n_1}^2 \right] \\ \cdot \phi\left(\sqrt{n_1} \left(\frac{1}{n_1} W_{n_1}\right)\right) \cdot \phi\left(\sqrt{n_1} \left(\frac{1}{n_1} Q_{n_1} - \sqrt{\lambda^*}\right)\right).$$

From this density,  $F_{n_2}(W_{n_2}, Q_{n_2}, R_{n_2})$  will be obtained, where  $n_2 = n_1 + 1$ .

First consider the following functional relationships between the statistics at stage  $n_1$  and stage  $n_2$ :

$$W_{n_2} = W_{n_1} + X_{1n_2} \quad (2.3.2)$$

$$Q_{n_2} = Q_{n_1} + X_{2n_2}$$

$$R_{n_2} = R_{n_1} + X_{1n_2}^2 + X_{2n_2}^2$$

The statistics are changed from stage  $n_1$  to stage  $n_2$  by two new observations,  $X_{1n_2}$  from group 1 and  $X_{2n_2}$  from group 2. Since  $X_{1n_2}$  and  $X_{2n_2}$  are independent of  $W_{n_1}, Q_{n_1}, R_{n_1}$ , the joint distribution of  $X_{1n_2}, X_{2n_2}, W_{n_1}, Q_{n_1}, R_{n_1}$  is simply

$$f_{n_1}^P(W_{n_1}, Q_{n_1}, R_{n_1}, X_{1n_2}, X_{2n_2}) = f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1}) \cdot \phi(X_{1n_2}) \cdot \phi(X_{2n_2} - \sqrt{\lambda^*}).$$

Equations (2.3.2) represent a transformation from the 5 dimensional space of  $W_{n_1}, Q_{n_1}, R_{n_1}, X_{1n_2}, X_{2n_2}$  to the 3 dimensional space of  $W_{n_2}, Q_{n_2}, R_{n_2}$ . A transformation from

5 dimensional space to 5 dimensional space can be achieved by introducing the surplus variables Z and U, yielding the following transformation, T:

$$W_{n_2} = W_{n_1} + X_{1n_2} \quad (2.3.3)$$

$$Q_{n_2} = Q_{n_1} + X_{2n_2}$$

$$R_{n_2} = R_{n_1} + X_{1n_2}^2 + X_{2n_2}^2$$

$$Z = X_{1n_2}$$

$$U = X_{2n_2}$$

The set of inverse transformations,  $T^{-1}$ , is then given by

$$W_{n_1} = W_{n_2} - Z \quad (2.3.4)$$

$$Q_{n_1} = Q_{n_2} - U$$

$$R_{n_1} = R_{n_2} - Z^2 - U^2$$

$$X_{1n_2} = Z$$

$$X_{2n_2} = U$$

This transformation has a Jacobian matrix of the following form

$$J = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & -2Z & -2U & 1 \end{bmatrix} = \begin{bmatrix} I & 0 \\ B_{21} & B_{22} \end{bmatrix}$$

so that

$$|J| = |I| |B_{22} - B_{21}I \ 0| = |I| |B_{22}| = |B_{22}| = 1.$$

Thus, the joint distribution of  $W_{n_2}, Q_{n_2}, R_{n_2}, Z, U$  is given by

$$f_{n_2}(W_{n_2}, Q_{n_2}, R_{n_2}, Z, U) = f_{n_1}^P(W_{n_2} - Z, Q_{n_2} - U, R_{n_2} - Z^2 - U^2, Z, U). \quad (2.3.5)$$

The marginal joint distribution of  $W_{n_2}, Q_{n_2}, R_{n_2}$  is obtained by integrating (2.3.5) with respect to  $U$  and  $Z$  over the appropriate regions. Ordinarily this region consists of all possible values of  $U$  and  $Z$ ,  $-\infty < U < \infty$ ,  $-\infty < Z < \infty$ ; so that the marginal is obtained by

$$f(W_{n_2}, Q_{n_2}, R_{n_2}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f_{n_1}^P(W_{n_2} - Z, Q_{n_2} - U, R_{n_2} - Z^2 - U^2, Z, U) dz du$$

By substitution this integration becomes

$$\begin{aligned}
 & f(w_{n_2}, Q_{n_2}, R_{n_2}) \\
 &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left\{ \frac{1}{n_1^2} x^2_{2(n_1-1)} \left[ R_{n_2} - z^2 - U^2 - \frac{1}{n_1} (w_{n_2} - z)^2 - \frac{1}{n_1} (Q_{n_2} - U)^2 \right] \right. \\
 &\quad \cdot \phi \left[ \sqrt{n_1} \frac{1}{n_1} (w_{n_2} - z) \right] \cdot \phi \left[ \sqrt{n_1} \frac{1}{n_1} (Q_{n_2} - U) \right] - \sqrt{\lambda^*} \\
 &\quad \cdot \phi \left[ (z) \cdot \phi \left( U - \sqrt{\lambda^*} \right) \right] \left. \right\} dz dU
 \end{aligned}$$

Since the chi-squared density function is only defined for positive values, the integration region of U and Z must be chosen so that

$$R_{n_2} - z^2 - U^2 - \frac{1}{n_1} (w_{n_2} - z)^2 - \frac{1}{n_1} (Q_{n_2} - U)^2 \geq 0$$

Therefore, for a given value of U, say  $U^*$ , the range of allowable Z values is given by the following roots.

$$z_{\text{limits}} = \frac{w_{n_2}}{n_1} \pm \sqrt{\frac{n_1}{n_1+1} \left[ R_{n_2} - \frac{w_{n_2}^2}{n_1+1} - \frac{Q_{n_2}^2}{n_1+1} \right] - \left( U^* - \frac{Q_{n_2}}{n_1+1} \right)^2}$$

(2.3.6).

Let the smaller root (the lower limit of Z integration) be denoted  $z_L$  and the larger (the upper limit of Z) by  $z_U$ .

The limits of the U integration are given by:

$$U_{\text{limits}} = \frac{Q_{n_2}^2}{n_1} \pm \sqrt{\frac{n_1}{n_1+1} \left[ R_{n_2} - \frac{W_{n_2}^2}{n_1+1} - \frac{Q_{n_2}^2}{n_1+1} \right]} \quad (2.3.7).$$

Let the smaller root (the lower limit of U integration) be denoted by  $U_L$  and the larger by  $U_U$  (the upper limit of U).

It should be noted that equations (2.3.6) and (2.3.7) have solutions only if  $R_{n_2} - \frac{W_{n_2}^2}{n_1+1} - \frac{Q_{n_2}^2}{n_1+1} \geq 0$ .

If this is not the case, all the above limits can be regarded as zero, so that  $f(W_{n_2}, Q_{n_2}, R_{n_2}) = 0$ .

For all points  $R_{n_2}, W_{n_2}, Q_{n_2}$ , such that  $R_{n_2} - \frac{W_{n_2}^2}{n_1+1} - \frac{Q_{n_2}^2}{n_1+1} \geq 0$ , the joint density is obtained by more

$$f(W_{n_2}, Q_{n_2}, R_{n_2}) = \int_{U_L}^{U_U} \int_{Z_L}^{Z_U} f_{n_1}^P(W_{n_2}-Z, Q_{n_2}-U, R_{n_2}-Z^2-U^2, Z, U) dz dU.$$

(2.3.8)

The result of this integration yields

$$f(W_{n_2}, Q_{n_2}, R_{n_2}) = \frac{1}{(n_1+1)^2} x_{2(n_1)}^2 \left[ R_{n_2} - \frac{1}{(n_1+1)} W_{n_2}^2 - \frac{1}{(n_1+1)} Q_{n_2}^2 \right] \\ \cdot \phi \left( \sqrt{n_1+1} \left( \frac{1}{n_1+1} W_{n_2} \right) \right) \cdot \phi \left( \sqrt{n_1+1} \left( \frac{1}{n_1+1} (Q_{n_2} - \sqrt{\lambda^*}) \right) \right).$$

This is the density which results if the first step at which a decision can be made is  $n_2 = n_1 + 1$ .

However, the direct method restricts the set of points  $(W_{n_1}, Q_{n_1}, R_{n_1}, X_{2n_2}, X_{2n_2})$  to consist of only those points such that  $V_{n_1}^A < V_{n_1} < V_{n_1}^R$ . The limits in equation (2.3.8) do not consider this restriction. The result of applying this restriction involves altering the U and Z limits of integration. The integration region consists of all point U, Z such that:

$$(1) \quad R_{n_2} - z^2 - U^2 - \frac{1}{n_1} (w_{n_2} - z)^2 - \frac{1}{n_1} (Q_{n_2} - U)^2 \geq 0$$

$$(2) \quad V_A^{n_1} < \frac{\left[ w_{n_2} - z - Q_{n_2} + U \right]^2}{2 \left[ n_1 (R_{n_2} - z^2 - U^2) - (w_{n_2} - z)^2 - (Q_{n_2} - U)^2 \right]} < V_R^{n_1}$$

From these constraints integration limits  $U_U, U_L$  and  $z_U, z_L$  can be obtained, such that

$$f_{n_2}(w_{n_2}, Q_{n_2}, R_{n_2}) = \int_{U_L}^{U_U} \int_{z_L}^{z_U} f_{n_1}^P(w_{n_1} - z, Q_{n_2} - U, R_{n_2} - U^2 - z^2, z, U) dz dU.$$

Explicit expressions for these limits can be best derived geometrically.

Let  $V_A = V_A^{n_1}$  and  $V_R = V_R^{n_1}$  such that at stage  $n_1$

$H_0$  is accepted if

$$\frac{\left[ w_{n_1} - Q_{n_1} \right]^2}{2 \left[ n_1 R_{n_1} - w_{n_1}^2 - Q_{n_1}^2 \right]} \leq V_A \quad (2.3.9)$$

and  $H_0$  is rejected if

$$\frac{[W_{n_1} - Q_{n_1}]^2}{2[W_{n_1}^2 - 2W_{n_1}Q_{n_1} + Q_{n_1}^2]} \geq V_R \quad (2.3.10)$$

Solving the above expressions, when the equalities are satisfied, yields the following two surfaces:

$$B_A: R_{n_1} = \frac{(2V_A + 1)W_{n_1}^2 + (2V_A + 1)Q_{n_1}^2 - 2W_{n_1}Q_{n_1}}{2n_1V_A}$$

$$R_{n_1} = C_A W_{n_1}^2 + C_A Q_{n_1}^2 - 2P_A W_{n_1} Q_{n_1}$$

and

$$B_R: R_{n_1} = \frac{(2V_R + 1)W_{n_1}^2 + (2V_R + 1)Q_{n_1}^2 - 2W_{n_1}Q_{n_1}}{2n_1V_R}$$

$$R_{n_1} = C_R W_{n_1}^2 + C_R Q_{n_1}^2 - 2P_R W_{n_1} Q_{n_1}$$

where

$$C_A = \frac{2V_A + 1}{2n_1V_A} \quad \text{and} \quad P_A = \frac{1}{2n_1V_A}$$

with similar expressions for  $C_R$  and  $P_R$ .

The surface  $B_A$  is an elliptic paraboloid since the discriminant,  $D$

$$D = 4P_A^2 - 4C_A^2 = 4(1 - (2V_A + 1)^2)$$

will always be negative for  $V_A > 0$ .

Similarly the surface  $B_R$  is an elliptic paraboloid, usually containing the surface  $B_A$ . All points lying between these two surfaces constitute the continuation region,  $C_{n_1}$ .

Next consider the surface induced by the transformation  $T$ . This surface contains all points in  $T_{n_1}$  space,  $(W_{n_1}, Q_{n_1}, R_{n_1})$ , which can be mapped into some point in  $T_{n_2}$  space

$$(W_{n_2} = a, Q_{n_2} = b, R_{n_2} = c).$$

Since

$$a = W_{n_1} + X_{1n}$$

$$b = Q_{n_1} + X_{2n_1}$$

$$c = R_{n_1} + X_{1n_1}^2 + X_{2n_1}^2;$$

this surface is given by

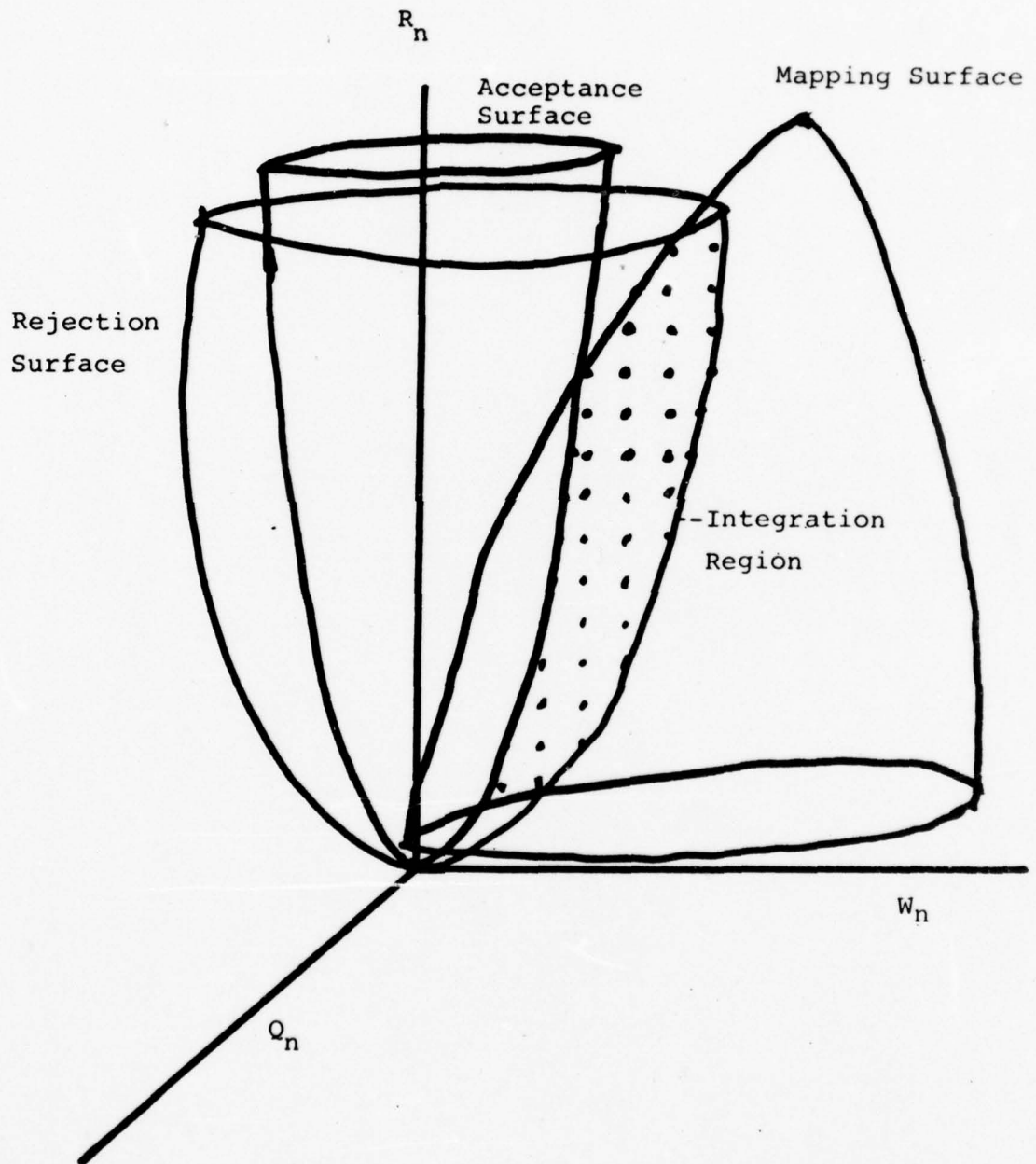
$$c = R_{n_1} + (a - W_{n_1})^2 + (b - Q_{n_1})^2: P$$

The surface  $P$  is an inverted elliptic paraboloid.

The intersection of the continuation region  $C_{n_1}$ , with the mapping surface  $P$ , determines the integration region for equation (2.3.8). This region is shown in Figure 2, and depends upon the point  $(a, b, c)$  as well as the regions  $V_A$  and  $V_R$ .

FIGURE 2

## THE DIRECT METHOD INTEGRATION REGION



If this region is projected onto the  $W_{n_1}, Q_{n_1}$  axes one obtains the set of all  $W_{n_1}, Q_{n_1}$  points for which  $W_{n_1}, Q_{n_1}, R_{n_1}$  are contained on both the continuation surface and the mapping surface. Let this set be denoted by H;

$$H: \{W_{n_1}, Q_{n_1}\} \text{ s.t. } (W_{n_1}, Q_{n_1}, R_{n_1}) \in C_{n_1} \text{ and } P.$$

The integration region for U and Z, for a given point  $W_{n_2} = a, Q_{n_2} = b, R_{n_2} = c$  will consist of all points U, Z such that the doublet  $W = a - Z, Q = b - U$  is contained in the set H. Let this set be denoted by G,

$$G: \{Z, U\} \text{ such that } (a-Z, b-U) \in H.$$

Since there is a one-to-one relationship between the sets G and H, the limits  $U_U, U_L, Z_U, A_L$  can be found by inspection of the set H.

An analytic expression for H can be found by projecting  $B_A \cap P$  and  $B_R \cap P$  onto the  $W_{n_1}, Q_{n_1}$  axes. Since

$$B_R: R_{n_1} = C_R W_{n_1}^2 + C_R Q_{n_1}^2 - 2P_R W_{n_1} Q_{n_1}$$

$$P: R_{n_1} = C - (W_{n_1} - a)^2 - (Q_{n_1} - b)^2$$

the projection of  $B_R \cap P$  onto the  $Q_{n_1}, W_{n_1}$  axes is obtained

by substitution, yielding the curve RE:

$$(C_R+1)W_{n_1}^2 + (C_R+1)Q_{n_1}^2 - 2aW_{n_1} - 2bQ_{n_1} - 2P_R W_{n_1} Q_{n_1} = c - a^2 - b^2$$

Similarly the projection of  $B_A \cap P$  onto the  $Q_{n_1}, W_{n_1}$  axes yields the curve AE:

$$(C_A+1)W_{n_1}^2 + (C_A+1)Q_{n_1}^2 - 2aW_{n_1} - 2bQ_{n_1} - 2P_A W_{n_1} Q_{n_1} = c - a^2 - b^2$$

Both RE and AE are equations of an ellipse; and since the coefficients of  $W_{n_1}^2$  and  $Q_{n_1}^2$  are equal the axes of the ellipse are rotated  $45^\circ$ . Thus, the set H consists of all points which are inside RE and outside AE.

Figure 3 shows the integration region for a particular case. Many such integration regions can arise depending upon the values of  $a, b, c, V_A, V_R$ . However, the region will always be one of the following:\*

I. A point not possible at step  $(n+1)$ .

This consists of all points  $(W_{n+1}, Q_{n+1}, R_{n+1})$  such that  $R_{n+1} - \frac{W_{n+1}^2}{n+1} - \frac{Q_{n+1}^2}{n+1} \leq 0$ , which means

$f(W_{n+1}, Q_{n+1}, R_{n+1}) = 0$ . All future discussions about integration regions will pertain to all points possible at step  $(n+1)$ .

\*For examining the types of integration regions that can arise, the following less cumbersome notation will be used:  $n = n_1$ .

$$\begin{aligned}
RE' : & \left( \frac{n+1}{n} \right) \left[ Q_n - \frac{\sqrt{2}(a+b)n}{2(n+1)} \right]^2 + \left( \frac{V_R + nV_R + 1}{nV_R} \right) \left[ W_n - \frac{\sqrt{2}(a-b)nV_R}{2(V_R + nV_R + 1)} \right]^2 \\
& = \left\{ C - a^2 - b^2 + \frac{n(a+b)^2}{2(n+1)} + \frac{nV_R(a-b)^2}{2(V_R + nV_R + 1)} \right\}
\end{aligned}$$

Note that  $RE$  will only be defined if the following inequality is satisfied

$$C - a^2 - b^2 + \frac{n(a+b)^2}{2(n+1)} + \frac{nV_R(a-b)^2}{2(V_R + nV_R + 1)} > 0$$

or

$$C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R + nV_R + 1)} > 0$$

Whenever this inequality is not satisfied,  $B_R$  never intersects  $P$ . This means that none of the points that can be mapped into  $a, b, c$  lie in the continuation region, resulting in  $f(a, b, c) = 0$ .

$RE'$  is an ellipse with center at

$$Q_n = \frac{\sqrt{2}(a+b)n}{2(n+1)}$$

$$W_n = \frac{\sqrt{2}(a-b)nV_R}{2(V_R + nV_R + 1)}$$

II. Case when only a decision to reject  $H_0$  is possible at stage  $n$ .

When  $V_A$  is a number less than zero it is not possible to accept  $H_0$  at stage  $n$ , since the left hand side of equation (2.3.9) can never be less than zero. Assuming  $V_R < \infty$ , the only decision that can be made at stage  $n$ , is the decision to reject  $H_0$ .

If no decision could be made at stage  $n$ ,  $V_R = \infty$  and  $V_A < 0$ , and as previously discussed, the set  $H$  consists of all  $W_n, Q_n$  inside the following circle,  $RE_\infty$ :

$$(W_n - \frac{na}{n+1})^2 + (Q_n - \frac{nb}{n+1})^2 = \frac{n}{n+1} \left[ c - \frac{a^2}{n+1} - \frac{b^2}{n+1} \right]$$

This is the set of all  $W_n, Q_n$  coordinates of all points  $W_n, Q_n, R_n$  which can be mapped into the point  $(W_{n+1} = a, Q_{n+1} = b, R_{n+1} = c)$  and which satisfy

$$0 < \frac{\left[ W_n - Q_n \right]^2}{2 \left[ nR_n - W_n^2 - Q_n^2 \right]} < \infty .$$

Once the  $W_n, Q_n$  limits of the set  $H$  are obtained, the  $U, Z$  limits are obtained by the following relationship between the sets  $H$  and  $G$

$$U = b - Q_n$$

$$Z = a - W_n .$$

For the case when no decision can be made at stage  $n$ , these limits become those given by equations (2.3.6) and (2.3.7).

Whenever a decision to reject  $H_0$  at stage  $n$  is possible, a set of points,  $W_n^*, Q_n^*, R_n^*$ , in  $W_n, Q_n, R_n$  space exist such that

$$V(W_n^*, Q_n^*, R_n^*) = \frac{[W_n^* - Q_n^*]^2}{2[nR_n^* - W_n^{*2} - Q_n^{*2}]} \geq V_R < \infty.$$

Since these points are not included in the set  $H$ , the set  $H$  now consists of all  $W_n, Q_n$  inside the following ellipse, RE:

$$(C_R + 1)W_n^2 + (C_R + 1)Q_n^2 - 2aW_n - 2bQ_n - 2P_R W_n Q_n = c - a^2 - b^2$$

To compare the two curves  $RE_\infty$  and RE consider the following rotated coordinate system:

$$\begin{aligned} Q_n' &= \frac{\sqrt{2}}{2} [Q_n + W_n] \\ W_n' &= \frac{\sqrt{2}}{2} [-Q_n + W_n] \end{aligned}$$

The curves in this new coordinate system become

$$RE_\infty': \left[ Q_n' - \frac{\sqrt{2}n(a+b)}{2(n+1)} \right]^2 + \left[ W_n' - \frac{\sqrt{2}n(a-b)}{2(n+1)} \right]^2 = \frac{n}{n+1} \left\{ C - \frac{a^2}{n+1} - \frac{b^2}{n+1} \right\}$$

and

$$RE': \left( \frac{n+1}{n} \right) \left[ Q_n' - \frac{2(a+b)n}{2(n+1)} \right]^2 + \left( \frac{V_R + nV_R + 1}{nV_R} \right) \left[ W_n' - \frac{2(a-b)nV_R}{2(V_R + nV_R + 2)} \right]^2$$

$$= \left\{ C - a^2 - b^2 + \frac{n(a+b)^2}{2(n+1)} + \frac{nV_R(a-b)^2}{2(V_R + nV_R + 1)} \right\}$$

Note that RE will only be defined if the following inequality is satisfied

$$C - a^2 - b^2 + \frac{n(a+b)^2}{2(n+1)} + \frac{nV_R(a-b)^2}{2(V_R + nV_R + 1)} > 0$$

or

$$C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R + nV_R + 1)} > 0$$

Whenever this inequality is not satisfied,  $B_R$  never intersects P. This means that none of the points that can be mapped into  $a, b, c$  lie in the continuation region, resulting in  $f(a, b, c) = 0$ .

$RE'$  is an ellipse with center at

$$Q_n' = \frac{\sqrt{2}(a+b)n}{2(n+1)}$$

$$W_n' = \frac{\sqrt{2}(a-b)nV_R}{2(V_R + nV_R + 1)}$$

and minor axis along the  $W_n'$  axis. The circle  $RE_\infty'$  contains the ellipse  $RE''$ . This can be seen by substituting the ellipse end points into the equation of the circle. Consider first the end points given by

$$W_n' = \frac{\sqrt{2}(a-b)nV_R}{2(V_R + nV_R + 1)}$$

$$Q_n' = \frac{\sqrt{2}(a+b)n}{n+1} \pm \sqrt{\frac{n}{n+1} C \left\{ -\frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R + nV_R + 1)} \right\}}$$

Substituting these points into  $RE_\infty'$  yields

$$\begin{aligned} & \left[ \frac{n}{n+1} \left\{ C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R + nV_R + 1)} \right\} \right] + \frac{n^2(a-b)^2}{2(n+1)^2(V_R + nV_R + 1)^2} \\ &= \frac{n}{n+1} \left\{ C - \frac{a^2}{n+1} - \frac{b^2}{n+1} \right\} \end{aligned}$$

which simplifies to

$$\frac{n^2(a-b)^2}{2(n+1)^2(V_R + nV_R + 1)} \left[ \frac{1}{(V_R + nV_R + 1)} - 1 \right]$$

Since this quantity will always be less than or equal to zero, this set of end points will be contained in  $RE_\infty'$ .

Next consider the set of end points given by

$$W_n = \frac{\sqrt{2}(a-b)nV_R}{2(V_R+nV_R+1)} \pm \sqrt{\frac{nV_R}{(V_R+nV_R+1)} \left\{ C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R+nV_R+1)} \right\}}$$

$$Q_n = \frac{\sqrt{2}(a+b)n}{2(n+1)}$$

Substituting this into  $RE_\infty'$  yields the following expression

$$\left\{ -G - \frac{H(a-b)^2}{2} \pm \sqrt{2}(a-b)\sqrt{HG} \right\} \left[ \frac{n}{(n+1)(V_R+nV_R+1)} \right]$$

where

$$H = \frac{nV_R}{V_R+nV_R+1}$$

and

$$G = C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 H}{2}$$

The above expression may be rearranged to yield

$$\left[ \sqrt{G} \pm (a-b)\sqrt{H} \frac{\sqrt{2}}{2} \right]^2 \left[ \frac{-n}{(n+1)(V_R+nV_R+1)} \right]$$

Since this quantity will always be zero or negative, this set of end points will also be contained in  $RE_\infty'$ .

Since a decision to reject  $H_0$  can be made at stage  $n$ , the integration region is reduced to the set of all points contained in ellipse  $RE$ , as shown in Figure 3. To determine the  $U$  integration limits on the integral (2.3.8) first requires finding the  $Q_n$  limits of  $RE$ .

Letting  $Q_{n_U}$  be the maximum value of  $Q_n$  and  $Q_{n_L}$  the minimum value of  $Q_n$  on this ellipse, the integration limits for  $U$  are given by

$$\begin{aligned} U_L &= b - Q_{n_U} \\ U_U &= b - Q_{n_L} . \end{aligned}$$

(2.3.11)

Explicit expressions for  $Q_{n_U}$  and  $Q_{n_L}$  for given  $a, b, c, V_R$  may be obtained by noting that at both points

$$\frac{dW_n}{dQ_n} = \infty .$$

Therefore an expression for  $\frac{dW_n}{dQ_n}$  must be found and examined to see at what points it approaches infinity.

The derivative  $\frac{dW_n}{dQ_n}$  is given by

$$\frac{dW_n}{dQ_n} = \frac{P_R}{C_R+1} + \frac{\frac{1}{2} \left[ \frac{2(a+P_R Q_n)}{(C_R+1)^2} + \frac{2b-2(C+1)Q_n}{(C_R+1)} \right]}{\left[ \frac{(a+P_R Q_n)^2}{(C_R+1)^2} - \left( \frac{a^2+b^2-C-2bQ_n+(C_R+1)Q_n^2}{(C_R+1)} \right) \right]^{\frac{1}{2}}}$$

In order for this derivative to approach infinity the denominator must be equal to zero. Equating the numerator to zero yields,

$$\left[ \frac{(a+P_R Q_n)^2}{(C_R+1)^2} - \left( \frac{a^2+b^2-C-2bQ_n+(C_R+1)Q_n^2}{(C_R+1)} \right) \right]^{\frac{1}{2}} = 0$$

and solving for  $Q_n$  yields

$$Q_n = \frac{b(C+1)+aP_R}{(C_R+1)^2-P_R^2} + \sqrt{\left[ \frac{b(C+1)+aP_R}{P_R^2-C_R+1} \right]^2 - \left[ \frac{a^2-(C+1)(a^2+b^2-c)}{P_R^2-(C+1)^2} \right]} \quad (2.3.12)$$

The larger root will be  $Q_{n_U}$  and the smaller will be  $Q_{n_L}$ .

The limits  $W_{n_L}$  and  $W_{n_U}$  depend upon the value of  $Q_n$ . For a given value  $Q' = b - U$ ;  $Q_{n_L} \leq Q' \leq Q_{n_U}$  the limits for  $W_n$  can be found by solving the equation of the ellipse RE, yielding

$$W_n = \frac{(a + P_R Q')}{(C_R + 1)} \pm \sqrt{\frac{[(a + P_R Q')^2 - \frac{a^2 + b^2 - c - 2bQ' + (C_R + 1)Q'^2}{C_R + 1}]}{(C_R + 1)^2}} \quad (2.3.13)$$

Letting  $W_{n_L}$  be the smaller root and  $W_{n_U}$  the larger, the  $Z$  integration limits become

$$Z_U = a - W_{n_L} \quad (2.3.14)$$

$$Z_L = a - W_{n_U}.$$

In summary, whenever  $V_A < 0$  and  $V_R < \infty$  the integration limits  $U_L, U_U$  for a point  $W_n = a, Q_n = b, R_n = c$ , can be obtained from equation (2.3.11), where  $Q_{n_L}$  and  $Q_{n_U}$  are values obtained from equation (2.3.12). The limits  $Z_L$  and  $Z_U$  depend upon the value of  $U$ ; for a given value  $U'$  the limits are obtained from equation (2.3.14) where  $W_{n_L}$  and  $W_{n_U}$  are obtained from equation (2.3.13).

III. Case when only a decision to accept  $H_0$  is possible at stage  $n$ .

When  $V_R = \infty$  a decision to reject  $H_0$  cannot be made at stage  $n$ . If  $V_R = \infty$ ,

$$C_R = \frac{2V_R + 1}{2nV_R} = \frac{1}{n}$$

and

$$P_R = \frac{1}{2nV_R} = 0$$

so the ellipse  $B_R$  becomes:

$$R_n = \left(1 + \frac{1}{n}\right) W_n^2 + \left(1 + \frac{1}{n}\right) Q_n^2.$$

The projection of  $B_R \cap P$  onto the  $W_n, Q_n$  axes yields, RE:

$$\left(1 + \frac{1}{n}\right) W_n^2 + \left(1 + \frac{1}{n}\right) Q_n^2 - 2aW_n - 2bQ_n = c - a^2 - b^2,$$

which is now the equation of a circle with center at

$$W_n = \frac{a}{1 + \frac{1}{n}} = \frac{na}{n+1}$$

$$Q_n = \frac{b}{1 + \frac{1}{n}} = \frac{nb}{n+1}$$

and

$$\text{radius} = \sqrt{\frac{nc}{n+1} - \frac{na^2}{(n+1)^2} - \frac{nb^2}{(n+1)^2}}.$$

The equation for AE is still given by:

$$(C_A+1) W_n^2 + (C_A+1) Q_n^2 - 2aW_n - 2bQ_n - 2P_A W_n Q_n = c - a^2 - b^2$$

which is the equation of an ellipse with center at

$$Q_n = \frac{b(C_A+1)}{(C_A-P_A+1)(C_A+P_A+1)}$$

$$W_n = \frac{a(C_A+1)}{(C_A-P_A+1)(C_A+P_A+1)}$$

In this situation the set H consists of all  $W_n, Q_n$  which lie outside the curve AE yet inside RE.

By equating the left hand sides of RE and AE one obtains the following equation:

$$W_n^2 + Q_n^2 - 2W_n Q_n = 0$$

or

$$(W_n - Q_n)^2 = 0$$

This means that the two curves, AE and RE, will intersect only at the points where  $W_n = Q_n$ .  
Substituting this into RE yields

$$2\left(1 + \frac{1}{n}\right)Q_n^2 - 2(a+b)Q_n = c - a^2 - b^2$$

Solving for  $Q_n$  yields

$$\frac{(a+b) \pm \sqrt{(a+b)^2 - 2(1+\frac{1}{n})(a^2+b^2-c)}}{2(1+\frac{1}{n})}$$

At this point, it must be noted that there are a variety of ways in which the curves AE and RE can intersect. The above derivations have shown that when only a decision to accept  $H_0$  is possible at stage  $n$ , the curves will intersect along the line  $W_n = Q_n$ . The specific points of intersection are given by the previous equation. This equation may yield zero, one, or two distinct intersection points, depending upon the value of the discriminant; i.e.

$$(a+b)^2 - 2(1+\frac{1}{n})(a^2+b^2-c).$$

This equation reveals that the number of intersection points depends solely upon the point  $a, b, c$ .

Each of the intersection possibilities (i.e., zero, one, or two intersection points) indicates a different geometric relationship between AE and RE; which means that each results in a different  $U, Z$  integration region. Thus, to obtain the entire density (i.e. the density at all points) requires deriving the integration regions of all the possible intersection situations. Each of these possibilities will now be considered.

Whenever the following condition occurs

$$(a+b)^2 - 2\left(1+\frac{1}{n}\right)(a^2+b^2-c) \leq 0$$

the two curves RE and AE will never intersect.

This indicates one of the following geometric relationships must exist:

- (1) the curve RE contains AE
- (2) the curve AE contains RE
- (3) the curves AE and RE contain no points in common, given they don't intersect.

Situation (3) will occur only if neither curve contains the other's center. This is equivalent to satisfying the following inequalities (if they don't intersect):

$$\left[ \frac{n(a-b)^2}{2V_A(n+1)^2} \right] - \left[ c - \frac{a^2}{n+1} - \frac{b^2}{n+1} \right] > 0 \quad (2.3.15)$$

and

$$\left( \frac{(a^2+b^2)n}{n+1} \right) \left[ \frac{1}{4[(n+1)V_A+1]^2} - 1 \right] - \left( c - a^2 - b^2 \right) > 0 \quad (2.3.16)$$

When these inequalities are satisfied the set H consists of all  $W_n, Q_n$  contained inside RE. This is shown in Figure 4. The  $Q_n$  end points of this circle are given by:

$$\frac{nb}{n+1} \pm \sqrt{\frac{nc}{n+1} - \frac{na^2}{(n+1)^2} - \frac{nb^2}{(n+1)^2}} \quad (2.3.17)$$

Let the smaller root be denoted by  $Q_{n_L}$  and the larger by  $Q_{n_U}$ ; then the U integration limits are given by

$$U_U = b - Q_{n_L} \quad (2.3.18)$$

$$U_L = b - Q_{n_U}$$

For a given value of U, say  $U^*$  the Z integration limits are given by

$$Z_U = a - W_{n_L} \quad (2.3.19)$$

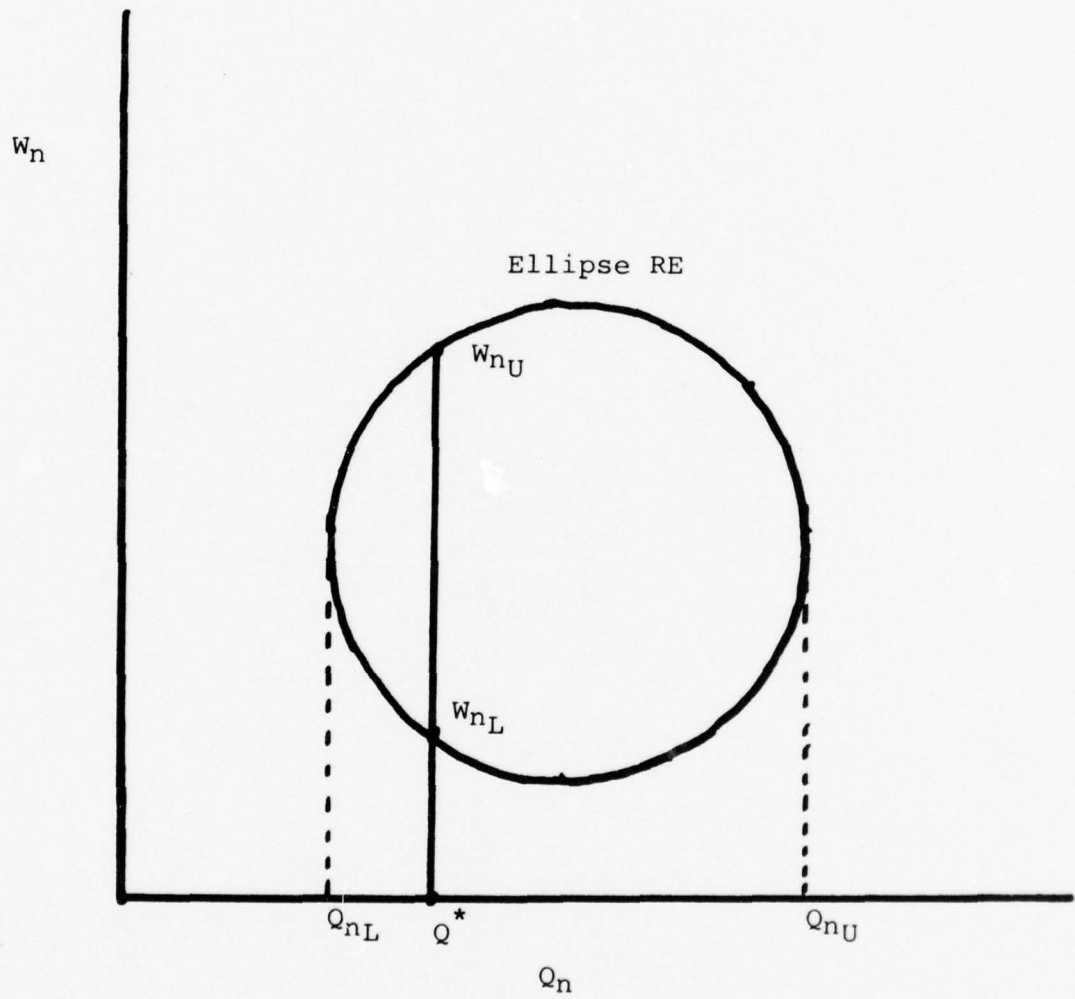
$$Z_L = a - W_{n_U}$$

Where  $W_{n_L}$  and  $W_{n_U}$  are the smallest and largest values of

$$\frac{na}{n+1} \pm \sqrt{\frac{n}{n+1}c - \frac{b^2}{n+1} - \frac{na^2}{(n+1)^2} - \frac{2bU^*}{n+1} - U^{*2}} \quad (2.3.20)$$

FIGURE 4

Integration Region  
When Neither a Decision to Accept  
or Reject Can Be Made



These limits are identical to those in equations (2.3.6) and (2.3.8); which is to be expected, since situation (1) is a case where all points  $W_n$ ,  $Q_n$ ,  $R_n$ , which can be mapped into the point  $a$ ,  $b$ ,  $c$ , lie in the continuation region  $C_n$ .

Situation (2) will occur whenever the center of the circle  $RE$  is a point inside the ellipse  $AE$ ; and the following point on  $RE$

$$W_{n_c} = \sqrt{\frac{na}{n+a} + \frac{nc}{n+1} - \frac{na^2}{(n+1)^2} - \frac{nb^2}{(n+1)^2}}$$

$$Q_{n_c} = \frac{nb}{n+1}, \quad (2.3.21)$$

is inside the ellipse  $AE$ . This is equivalent to satisfying the following inequalities:

$$\frac{n(a-b)^2}{2V_n(n+1)^2} - \left[ c - \frac{a^2}{n+1} - \frac{b^2}{n+1} \right] < 0 \quad (2.3.22)$$

and

$$\frac{1}{2nV_A} \left[ \frac{\sqrt{n}}{(n+1)} (a-b) + \frac{1}{\sqrt{n}} \sqrt{\frac{nc}{n+1} - \frac{na^2}{(n+1)^2} - \frac{nb^2}{(n+1)^2}} \right]^2 < 0 \quad (2.3.23)$$

Since the second inequality can never be satisfied, situation (2) will never occur.

Situation (1) will occur whenever the center of the ellipse AE is a point inside RE; and the point  $W_{n_c}, Q_{n_c}$  defined in equation (2.3.21) is outside AE. The second constraint amounts to requiring the left hand side of equation (2.3.23) to be greater than zero; which will always be true. The first is equivalent to satisfying the following inequality:

$$\frac{n(a-b)^2}{2V_A(n+1)^2} - \left[ c - \frac{a^2}{n+1} - \frac{b^2}{n+1} \right] < 0 \quad (2.3.24)$$

Whenever this is true, the region of interest must be broken up into 4 subregions as shown in Figure 5. Thus the integral in equation (2.3.8) will be broken up into 4 separate integrals, so that

$$f_{n+1}(a,b,c) = \sum_{i=1}^4 \left\{ \int_{U_{Li}}^{U_{Ui}} \int_{Z_{Li}}^{Z_{Ui}} f_n^p(a-z, b-u, c-z^2-u^2) dz du \right\} \quad (2.3.25)$$

The limits  $U_{U_i}, U_{L_i}, Z_{U_i}, Z_{L_i}$  will now be obtained for each region.

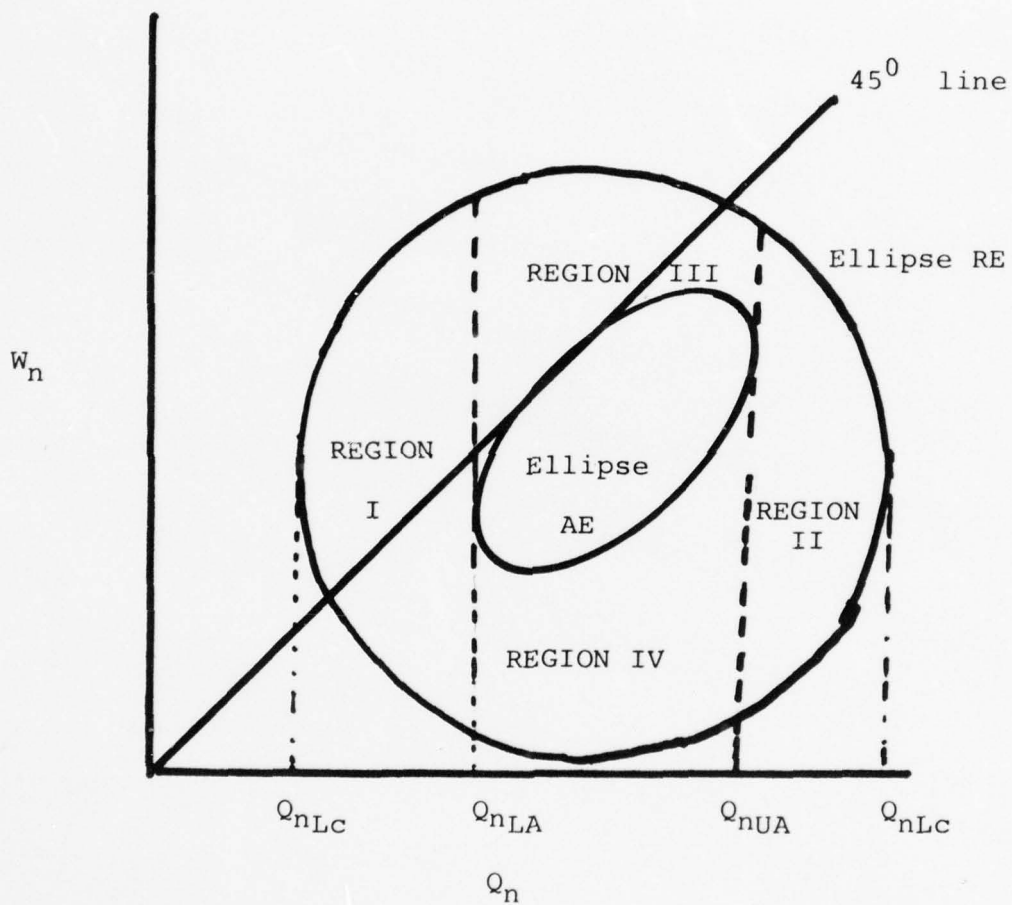
For each region a range of  $Q_n$  can be found;

$Q_{n_{Li}} \leq Q_n \leq Q_{n_{Ui}}$  from which the U integration limits

are obtained as:  $U_{L_i} = b - Q_{n_{Ui}}$  and  $U_{U_i} = b - Q_{n_{Li}}$ .

FIGURE 5

An Integration Region  
Consisting of Four Pieces



The range of  $Q_n$  for each of the subregions is as follows:

$$\text{Region I: } Q_{n_{L1}} = Q_{n_{LC}} \leq Q_n \leq Q_{n_{LE}} = Q_{n_{U1}}$$

$$\text{Region II: } Q_{n_{L2}} = Q_{n_{UA}} \leq Q_n \leq Q_{n_{UC}} = Q_{n_{U2}}$$

$$\text{Region III: } Q_{n_{L3}} = Q_{n_{LA}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U3}}$$

$$\text{Region IV: } Q_{n_{L4}} = Q_{n_{LA}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U4}}$$

Where  $Q_{n_{LC}}$  and  $Q_{n_{UC}}$  are the two  $Q_n$  end points of the circle RE, or the smallest and largest values of equation (2.3.17).

$Q_{n_{LA}}$  and  $Q_{n_{UA}}$  represent the  $Q_n$  end points of the ellipse AE. These are obtained by the same methods employed for Case II (equation (2.3.12)); yielding  $Q_{n_{LA}}$  and  $Q_{n_{UA}}$  as the smallest and largest values of

$$\frac{b(c_A+1)+aP_A}{(c_A+1)^2-P_A^2} \pm \sqrt{\left[ \frac{b(c_A+1)+aP_A}{P_A^2-(c_A+1)^2} \right]^2 - \left[ \frac{a^2-(c_A+1)(a^2+b^2-c)}{P_A^2-(c_A+1)^2} \right]} \quad (2.3.27)$$

Similarly, for each region a range of  $W_n$  values can be defined:  $W_{n_{Li}} \leq W_n \leq W_{n_{Ui}}$  from which the  $z$  limits are obtained as:  $z_{Li} = a - W_{n_{Ui}}$  and  $z_{Ui} = a - W_{n_{Li}}$ .

The range of  $W_n$  for each of the subregions is as follows:

$$\text{Region I: } W_{n_{L1}} = W_{n_{LC}} \leq W_n \leq W_{n_{UC}} = W_{n_{U1}}$$

$$\text{Region II: } W_{n_{L2}} = W_{n_{LC}} \leq W_n \leq W_{n_{UC}} = W_{n_{U2}}$$

$$\text{Region III: } W_{n_{L3}} = W_{n_{UA}} \leq W_n \leq W_{n_{UC}} = W_{n_{U3}}$$

$$\text{Region IV: } W_{n_{L4}} = W_{n_{LC}} \leq W_n \leq W_{n_{LA}} = W_{n_{U4}}$$

Where  $W_{n_{LC}}$  and  $W_{n_{UC}}$  are  $W_n$  points on the lower and upper portion of the circle RE; and  $W_{n_{LA}}$  and  $W_{n_{UA}}$  the analogous points on the ellipse AE. As in the previous cases, these values will depend upon the value of  $Q_n$ ,  $Q_{n_{Li}} \leq Q_n \leq Q_{n_{Ui}}$ , or equivalently the value of  $U$ . For a given value of  $U$ , say  $U^*$ ,  $W_{n_{LC}}$  and  $W_{n_{UC}}$  are the smallest and largest values of equation (2.3.20). The values  $W_{n_{LA}}$  and  $W_{n_{UA}}$  are the smallest and largest values of the following:

$$\frac{(a+P_A Q^*)}{(C_A+1)} \pm \sqrt{\frac{a+P_A Q^*}{C_A+1}^2 - \frac{a^2+b^2-c-2bQ^*+(C_A+1)Q^{*2}}{C_A+1}} \quad (2.3.28)$$

where  $Q^* = b - U^*$ .

The case where the curves RE and AE intersect at only one point must also be considered. This will happen whenever

$$(a+b)^2 - 2\left(1+\frac{1}{n}\right)(a^2+b^2-c) = 0.$$

If this is true the curves will intersect at the point

$$W_n = Q_n = \frac{n(a+b)}{2(n+1)}. \quad (2.3.29)$$

Based on the previous discussion this can only occur in the following situations:

- (1) the curve RE contains AE;
- (2) the curves AE and RE contain no points in common, except for the point of intersection given in equation (2.3.29).

Situation (2) will occur whenever the inequalities given by equations (2.3.15) and (2.3.16) are satisfied. Since the point of intersection will be on the boundary of RE, the integration regions  $U_U$ ,  $U_L$ ,  $Z_U$ , and  $Z_L$  can still be obtained by equations (2.3.18) and (2.3.19).

Situation (1) will occur whenever the inequality given in equation (2.3.24) is satisfied. The integration region must now be broken up into three pieces as shown in Figure 6. This is simply a special case of Figure 5 and may be evaluated by the same methods used to evaluate equation (2.3.25).

The curves RE and AE may also intersect at two points. This will happen whenever

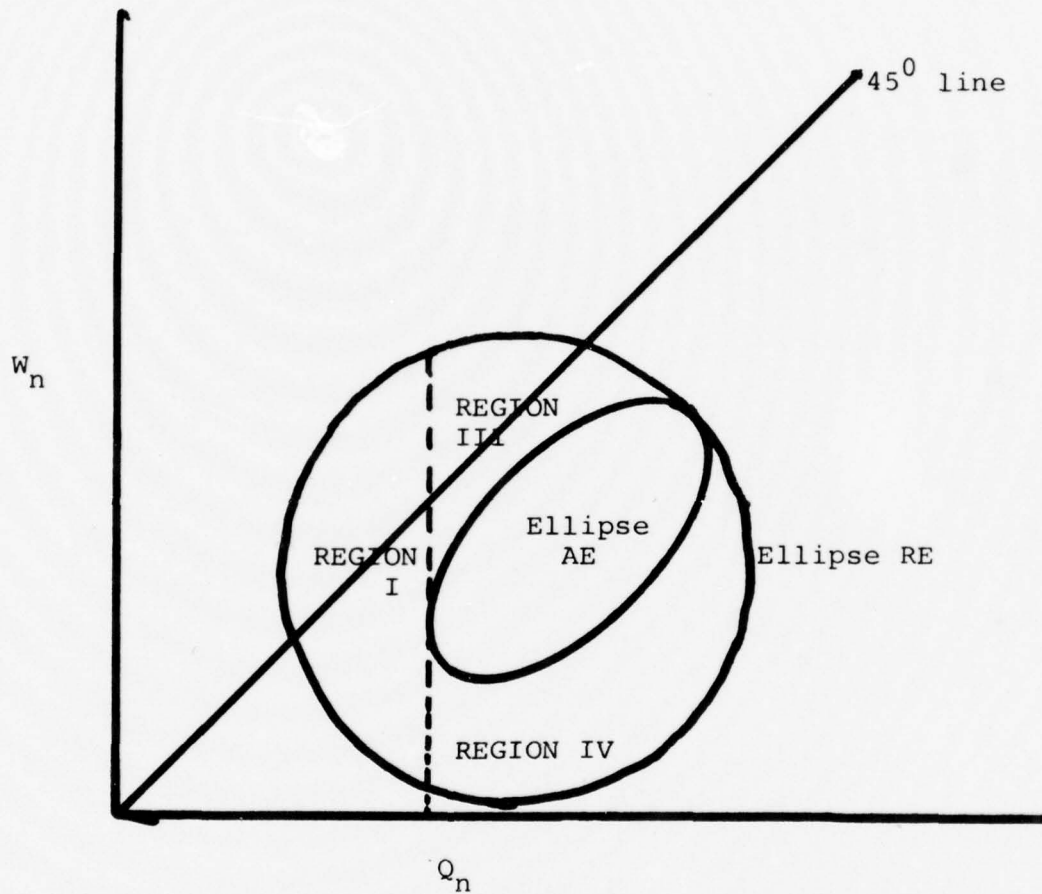
$$(a+b)^2 - 2\left(1+\frac{1}{n}\right)(a^2+b^2-c) > 0.$$

This indicates that one of the following geometric relationships must exist:

- (1) The ellipse AE is contained inside the circle RE, with the  $Q_n$  end points of AE touching the circle.
- (2) The intersection points fall below the axis of the ellipse AE, which is parallel to the line  $W_n = Q_n$ .
- (3) The intersection points fall above the axis of the ellipse AE, which is parallel to the line  $W_n = Q_n$ .

FIGURE 6

An Integration Region  
Consisting of Three Pieces



Consider the following set of rotated axes ( $45^\circ$  rotation):

$$\begin{aligned} Q_n' &= \frac{\sqrt{2}}{2} [Q_n + W_n] \\ W_n' &= \frac{\sqrt{2}}{2} [-Q_n + W_n] \end{aligned} \quad (2.3.29)$$

The ellipse AE in terms of this new coordinate system becomes:

$$\begin{aligned} (C_A + 1 - P_A) Q_n'^2 - \left[ \frac{\sqrt{2}(a+b)}{2(C_A + 1 - P_A)} \right]^2 + (C_A + 1 + P_A) \left[ W_n' - \frac{\sqrt{2}(a-b)}{2(C_A + 1 + P_A)} \right]^2 \\ = c - a^2 - b^2 + \frac{(a-b)^2}{2(C_A + 1 + P_A)} + \frac{(a+b)^2}{2(C_A + 1 - P_A)} \end{aligned} \quad (2.3.30)$$

Also, the line  $W_n = Q_n$  becomes:

$$W_n' = 0. \quad (2.3.31)$$

From these equations criteria for situations (1) - (3) can be established. Situation (1) will occur whenever  $a = b$ ; situation (2) will occur whenever  $a > b$ ; and situation (3) will occur whenever  $a < b$ .

Situation (1) is shown in Figure 7. The integration region must be divided into at most four subregions, as in Equation (2.3.25). The integration limits are the same as those obtained for equation (2.3.25), with the exception that one or two of the subregions may be empty.

Situation (2) is shown in Figure 8. The integration region must now be divided into three subregions. The range of  $Q_n$  for each of the subregions is as follows:

$$\begin{aligned}
 \text{Region I: } Q_{n_{L1}} &= Q_{n_{LC}} \leq Q_n \leq Q_{n_{LI}} = Q_{n_{U1}} \\
 \text{Region II: } Q_{n_{L2}} &= Q_{n_{LI}} \leq Q_n \leq Q_{n_{UI}} = Q_{n_{U2}} \\
 \text{Region III: } Q_{n_{L3}} &= Q_{n_{UI}} \leq Q_n \leq Q_{n_{UC}} = Q_{n_{U3}} \quad (2.3.32)
 \end{aligned}$$

The quantities  $Q_{n_{LC}}$  and  $Q_{n_{UC}}$  are again the two  $Q_n$  end points of the circle RE, or the smallest and largest values of equation (2.3.17).  $Q_{n_{LI}}$  and  $Q_{n_{UI}}$  are the intersection points of the ellipse AE with the circle RE, or the smallest and largest values of the following equation:

$$\frac{(a+b) \pm \sqrt{(a+b)^2 - 2\left(1+\frac{1}{n}\right)(a^2+b^2-c)}}{2\left(1+\frac{1}{n}\right)} \quad (2.3.33)$$

FIGURE 7

Integration Region When Ellipse AE  
Intersects Circle RE at Two Points  
Situation 1

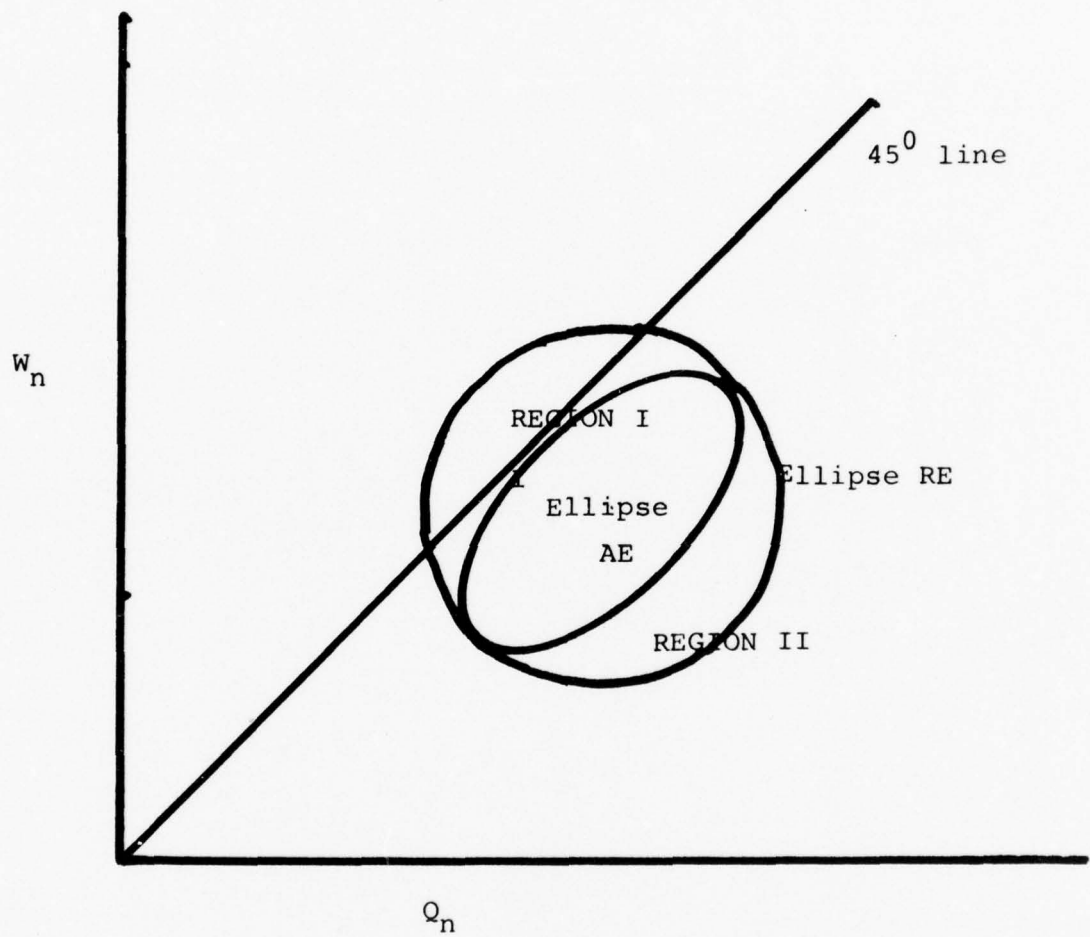
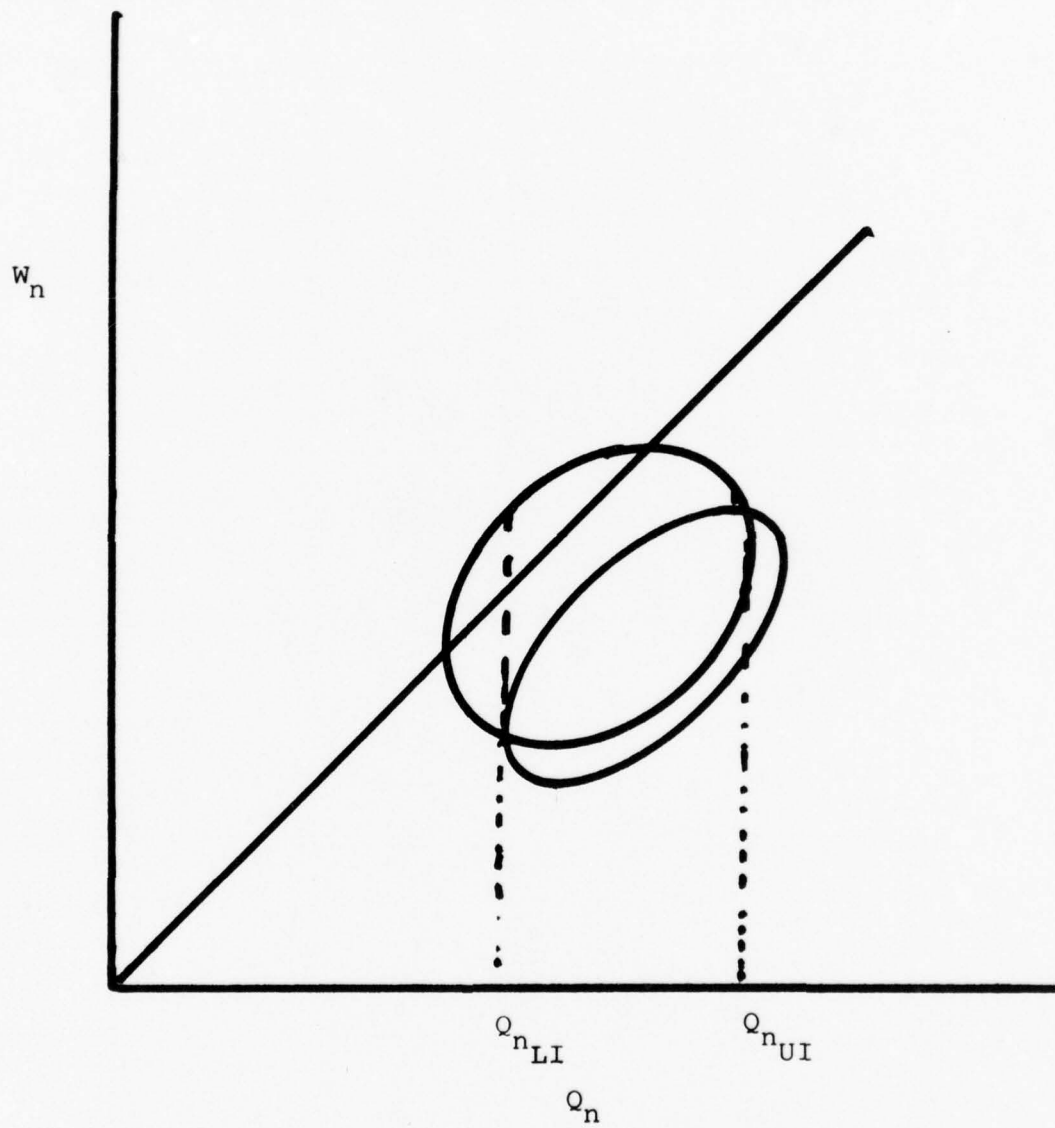


FIGURE 8

Integration Region When Ellipse AE  
Intersects Circle RE at Two Points  
Situation 3



The  $U$  integration limits for each region are then given by:

$$\begin{aligned} U_{Li} &= b - Q_{n_{Ui}} \\ U_{Ui} &= b - Q_{n_{Li}} \\ i &= 1, 2, 3 \end{aligned} \quad (2.3.34)$$

The range of  $W_n$  for each of the subregions is as follows:

$$\begin{aligned} \text{Region I: } W_{n_{L1}} &= W_{n_{LC}} \leq W_n \leq W_{n_{UC}} = W_{n_{U1}} \\ \text{Region II: } W_{n_{L2}} &= W_{n_{LC}} \leq W_n \leq W_{n_{UE}} = W_{n_{U2}} \\ \text{Region III: } W_{n_{L3}} &= W_{n_{LC}} \leq W_n \leq W_{n_{UC}} = W_{n_{U3}} \end{aligned} \quad (2.3.35)$$

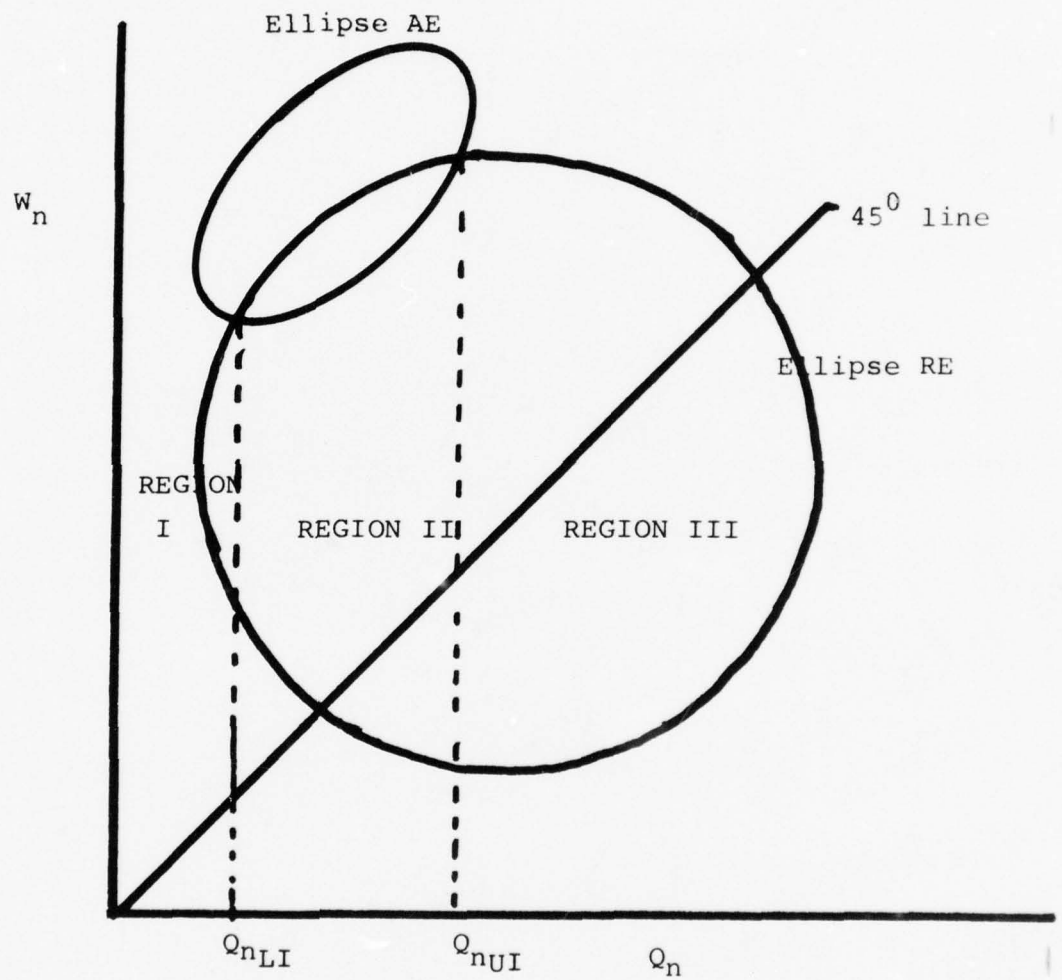
For a given value of  $U$ , say  $U^*$ ,  $W_{n_{LC}}$  and  $W_{n_{UC}}$  are the smallest and largest values of equation (2.3.20) and  $W_{n_{UC}}$  is the larger value of equation (2.3.28). Thus, the  $Z$  integration limits are obtained as:

$$\begin{aligned} Z_{Li} &= a - W_{n_{Ui}} \\ Z_{Ui} &= a - W_{n_{Li}} \\ i &= 1, 2, 3 \end{aligned} \quad (2.3.36)$$

Situation (3) is shown in Figure 9. As in situation (2), the integration region must be broken up into three subregions. The range of  $Q_n$  for each of the subregions and the  $U$  integration limits are still given by equations (2.3.32) and

FIGURE 9

Integration Region When Ellipse AE  
Intersects Circle RE at Two Points  
Situation 3



(2.3.34) respectively. However, the range of  $W_n$  for each of the subregions is now:

$$\begin{aligned}
 \text{Region I: } W_{n_{L1}} &= W_{n_{LC}} \leq W_n \leq W_{n_{UC}} = W_{n_{U1}} \\
 \text{Region II: } W_{n_{L2}} &= W_{n_{LC}} \leq W_n \leq W_{n_{LE}} = W_{n_{U2}} \\
 \text{Region III: } W_{n_{L3}} &= W_{n_{LC}} \leq W_n \leq W_{n_{UC}} = W_{n_{U3}} \quad (2.3.36)
 \end{aligned}$$

Where  $W_{n_{LE}}$  is the smaller value of equation (2.3.28).

Given these values the  $Z$  integration limits are given by equation (2.3.36).

It is also possible that the ellipse  $AE$  does not exist. This will occur whenever the surface  $B_A$  does not intersect the mapping function  $P$ , or whenever the following inequality is satisfied:

$$\frac{n(a-b)^2}{2(n+1)[(n+1)V_A+1]} - C - \left[ \frac{a^2}{n+1} - \frac{b^2}{n+1} \right] \geq 0 \quad (2.3.37)$$

This is not a special case, however, because whenever this inequality is satisfied, inequalities (2.3.15) and (2.3.16) are also satisfied. Thus the integration regions are obtained from equations (2.3.17) - (2.3.20).

In summary, this section has discussed the various types of integration regions that can result when only a decision to accept  $H_0$  is possible at stage  $n$ , criteria for determining when each of these regions is appropriate, and formulas to calculate the required  $U$ ,  $Z$  limits for each of these regions.

IV. Case when either a decision to accept or reject  $H_0$  is possible at stage  $n$ .

Whenever  $0 < V_A < V_R < \infty$ , both acceptance and rejection are possible at stage  $n$ . In this case, both the curves AE and RE become equations of an ellipse. In order to determine the integration region, it is necessary to know the intersection points of the two ellipses.

The intersection points are most easily found by transforming AE and RE into a coordinate system rotated 45 degrees. The equation for RE in the rotated axes becomes,  $RE'$ :

$$\begin{aligned} (C_R - P_R + 1) Q_n'^2 + (C_R + 1 + P_R) W_n'^2 - S(2a + 2b) Q_n' \\ - S(2a - 2b) W_n' = C - a^2 - b^2 \end{aligned} \quad (2.3.30)$$

and that of AE ,

$AE'$ :

$$\begin{aligned} (C_A - P_A + 1) Q_n'^2 + (C_A + 1 + P_A) W_n'^2 - S(2a + 2b) Q_n' \\ - S(2a - 2b) W_n' = C - a^2 - b^2 \end{aligned} \quad (2.3.31)$$

where  $S$  is given by

$$S = \sin(45^\circ) = \frac{\sqrt{2}}{2}$$

These equations may be further simplified as:

RE' :

$$\begin{aligned} & (C_R - P_R + 1) \left\{ Q_n' - \frac{S(a+b)}{(C_R - P_R + 1)} \right\}^2 + (C_R - P_R + 1) \left\{ W_n' - \frac{S(a-b)}{(C_R + P_R + 1)} \right\}^2 \\ &= c - a^2 - b^2 + \frac{(a+b)^2}{2(C_R - P_R + 1)} + \frac{(a-b)^2}{2(C_R + P_R + 1)} \end{aligned}$$

and

AE' :

$$\begin{aligned} & (C_A - P_A + 1) \left\{ Q_n' - \frac{S(a+b)}{(C_A - P_A + 1)} \right\}^2 + (C_A + P_A + 1) \left\{ W_n' - \frac{S(a-b)}{(C_A + P_A + 1)} \right\}^2 \\ &= c - a^2 - b^2 + \frac{(a+b)^2}{2(C_A - P_A + 1)} + \frac{(a-b)^2}{2(C_A + P_A + 1)} \end{aligned}$$

Since

$$P_A = \frac{1}{2nV_A}$$

and

$$C_A = \frac{2V_A + 1}{2nV_A} ,$$

(with similar expressions for  $P_R$  and  $C_R$ ), these may be substituted into the above; which yields after combining similar terms, the following expressions:

RE' :

$$\begin{aligned}
& (C_R - P_R + 1) \left\{ Q'_n - \frac{S(a+b)}{(C_R - P_R + 1)} \right\}^2 + (C_R + P_R + 1) \left\{ W'_n - \frac{S(a-b)}{(C_R + P_R + 1)} \right\}^2 \\
& = C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2_n}{2(n+1)(V_R + nV_R + 1)}
\end{aligned}$$

and

AE' :

$$\begin{aligned}
& (C_A - P_A + 1) \left\{ Q'_n - \frac{S(a+b)}{(C_A - P_A + 1)} \right\}^2 + (C_A + P_A + 1) \left\{ W'_n - \frac{S(a-b)}{(C_A + P_A + 1)} \right\}^2 \\
& = C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2_n}{2(n+1)(V_A + nV_A + 1)}
\end{aligned}$$

Since

$$C_A - P_A + 1 = C_R - P_R + 1 ,$$

the above equations show that both curves will have identical  $Q'_n$  coordinates for their centers.

Solving for  $Q'_n$  in  $RE'$  yields a solution of the following form:

$$Q'_n = K \pm D$$

where

$$K = \frac{S(a+b)}{(C_R - P_R + 1)}$$

$$D = \sqrt{\frac{.5(a+b)^2}{(C_R - P_R + 1)} - \left[ \frac{a^2 + b^2 - c + (C_R + 1 + P_R)W_n'^2 - S(2a+2b)W_n'}{C_R - P_R + 1} \right]}$$

Substituting this form in the equation for  $AE'$  yields

$$\begin{aligned} & (C_A - P_A + 1)(K^2 + D^2) + (C_A + 1 + P_A)W_n'^2 \\ & - S(2a+2b)K - S(2a-2b)W_n' \\ & + (\pm 2KD(C_A - P_A + 1) - S(2a+2b)(\pm D)) \\ & = C - a^2 - b^2 \end{aligned} \quad (2.3.32)$$

In general an equation describing the intersection of two ellipses will be a quartic. Equation (2.3.32) is a special case, however, and can be reduced to a quadratic by noting that the following term

$$\pm D(2K(C_A - P_A + 1) - S(2a+2b))$$

$$= \frac{+}{-} D \left[ \frac{S(2a+2b)(C_A - P_A + 1)}{(C_R - P_R + 1)} - S(2a+2b) \right]$$

is zero since

$$(C_A - P_A + 1) = (C_R - P_R + 1) = \frac{n+1}{n}.$$

Solving equation (2.3.32) for  $W_n'$  and substituting into  $RE'$  yields the following  $W_n'$ ,  $Q_n'$  intersection points:

$$W_n' = 0 \quad (2.3.33)$$

$$Q_n' = \frac{1}{n+1} \left[ S(a+b)n \pm \sqrt{S[(a+b)n]^2 - n(n+1)(a^2+b^2-c)} \right]$$

In terms of the original  $W_n$ ,  $Q_n$  axes the intersection points become:

$$W_n = Q_n = \frac{1}{2(n+1)} \left[ n(a+b) \pm \sqrt{[(a+b)n]^2 - n(n+1)(a^2+b^2-c)} \right] \quad (2.3.34)$$

This means that the two ellipses, AE and RE, will intersect at zero, one, or two points. The sign of the discriminant of equation (2.3.34),

$$DIS = [(a+b)n]^2 - n(n+1)(a^2+b^2-c),$$

determines the number of intersection points. Whenever:

$$1. \quad DIS < 0 \quad (2.3.35)$$

AE and RE will not intersect.

$$2. \quad \text{DIS} = 0 \quad (2.3.36)$$

AE and RE will intersect at only one point,  
this point being

$$W_n = Q_n = \frac{n(a+b)}{2(n+1)}$$

$$3. \quad \text{DIS} > 0 \quad (2.3.37)$$

AE and RE will intersect at two points.

Consider first, the case when AE and RE do not intersect, or when equation (2.3.35) is satisfied. This indicates one of the following geometric relationships must exist:

- (1) the curves AE and/or RE do not exist
- (2) the curve RE contains AE
- (3) the curve AE contains RE
- (4) the curves AE and RE contain no points in common.

Situation (1) will occur if either of the ellipses has an imaginary radius, or whenever either of the following equations is satisfied:

$$C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R + nV_R + 1)} \leq 0 \quad (2.3.38)$$

$$C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_A + nV_A + 1)} \leq 0 \quad (2.3.39)$$

Since  $V_A \leq V_R$ , inequality (2.3.39) will be satisfied whenever (2.3.38) is satisfied. If (2.3.38) is satisfied,  $f(a,b,c) = 0$ , since none of the points that can be mapped into  $a,b,c$  lie in the continuation region.

If inequality (2.3.39) is satisfied and (2.3.38) is not, the point  $a,b,c$  is located such that the mapping function  $P$  intersects the rejection surface but never intersects the acceptance curve. This reduces to a case previously discussed, the case when only a decision to reject  $H_0$  is possible, and the integration regions are given by equations (2.3.11) through (2.3.14).

Assuming neither inequality (2.3.38) or (2.3.39) is satisfied, situation (4) will occur when neither curve contains the other's center, or when the following inequalities are satisfied:

$$\left(\frac{V_R + nV_R + 1}{nV_R}\right) \left(\frac{n^2(a-b)^2}{2}\right) \left[\frac{V_R}{(V_R + nV_R + 1)} - \frac{V_A}{(V_A + nV_A + 1)}\right]^2$$

$$- \left\{ C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_R + nV_R + 1)} \right\} > 0$$

(2.3.40)

and

$$\left(\frac{V_A + nV_A + 1}{nV_A}\right) \left(\frac{n^2(a-b)^2}{2}\right) \left[\frac{V_R}{(V_R + nV_R + 1)} - \frac{V_A}{(V_A + nV_A + 1)}\right]^2$$

$$- \left\{ C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_A + nV_A + 1)} \right\} > 0$$

(2.3.41)

As it is necessary for both inequalities to hold, and inequality (2.3.41) implies inequality (2.3.40), it is only necessary to examine the former. In other words, situation (4) will occur whenever RE and AE do not intersect, and RE does not contain AE's center point.

The set H consists of all points  $W_n, Q_n$  contained inside the ellipse RE. The integration region in this case becomes identical to that required for the case when only rejection is possible and can be evaluated using equations (2.3.11) - (2.3.14).

Situation (3) will occur whenever the four end points of the ellipse RE' are all points inside AE. First,

consider the RE' end points along the  $Q_n'$  axis. When this is substituted into AE', the following inequality must hold for situation (3) to occur:

$$\left(\frac{n(a-b)^2}{2}\right)\left(\frac{V_R}{(V_R+nV_R+1)} - \frac{V_A}{(V_A+nV_A+1)}\right) + \left(\frac{V_A+nV_A+1}{nV_A}\right)\left(\frac{(a-b)^2n^2}{2}\right)\left(\frac{V_R}{(V_R+nV_R+1)} - \frac{V_A}{(V_R+nV_A+1)}\right)^2 < 0.$$

Since  $V_A \leq V_R$ , this inequality can not be satisfied; and thus situation (3) can never occur.

Having shown that situation (3) cannot occur, situation (2) will occur whenever both the ellipses RE and AE exist (neither inequality (2.3.38) nor (2.3.31) is satisfied), and inequality (2.3.41) is not satisfied. In this case the integral given in equation (2.3.8) must be broken up into four separate pieces, similar to that given in equation (2.3.25). The limits  $U_{Ui}$ ,  $U_{Li}$ ,  $Z_{Ui}$  and  $Z_{Li}$ :  $i = 1, \dots, 4$  must be determined for each region.

For each region a range of  $Q_n$  can be found;

$Q_{n_{Li}} \leq Q_n \leq Q_{n_{Ui}}$  from which the U integration limits are obtained as:

$$U_{Li} = b - Q_{n_{Ui}}$$

$$U_{Ui} = b - Q_{n_{Li}}.$$

The range of  $Q_n$  for each of the pieces is as follows:

$$\text{Region I: } Q_{n_{L1}} = Q_{n_{LR}} \leq Q_n \leq Q_{n_{LA}} = Q_{n_{U1}}$$

$$\text{Region II: } Q_{n_{L2}} = Q_{n_{UA}} \leq Q_n \leq Q_{n_{UR}} = Q_{n_{U2}}$$

$$\text{Region III: } Q_{n_{L3}} = Q_{n_{LA}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U3}}$$

$$\text{Region IV: } Q_{n_{L4}} = Q_{n_{LA}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U4}}$$

(2.3.42) .

Where  $Q_{n_{LR}}$  and  $Q_{n_{UA}}$  are the minimum and maximum  $Q_n$  coordinates on the ellipse RE; and  $Q_{n_{LA}}$  and  $Q_{n_{UA}}$  are the analogous quantities on the ellipse AE.

$Q_{n_{LR}}$  and  $Q_{n_{UR}}$  have previously been derived as the smallest and largest values of equation (2.3.12). A similar expression derived for RE, yields  $Q_{n_{LA}}$  and  $Q_{n_{UA}}$  as the smallest and largest values of

$$\left[ \frac{b(C_A+1) + aP_A}{(C_A+1)^2 - P_A^2} \right] + \sqrt{\left[ \frac{b(C_A+1) + aP_A}{P_A^2 - (C_A+1)^2} \right]^2 - \left[ \frac{a^2 - (C_A+1)(a^2+b^2-c)}{P_A^2 - (C_A+1)^2} \right]}$$

(2.3.43) .

The range of  $W_n$  for each piece depends upon the value of  $Q_n$  (or equivalently  $U$ ). For a given value of  $U_i$ , say  $U^*$ ,  $U^* = b - Q_{n_i}^*$ ;  $Q_{n_{Li}} \leq Q_{n_i}^* \leq Q_{n_{Ui}}$  a range of  $W_n$  values can be defined;  $W_{n_{Li}} \leq W_n \leq W_{n_{ui}}$ , from which the  $Z$  limits are obtained as:

$$Z_{L_i} = a - W_{n_{Ui}}$$

$$Z_{U_i} = a - W_{n_{Li}} .$$

The range of  $W_n$  for each of the pieces is as follows:

$$\text{Region I: } W_{n_{L1}} = W_{n_{LR}} \leq W_n \leq W_{n_{UR}} = W_{n_{U1}}$$

$$\text{Region II: } W_{n_{L2}} = W_{n_{LR}} \leq W_n \leq W_{n_{UR}} = W_{n_{U2}}$$

$$\text{Region III: } W_{n_{L3}} = W_{n_{UA}} \leq W_n \leq W_{n_{UR}} = W_{n_{U3}}$$

$$\text{Region IV: } W_{n_{L4}} = W_{n_{LR}} \leq W_n \leq W_{n_{LA}} = W_{n_{U4}}$$

(2.3.44) .

$W_{n_{LR}}$  and  $W_{n_{UR}}$  are the upper and lower points on the ellipse **RE**, for a given value of  $U^* = b - Q_n^*$ .

These have been derived previously as the smallest and largest values of equation (2.3.13).  $W_{r_{LA}}$  and  $W_{n_{UA}}$  are the analogous points on the ellipse **AE**, and are obtained as the smallest and largest value of:

$$\left[ \frac{(a+P_A Q^*)}{(C_A+1)} \right] \pm \sqrt{\left[ \frac{a+P_A Q^*}{C_A+1} \right]^2 - \left[ \frac{a^2+b^2-C-2bQ^*+(C_A+1)Q^{*2}}{(C_A+1)} \right]}$$

(2.3.45) .

Next consider the case when **AE** and **RE** intersect at only one point, which will occur whenever equation (2.3.36) is satisfied. Based on the previous discussion this can only occur in the following situations:

- (1) either one or both of the curves **AE** and **RE** do not exist
- (2) the curve **RE** contains **AE**
- (3) the curves **AE** and **RE** contain no points in common, except for the point of intersection.

Situation (1) can never occur if equations (2.3.36) or (2.3.37) hold. This can be shown as follows:

If

$$(a+b)^2 - \left(2 \frac{n+1}{n}\right) (a^2+b^2-c) \geq 0$$

then

$$c = a^2+b^2 - \frac{(a+b)^2}{2(n+1)} + \frac{S_1}{2(n+1)}$$

$S_1$  being a quantity greater than or equal to zero.

Substituting this result into the equation of the radius of the ellipse AE and simplifying yields:

$$\text{Radius AE} = \frac{(a-b)^2}{2(C_A+1+P_A)} + \frac{S_1}{2(n+1)} .$$

Since this quantity will always be greater than equal to zero, the ellipse AE will always exist. The previous section also showed that a sufficient condition for RE to exist was the existence of AE. Hence, intersection of the ellipses AE and RE is a sufficient condition for their existence.

Situation (3) will occur whenever the inequality given in equation (2.3.11) is satisfied. Since the point of intersection will be on the boundary of RE, the integration regions  $U_L$ ,  $U_L$ ,  $Z_U$ , and  $Z_L$  can still be obtained by equations (2.3.11) and (2.3.14).

Similarly situation (2) occurs whenever inequality (2.3.41) is not satisfied, and requires the integration to be broken up into four pieces. The integration limits in each of these pieces may still be obtained by equations (2.3.42) through (2.3.45).

The curves AE and RE will intersect at two points whenever inequality (2.3.37) holds. In general, two ellipses can intersect at two points in many ways. However, consider the equations in the rotated axes coordinated system:

RE':

$$\left(\frac{n+1}{n}\right) \left\{ Q_n' - \left[ \frac{\sqrt{2}(a+b)n}{2(n+1)} \right] \right\}^2 + \left( \frac{V_R + nV_R + 1}{nV_R} \right) \left\{ W_n' - \left[ \frac{\sqrt{2}(a-b)nV_R}{2(V_R + nV_R + 1)} \right] \right\}^2$$

$$= C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a+b)^2 n}{2(n+1)(V_R + nV_R + 1)}$$

and

AE':

$$\left(\frac{n+1}{n}\right) \left\{ Q_n' - \left[ \frac{\sqrt{2}(a+b)n}{2(n+1)} \right] \right\}^2 + \left( \frac{V_A + nV_A + 1}{nV_A} \right) \left\{ W_n' - \left[ \frac{\sqrt{2}(a-b)nV_A}{2(V_A + nV_A + 1)} \right] \right\}^2$$

$$= C - \frac{a^2}{n+1} - \frac{b^2}{n+1} - \frac{(a-b)^2 n}{2(n+1)(V_A + nV_A + 1)}$$

From these equations the following relationships may be noted:

- (a) the curves  $RE'$  and  $AE'$  will have parallel major axes (i.e., parallel to the line  $W_n' = 0$ ).
- (b) the major axis of  $RE'$  will be greater than or equal to the major axis of  $AE'$ .
- (c) the major axes of  $RE'$  and  $AE'$  will always lie on the same side of the line  $W_n' = 0$ .
- (d) the two curves will have the same center point and equal major axes whenever  $a = b$ .
- (e) since

$$Q_n' = \frac{\sqrt{2}}{2} [Q_n + W_n]$$

$$W_n' = \frac{\sqrt{2}}{2} [-Q_n + W_n] ,$$

if the curves intersect, the intersection points will lie along the line  $W_n = Q_n$  or  $W_n' = 0$ .

Given these relationships one can conclude that whenever the curves intersect at two points, one of the following geometric situations must exist:

- (1) the ellipse  $RE'$  circumscribes the ellipse  $AE'$ .
- (2) the major axes of the ellipses lie above the line  $W_n' = 0$ .
- (3) the major axes of the ellipses lie below the line  $W_n' = 0$ .

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UNION COLL AND UNIV SCHENECTADY NY INST OF ADMINISTR--ETC F/G 12/1  
AN EXACT TEST FOR THE SEQUENTIAL ANALYSIS OF VARIANCE.(U)

AUG 79 R W MILLER

N00014-77-C-0438

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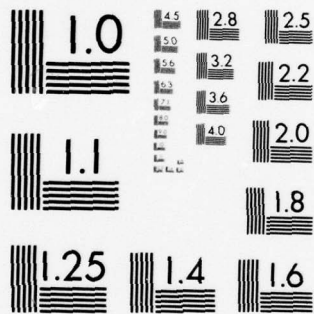
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Situation (1) will occur whenever  $a = b$ , and requires the integral of equation (2.3.8) to be broken up into two pieces. These two pieces may be described by  $W_n, Q_n$  regions identical to those of Regions III and IV given in (2.3.42) and (2.3.44). Thus the integration limits  $U_{Li}, U_{Ui}, Z_{Li}$ , and  $Z_{Ui}$  may be obtained from equations (2.3.43) - (2.3.45).

Situation (2) will occur whenever  $a > b$ , and requires the integral of equation (2.3.8) to be broken up into five pieces, as shown in Figure 10. The range of  $Q_n$  for each of the subregions is as follows:

$$\begin{aligned}
 \text{Region I: } Q_{n_{L1}} &= Q_{n_{LR}} \leq Q_n \leq Q_{n_{LA}} = Q_{n_{U1}} \\
 \text{Region II: } Q_{n_{L2}} &= Q_{n_{LA}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U2}} \\
 \text{Region III: } Q_{n_{L3}} &= Q_{n_{LA}} \leq Q_n \leq Q_{n_{LI}} = Q_{n_{U3}} \\
 \text{Region IV: } Q_{n_{L4}} &= Q_{n_{UI}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U4}} \\
 \text{Region V: } Q_{n_{L5}} &= Q_{n_{UA}} \leq Q_n \leq Q_{n_{UR}} = Q_{n_{U5}}
 \end{aligned}$$

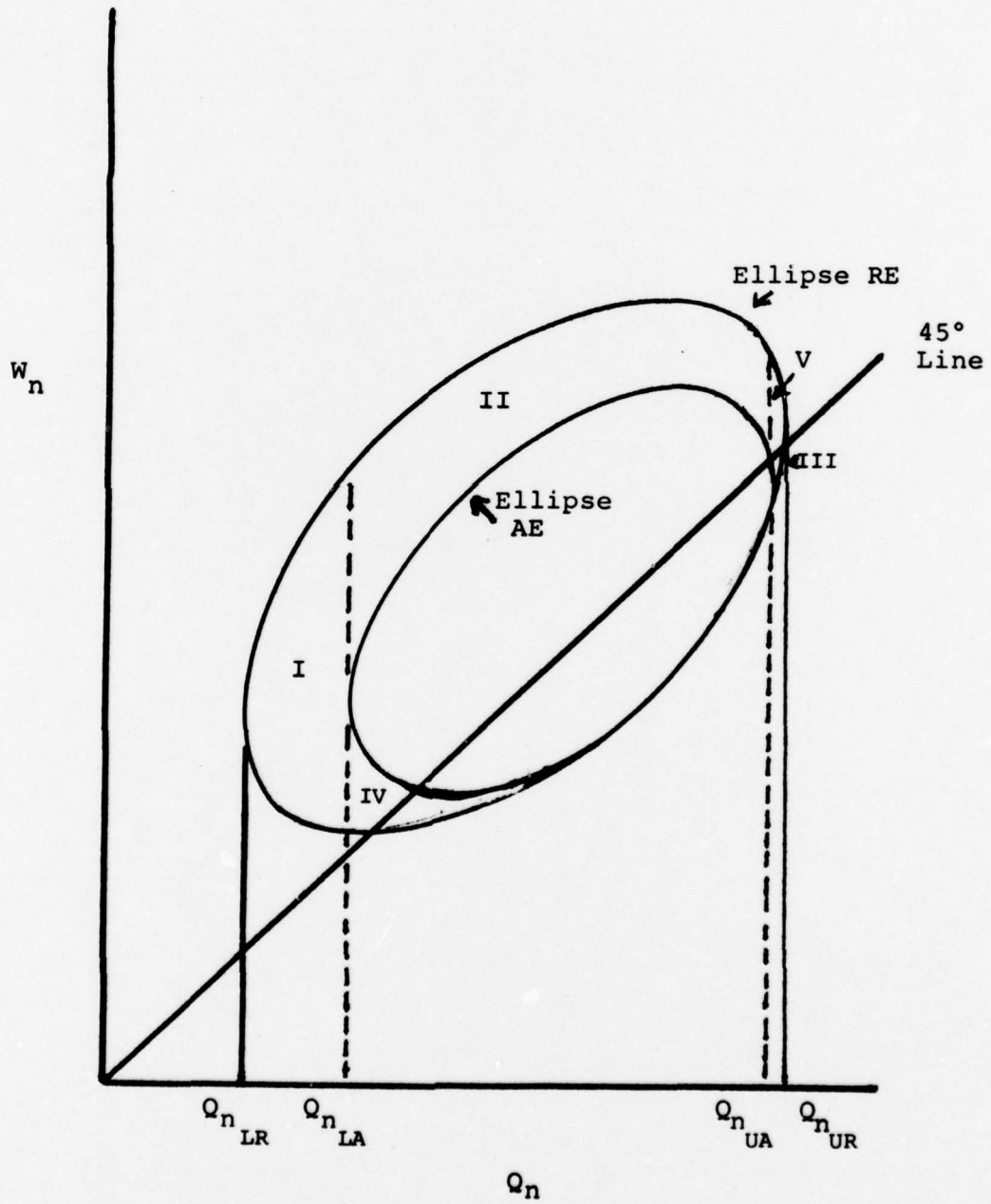
(2.3.46) .

The quantities  $Q_{n_{LA}}$  and  $Q_{n_{UA}}$  have previously been defined and may be obtained as the minimum and maximum of (2.3.43). Similarly  $Q_{n_{LR}}$  and  $Q_{n_{UR}}$  are the minimum and maximum of (2.3.12).  $Q_{n_{LI}}$  and  $Q_{n_{UI}}$  represent the two intersection points of AE and RE, and are defined as:

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FIGURE 10

Integration Region When Both a Decision  
to Accept and Reject is Possible  
Situation 2



$$Q_{n_{LI}} = \min \{R_1, R_2\}$$

$$Q_{n_{UI}} = \max \{R_1, R_2\}$$

where

$$R_1 = \frac{(a+b)n + n\sqrt{(a+b)^2 - 2\left(\frac{n+1}{n}\right)(a^2+b^2-c)}}{2(n+1)}$$

$$R_2 = \frac{n(a+b) - n\sqrt{(a+b)^2 - 2\left(\frac{n+1}{n}\right)(a^2+b^2-c)}}{2(n+1)} \quad (2.3.47).$$

The U integration limits for each piece are again obtained as:

$$U_{Ui} = b - Q_{n_{Li}}$$

$$U_{Li} = b - Q_{n_{Ui}}$$

Similarly for a given value of U, say  $U^* = b - Q^*$ , the range of  $W_n$  for each region is given by:

$$\text{Region I: } W_{n_{L1}} = W_{n_{LR}} \leq W_n \leq W_{n_{UR}} = W_{n_{U1}}$$

$$\text{Region II: } W_{n_{L2}} = W_{n_{UA}} \leq W_n \leq W_{n_{UR}} = W_{n_{U2}}$$

$$\text{Region III: } W_{n_{L3}} = W_{n_{LR}} \leq W_n \leq W_{n_{LA}} = W_{n_{U3}}$$

$$\text{Region IV: } W_{n_{L4}} = W_{n_{LR}} \leq W_n \leq W_{n_{LA}} = W_{n_{U4}}$$

$$\text{Region V: } W_{n_{L5}} = W_{n_{LR}} \leq W_n \leq W_{n_{UR}} = W_{n_{U5}}$$

$W_{n_{LR}}$  and  $W_{n_{UR}}$  being the maximum and minimum of (2.3.45),  
and  $W_{n_{LA}}$  and  $W_{n_{UA}}$  the same for (2.3.13).

The  $Z$  limits are obtained for each region as:

$$Z_{Ui} = a - W_{n_{Li}}$$

$$Z_{Li} = a - W_{n_{Ui}}$$

Situation (3) results whenever  $a < b$ , and again requires that equation (2.3.8) be split up into five separate integrals, as shown in Figure 11. In this case the range of  $Q_n$  for each of the subregions is as follows:

$$\text{Region I: } Q_{n_{L1}} = Q_{n_{LR}} \leq Q_n \leq Q_{n_{LA}} = Q_{n_{U1}}$$

$$\text{Region II: } Q_{n_{L2}} = Q_{n_{LA}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U2}}$$

$$\text{Region III: } Q_{n_{L3}} = Q_{n_{LA}} \leq Q_n \leq Q_{n_{LI}} = Q_{n_{U3}}$$

$$\text{Region IV: } Q_{n_{L4}} = Q_{n_{UI}} \leq Q_n \leq Q_{n_{UA}} = Q_{n_{U4}}$$

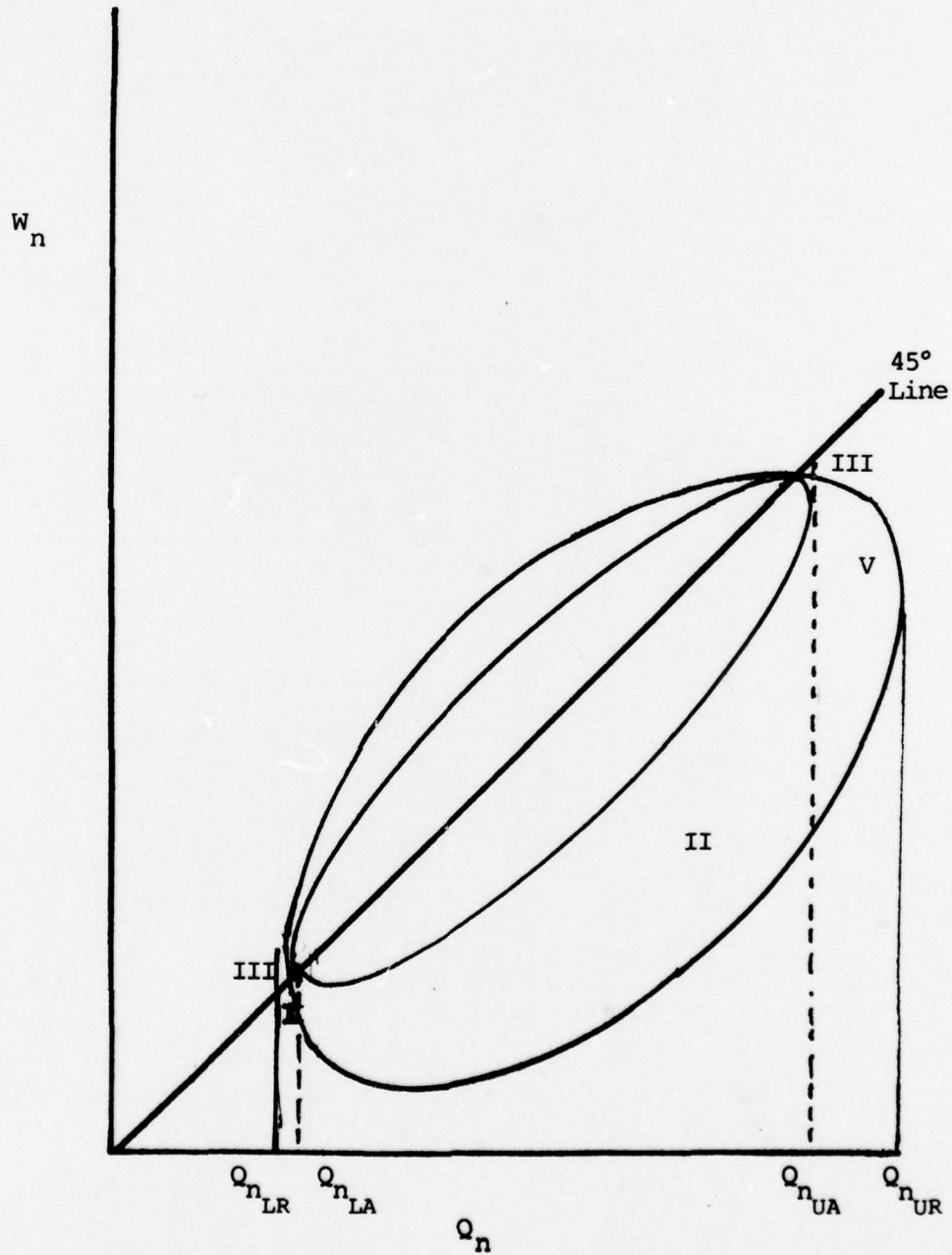
$$\text{Region V: } Q_{n_{L5}} = Q_{n_{UA}} \leq Q_n \leq Q_{n_{UR}} = Q_{n_{U5}}$$

(2.3.48).

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FIGURE 11

Integration Region When Both a Decision  
to Accept and Reject is Possible  
Situation 3



For a given value of  $U^* = b - Q^*$  the  $W_n$  range for each region is:

$$\text{Region I: } W_{nL1} = W_{nLR} \leq W_n \leq W_{nUR} = W_{nU1}$$

$$\text{Region II: } W_{nL2} = W_{nLR} \leq W_n \leq W_{nLA} = W_{nU2}$$

$$\text{Region III: } W_{nL3} = W_{nUA} \leq W_n \leq W_{nUR} = W_{nU3}$$

$$\text{Region IV: } W_{nL4} = W_{nUA} \leq W_n \leq W_{nUR} = W_{nU4}$$

$$\text{Region V: } W_{nL5} = W_{nLR} \leq W_n \leq W_{nUR} = W_{nU5}$$

(2.3.49).

#### 2.4 OBTAINING THE PROBABILITIES OF ACCEPTANCE, REJECTION AND CONTINUATION

The previous section (2.3) has given methods for calculating the density  $f_{n+1}(a,b,c)$ , for a given point  $W_{n+1} = a$ ,  $Q_{n+1} = b$ ,  $R_{n+1} = c$ , from the density at stage  $n$ ,  $f_n(W_n, Q_n, R_n)$ . Once this density has been obtained for all possible values of  $a, b, c$ , the probability of accepting  $H_0$  ( $P_A^{n+1}$ ), probability of rejecting  $H_0$  as ( $P_R^{n+1}$ ), and the probability of continuing ( $P_C^{n+1}$ ) must be calculated. This requires integrating the three dimensional density  $f_{n+1}(W_{n+1}, Q_{n+1}, R_{n+1})$  over all values of  $W_{n+1}, Q_{n+1}, R_{n+1}$  for which the statistic

$$v(W_{n+1}, Q_{n+1}, R_{n+1}) = \frac{[W_{n+1} - Q_{n+1}]^2}{2[(n+1)R_{n+1} - Q_{n+1}^2 - W_{n+1}^2]}$$

is in the appropriate region (e.g., acceptance region, rejection region, or continuation region). Thus  $P_A^{n+1}$ ,  $P_R^{n+1}$ , and  $P_C^{n+1}$  may be calculated as:

$$P_R^{n+1} = \iiint_{0 \leq v(W, Q, R) \leq v_R^{n+1}} f_{n+1}(W, Q, R) dW dQ dR$$

$$P_A^{n+1} = \int \int \int_{V_R^{n+1} \leq V(W,Q,R) \leq \infty} f_{n+1}(W,Q,R) dW dQ dR$$

and

$$P_C^{n+1} = \int \int \int_{V_A^{n+1} \leq V(W,Q,R) \leq V_A^{n+1}} f_{n+1}(W,Q,R) dW dQ dR$$

These integrals amount to integrating  $f_{n+1}(W,Q,R)$  over elliptic paraboloids, and may be reexpressed as the following iterated integrals:

$$\begin{aligned} P_A^{n+1} &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{R_a}^{\infty} f_{n+1}(W,Q,R) dR dW dQ \\ P_R^{n+1} &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{R_o}^{R_r} f_{n+1}(W,Q,R) dR dW dQ \\ P_C^{n+1} &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{R_r}^{R_a} f_{n+1}(W,Q,R) dR dW dQ \end{aligned} \quad (2.4.1).$$

with

$$R_O = \frac{W^2}{n+1} + \frac{Q^2}{n+1}$$

$$R_a = \frac{[W-Q]^2}{2(n+1)V_A^{n+1}} + \frac{W^2}{n+1} + \frac{Q^2}{n+1}$$

$$R_r = \frac{[W-Q]^2}{q(n+1)V_R^{n+1}} + \frac{W^2}{n+1} + \frac{Q^2}{n+1}$$

In practice only two of the three integrals need be calculated due to the following identity:

$$P_C^n = P_A^{n+1} + P_R^{n+1} + P_C^{n+1}.$$

So if  $P_A^i$  and  $P_R^i$  are calculated at each stage  $i$ ,  $P_C^i$  may be obtained by subtraction,

$$P_C^i = P_C^{i-1} - P_A^i P_R^i.$$

2.5 SUMMARY OF THE DIRECT METHOD FOR A  $k=2$  SANOVA TEST

The purpose of this section is to summarize the procedure for obtaining the OC and ASN curves for a  $k=2$  SANOVA test.

First, a test of this type requires specification of the following quantities:

- (1) The null hypothesis value,  $\lambda_0$ .
- (2) The alternative hypothesis value,  $\lambda_1$ .
- (3) A truncation point,  $m_0$ .
- (4) A set of regions:  $V_A^i, V_R^i, i = 2, \dots, m_0$ , such that at any stage  $N$

These regions are to be compared with the statistic,  $V_n$ , of equation (2.3.1), such that at any stage  $n$ ,

- (a)  $H_0$  is accepted if  $V_n \leq V_A^n$
- (b)  $H_1$  is accepted if  $V_n \geq V_R^n$ .

- (5) Values of  $\alpha$  and  $\beta$  (needed only if the regions are to be modified Wald regions).

Second, the first step at which a decision can be made, say  $n_1$ ,  $2 \leq n_1 \leq m_0$ , is determined.

Third, one must determine how many and which points on the OC and ASN curves will be calculated. Suppose  $L$  values are chosen, denoted by  $\lambda_\ell^*$ ,  $\ell = 1, \dots, L$ , such that  $\lambda_0 = \lambda_1^* < \lambda_2^* < \dots < \lambda_L^* = \lambda_1$ .

For a given  $\lambda_\ell^*$ , the first stage density  $f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1})$  may be calculated as follows:

$$\begin{aligned}
 f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1}) &= \left( \frac{1}{n_1} \right)^2 \chi^2_{2(n_1-1)} \left[ R_{n_1} - \frac{W_{n_1}^2}{n_1} - \frac{Q_{n_1}^2}{n_1} \right] \\
 &\cdot \phi \left( \sqrt{n_1} \left( \frac{W_{n_1}}{n_1} \right) \right) \cdot \phi \left( \sqrt{n_1} \left( \frac{Q_{n_1}}{n_1} - \sqrt{\lambda_{\ell}^{*1}} \right) \right)
 \end{aligned}
 \tag{2.5.1}$$

Note that this density is completely specified by  $\chi_{\ell}^{*}$  and  $n_1$ .

The probabilities of acceptance, rejection, and continuation at stage  $n_1$  (the first stage at which a decision can be made);  $P_A^{n_1}$ ,  $P_R^{n_1}$ , and  $P_C^{n_1}$ , may be calculated using the noncentral F distribution (given in equation (1.1.1)) and is shown in appendix A.

To calculate the joint density at the next stage,  $f_{n_1+1}(W_{n_1+1}, Q_{n_1+1}, R_{n_1+1})$ , requires utilizing the procedures developed in section 2.3.

As shown in section 2.3, this consists of performing a bivariate integration of the following five dimensional joint density function.

$$\begin{aligned}
 f_{n_1} \left( W_{n_1}, Q_{n_1}, R_{n_1}, X_{1n_2}, X_{2n_2} \right) &= f_{n_1} \left( W_{n_1}, Q_{n_1}, R_{n_1} \right) \\
 &\cdot \phi \left( X_{1n_2} \right) \cdot \phi \left( X_{2n_2} - \sqrt{\lambda_{\ell}^{*1}} \right)
 \end{aligned}
 \tag{2.5.2}$$

where  $n_2 = n_1 + 1$ .

This is the joint density of the statistics at stage  $n$ ;  $W_{n_1}, Q_{n_1}, R_{n_1}$ ; and the new observations taken at stage  $n_2 = n_1 + 1$ ;  $X_{1n_2}, X_{2n_2}$ .

For any given point:  $W_{n_1+1} = a, Q_{n_1+1} = b, R_{n_1+1} = c$ ; the joint density  $f_{n_1+1}(a, b, c)$  is calculated by performing the following bivariate integration.

$$f_{n_1+1}(a, b, c) = \int_{U_L}^{U_U} \int_{Z_L}^{Z_U} f_{n_1}^P(a-z, b-u, c-z^2-u^2, z, u) dz du \quad (2.5.3)$$

The limits  $U_L, U_U, Z_L$ , and  $Z_U$  are dependent upon the particular point  $(a, b, c)$  as well as the regions  $V_A^{n_1}$  and  $V_R^{n_1}$ .

If no decision could be made at stage  $n_1$ , these limits are the limits for integrating around the following circle.

$$c - z^2 - u^2 - \frac{(a-z)^2}{n_1} - \frac{(b-u)^2}{n_1} = 0 \quad (2.5.4)$$

and are given in equations (2.3.6) and (2.3.7). Whenever a decision can be made at stage  $n$ , the integration region becomes a subset of the points contained inside this circle.

In some cases the integral given in equation (2.5.3) cannot be evaluated as one integral; rather it must be broken up into several pieces, with the overall integral

being the sum of the individual integrals. Equation (2.3.25) is such an example. In such cases, the integration limits for each of the pieces must be determined.

The required integration region for equation (2.5.3) can be one of many. In section (2.3) every possible integration region has been explored; and for each case specific expressions for the  $U, Z$  integration limits have been given.

The  $U, Z$  integration determination may be best summarized in flowchart format, such as shown in Figure 12

This integration must be determined and performed for all points  $W_{n_1+1}, Q_{n_1+1}, R_{n_1+1}$ , thus obtaining the entire density  $f_{n_1+1}(W_{n_1+1}, Q_{n_1+1}, R_{n_1+1})$ . From this density the probabilities of acceptance ( $P_A^{n_1+1}$ ), rejection ( $P_R^{n_1+1}$ ), and continuation ( $P_C^{n_1+1}$ ) must be calculated. Their calculation requires performing a trivariate integration of the density  $f_{n_1+1}(W_{n_1+1}, Q_{n_1+1}, R_{n_1+1})$  over elliptic paraboloids. This is most easily performed as iterated integrals as shown in (2.4.1).

The entire process of obtaining the density,  $f_i(W_i, Q_i, R_i)$ , from the density,  $f_{i-1}^P(W_{i-1}, Q_{i-1}, R_{i-1}, X_{1i}, X_{2i})$ , and ultimately the probabilities,  $P_A^i, P_R^i, P_C^i$ , must be iterated for all stages,  $i = n_1 + 2, \dots, m_0$ .

The final result, for a given  $\lambda_\ell^*$ , is the set of probabilities,  $P_A^i, P_R^i, P_C^i, i = 2, \dots, m_0$ . These probabilities will depend upon the value of  $\lambda_\ell^*$ . This can easily be seen by noting that both the first step density of equation (2.5.1) as well as the five dimensional density of equation (2.5.2) are both functions of  $\lambda_\ell^*$ . Therefore, the notation  $P_A^i(\lambda_\ell^*), P_R^i(\lambda_\ell^*), P_C^i(\lambda_\ell^*), i = 2, \dots, m_0$ , will be used to denote such a dependence. From these probabilities, the point on the OC and ASN curves for  $\lambda = \lambda_\ell^*$  may be calculated. These quantities are calculated as follows:

$$OC(\lambda_\ell^*) = \sum_{L=Z}^{m_0} P_A^i(\lambda_\ell^*) \quad (2.5.5)$$

and

$$ASN(\lambda_\ell^*) = \sum_{L=Z}^{m_0} P_R^i(\lambda_\ell^*) + P_A^i(\lambda_\ell^*) \cdot i = 1 + \sum_{L=Z}^{m_0} P_C^i(\lambda_\ell^*) \quad (2.5.6)$$

Note that, by having all the probabilities  $P_A^i(\lambda_\ell^*), P_R^i(\lambda_\ell^*), P_C^i(\lambda_\ell^*)$ , other quantities of interest may also be calculated (e.g. variance of DSN, median of DSN, percentile of DSN, etc.).

This entire process has given a single point on the OC and ASN curves. To obtain the next point on the OC and ASN curves the density  $f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1})$  must again be obtained from equation (2.5.1) with  $\lambda = \lambda_{\ell+1}^*$ . The process of obtaining the density,  $f_i(W_i, Q_i, R_i)$ , and the probabilities  $P_A^i(\lambda_{\ell+1}^*)$ ,  $P_R^i(\lambda_{\ell+1}^*)$ ,  $P_C^i(\lambda_{\ell+1}^*)$ , must then be iterated for all stages  $i = n_1+1, \dots, m_0$ .

The Direct Method for  $K = 2$  SANOVA has been summarized in flowchart format as shown in Figure 13.

FIGURE 12

For any given stage,  $n$ : with regions  $V_A$  and  $V_R$ , the density of the point ( $W_n = a$ ,  $Q_n = b$ ,  $R_n = c$ ) is found by integrating the density of equation (2.3.5) as shown in equation (2.3.8). The integration limits  $U_U$ ,  $U_L$ ,  $Z_U$ ,  $Z_L$  may be obtained from the following flowchart.

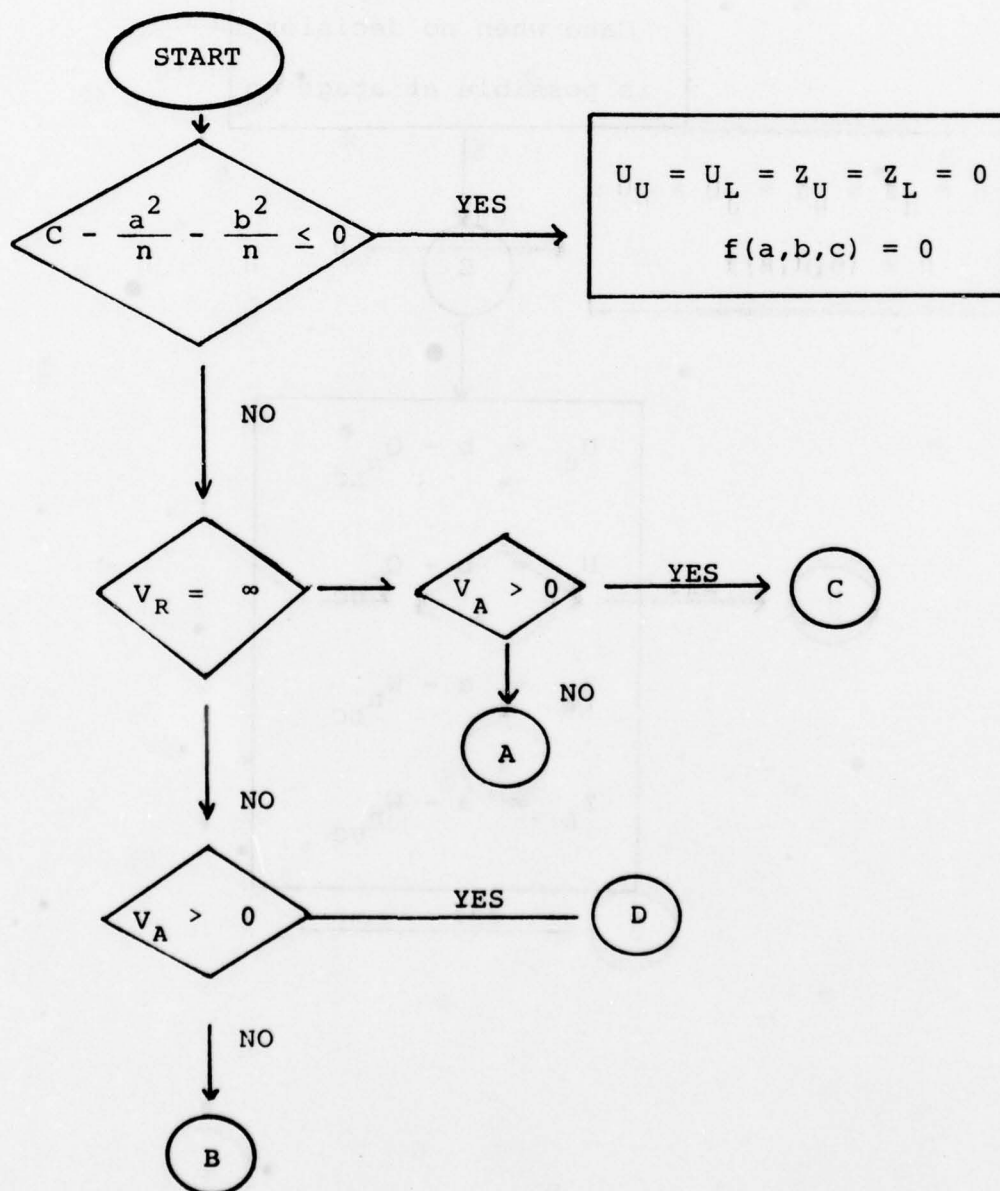


FIGURE 12 (continued)

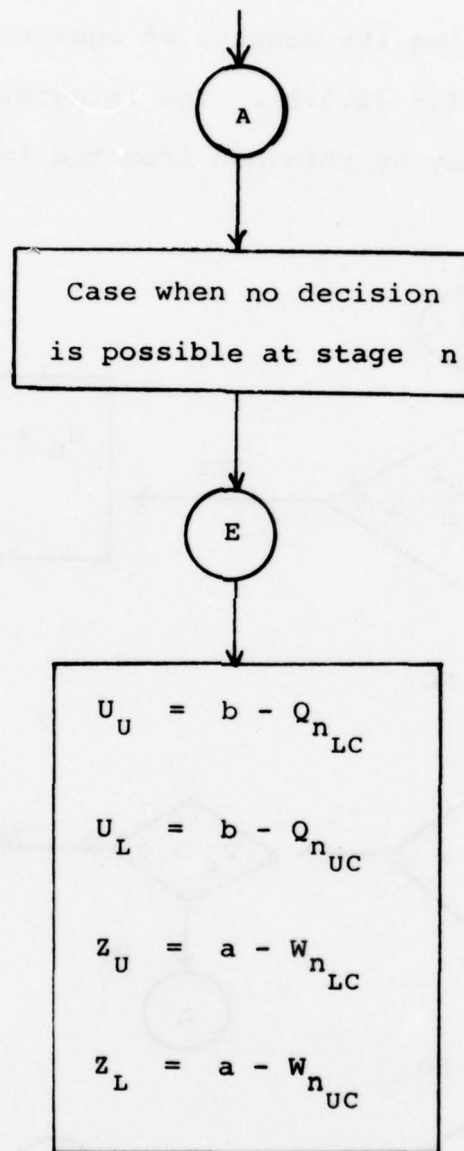


FIGURE 12 (continued)

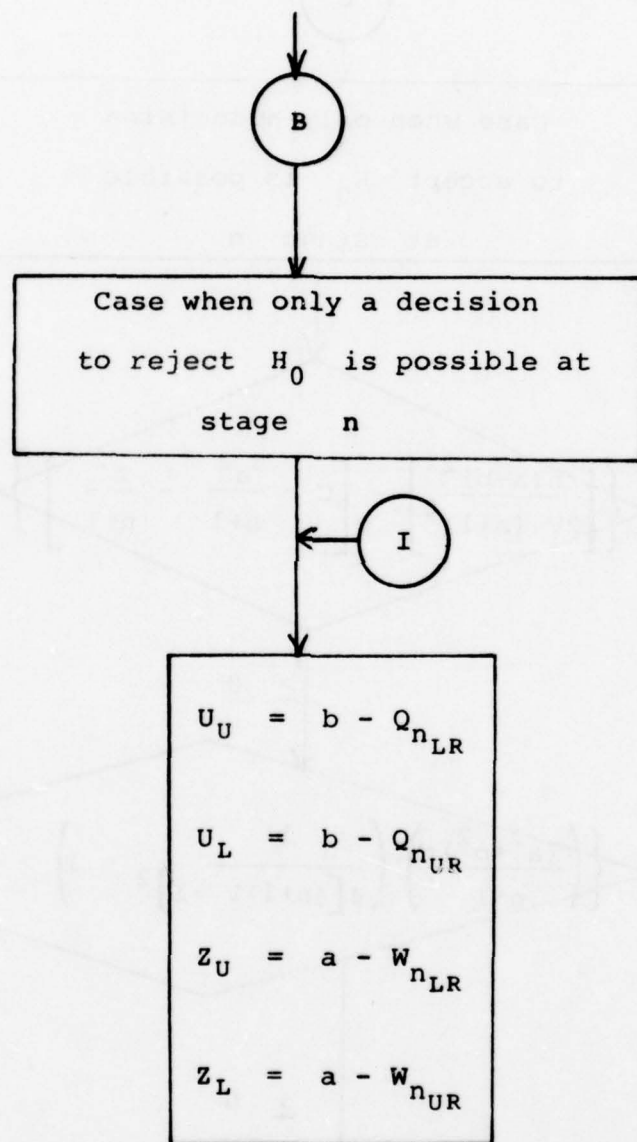


FIGURE 12 (Continued)

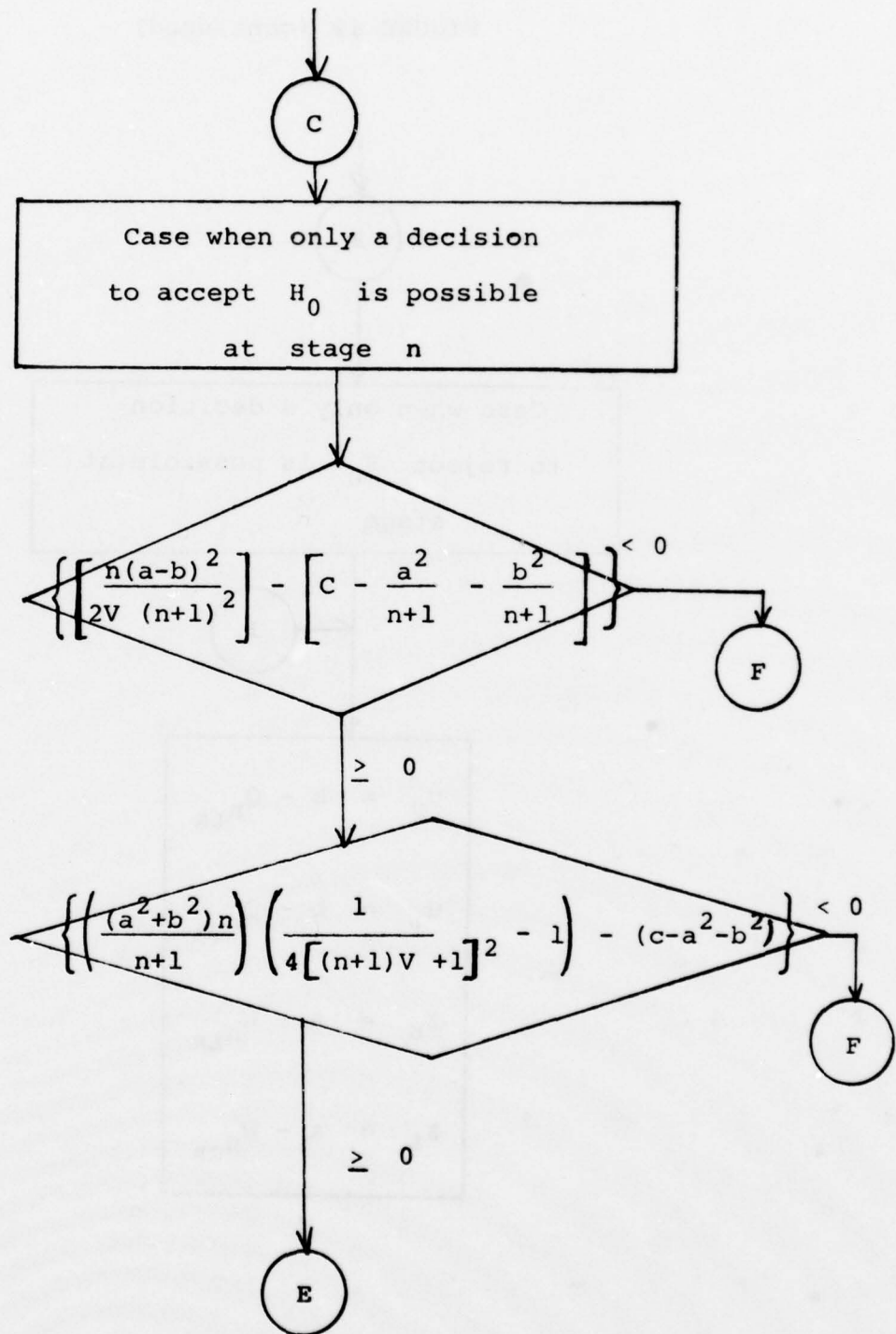


FIGURE 12 (Continued)



The integral must be broken  
up into at most 4 pieces  
as given in equation (2.3.25).

The number of pieces will depend  
upon the sign of  $(a+B)^2 - 2(1+\frac{1}{n})(a^2+b^2-c)$

The integration limits for each  
piece are given by:

<u>Piece</u>	<u>U Limits</u>	<u>Z Limits</u>
1	$U_U = b - Q_{n_{LC}}$ $U_L = b - Q_{n_{LA}}$	$Z_U = a - W_{n_{LC}}$ $Z_L = a - W_{n_{UC}}$
2	$U_U = b - Q_{n_{UA}}$ $U_L = b - Q_{n_{UC}}$	$Z_U = a - W_{n_{LC}}$ $Z_L = a - W_{n_{UC}}$
3	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{UA}}$ $Z_L = a - W_{n_{UC}}$
4	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{LC}}$ $Z_L = a - W_{n_{LA}}$

FIGURE 12 (Continued)

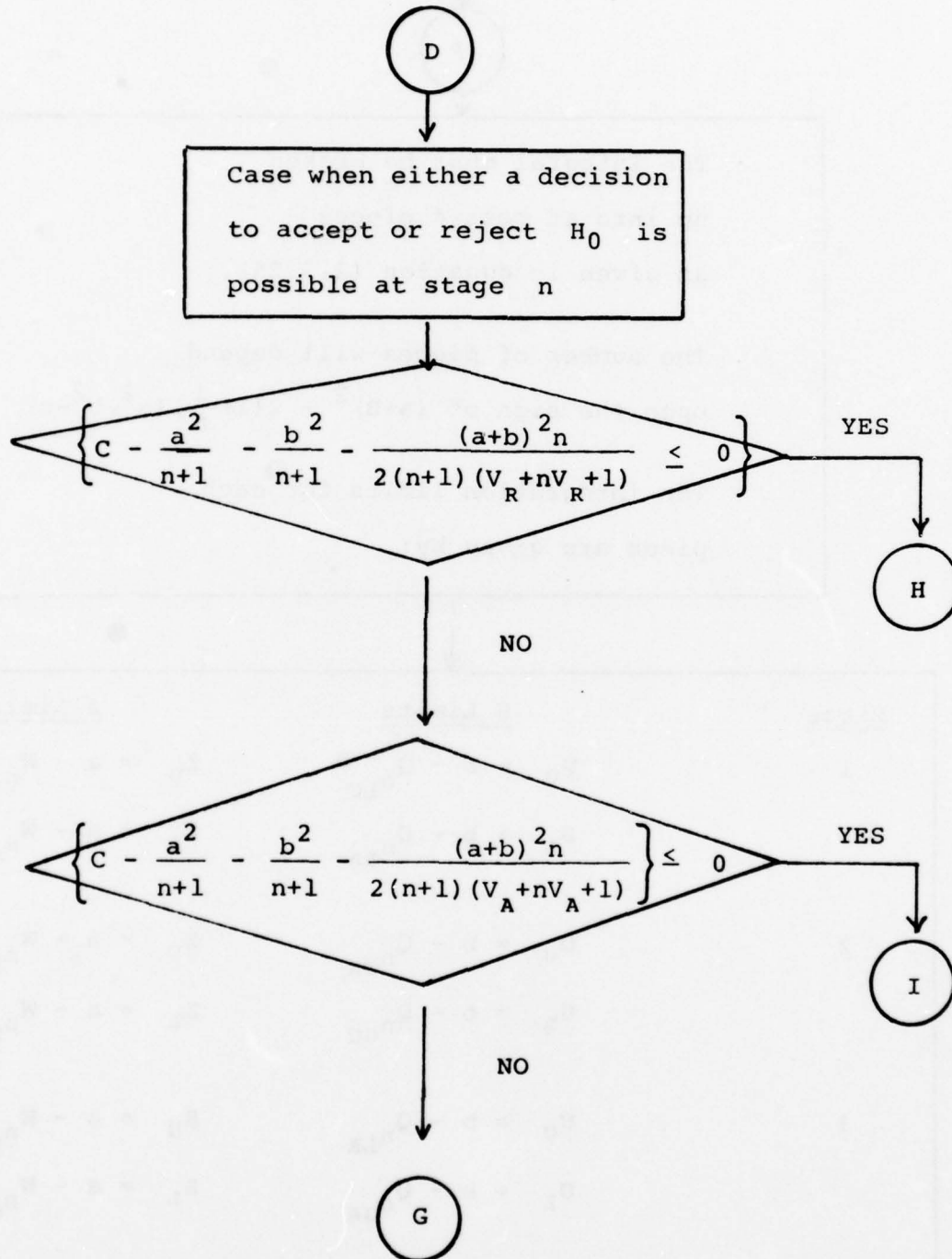


FIGURE 12 (Continued)

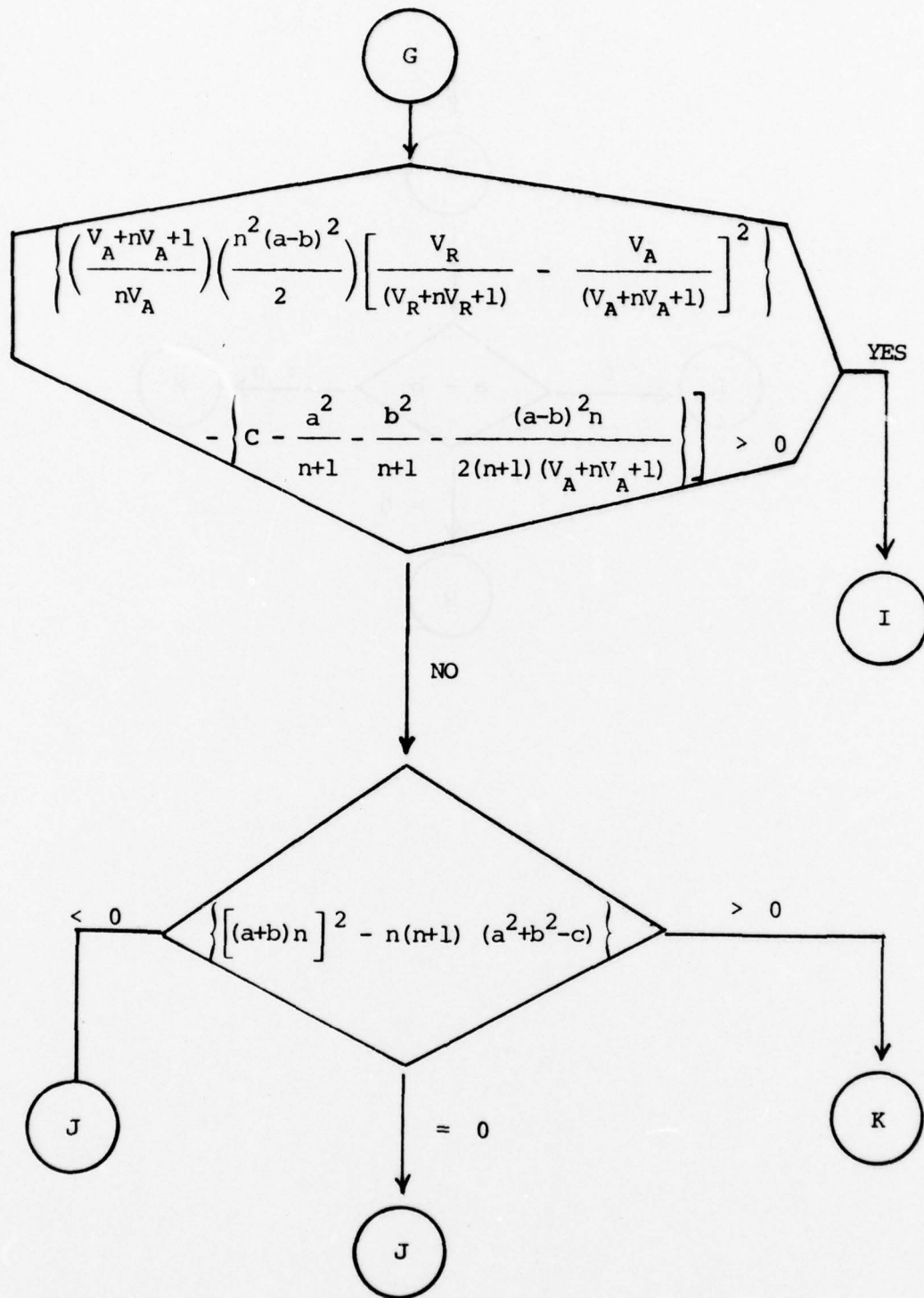


FIGURE 12 (Continued)

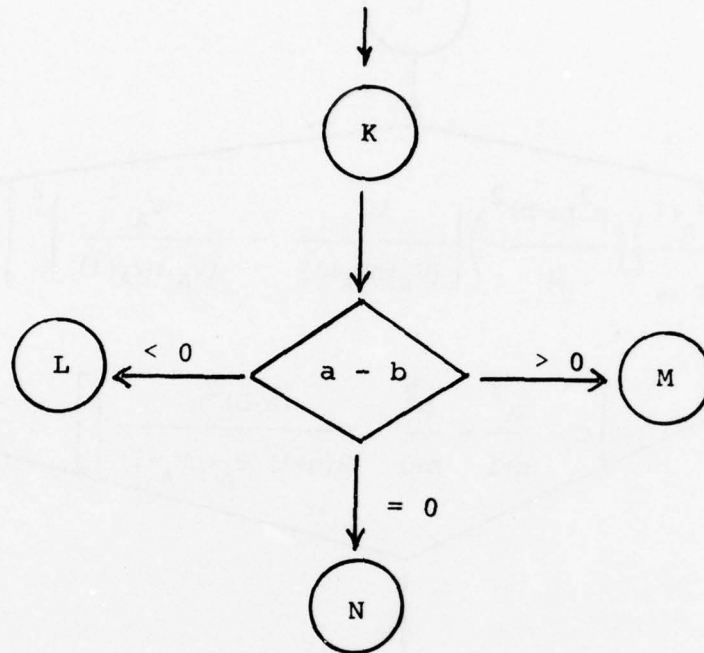


FIGURE 12 (Continued)

J



The integral must be broken up  
into at most four pieces.

One or two of the pieces may  
be null.

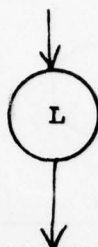
The integration regions for each  
piece are given as:



N

<u>Piece</u>	<u>U Limits</u>	<u>Z Limits</u>
1	$U_U = b - Q_{n_{LR}}$ $U_L = b - Q_{n_{LA}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{UR}}$
2	$U_U = b - Q_{n_{UA}}$ $U_L = b - Q_{n_{UR}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{UR}}$
3	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{UA}}$ $Z_L = a - W_{n_{UR}}$
4	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{LA}}$

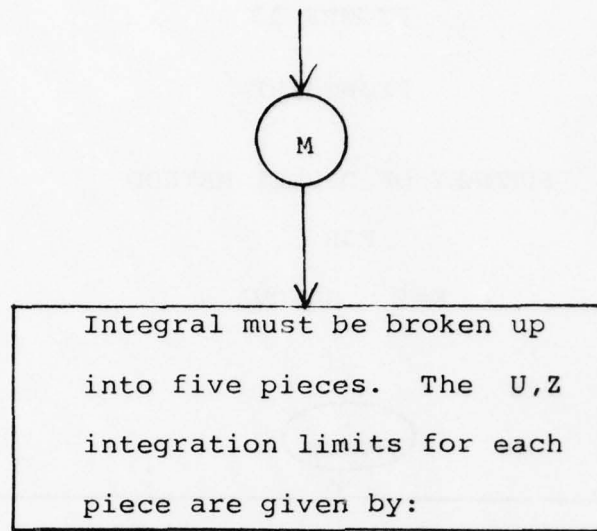
FIGURE 12 (Continued)



Integral must be broken up into five pieces. The U,Z integration regions for each piece are as follows:

<u>Piece #</u>	<u>U Limits</u>	<u>Z Limits</u>
1	$U_U = b - Q_{n_{LR}}$ $U_L = b - Q_{n_{LA}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{UR}}$
2	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{LA}}$
3	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{LI}}$	$Z_U = a - W_{n_{UA}}$ $Z_L = a - W_{n_{UR}}$
4	$U_U = b - Q_{n_{UI}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{UA}}$ $Z_L = a - W_{n_{UR}}$
5	$U_U = b - Q_{n_{UA}}$ $U_L = b - Q_{n_{UR}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{UR}}$

FIGURE 12 (Continued)



<u>Piece #</u>	<u>U Limits</u>	<u>Z Limits</u>
1	$U_U = b - Q_{n_{LR}}$ $U_L = b - Q_{n_{LA}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{UR}}$
2	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{UA}}$ $Z_L = a - W_{n_{UR}}$
3	$U_U = b - Q_{n_{LA}}$ $U_L = b - Q_{n_{LI}}$	$Z_U = a - W_{n_{LR}}$ $Z_L = a - W_{n_{LA}}$
4	$U_U = b - Q_{n_{UI}}$ $U_L = b - Q_{n_{UA}}$	$Z_U = a - W_{n_{LR}}$ $Z = a - W_{n_{LA}}$
5	$U_U = b - Q_{n_{UA}}$ $U_L = b - Q_{n_{UR}}$	$Z_U = a - W_{n_{LR}}$ $Z_U = a - W_{n_{UR}}$

FIGURE 13

## FLOWCHART

## SUMMARY OF DIRECT METHOD

FOR

K=2    SANOVA

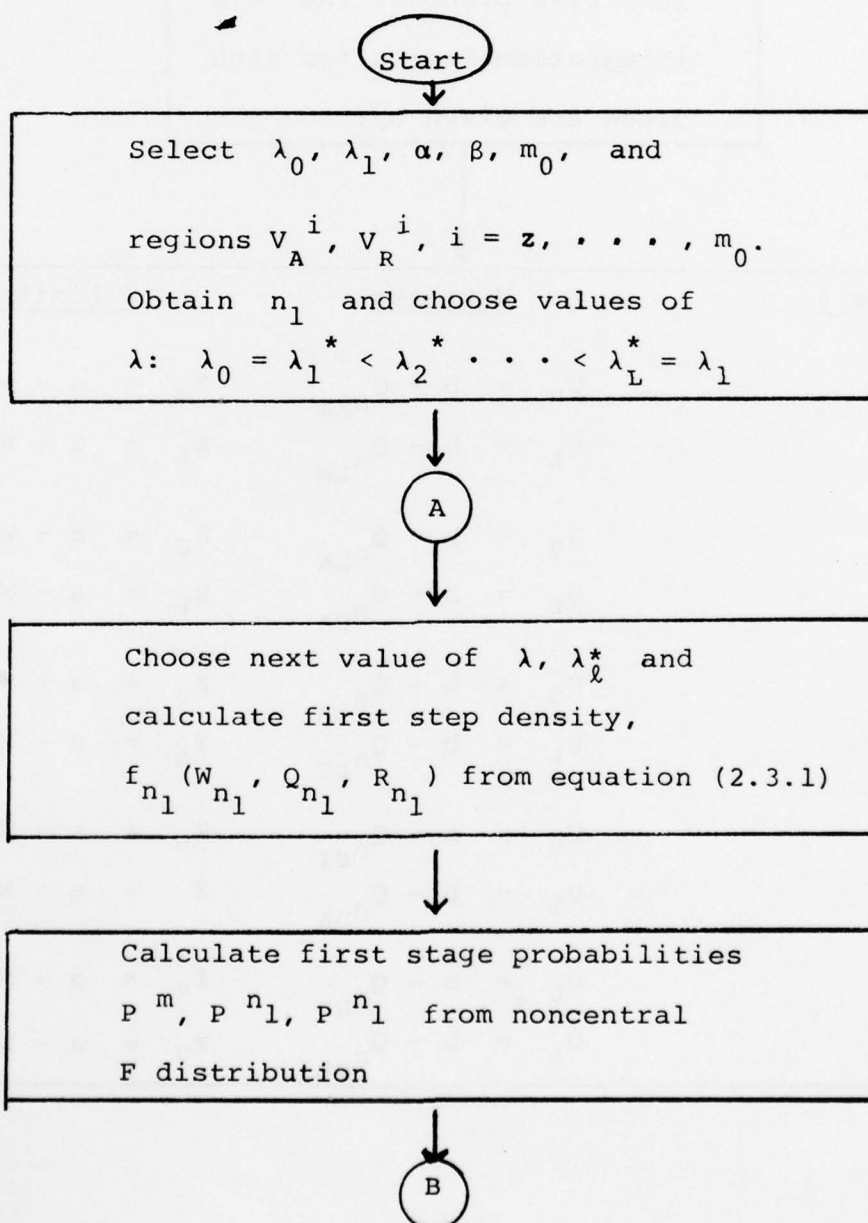


FIGURE 13 (Continued)

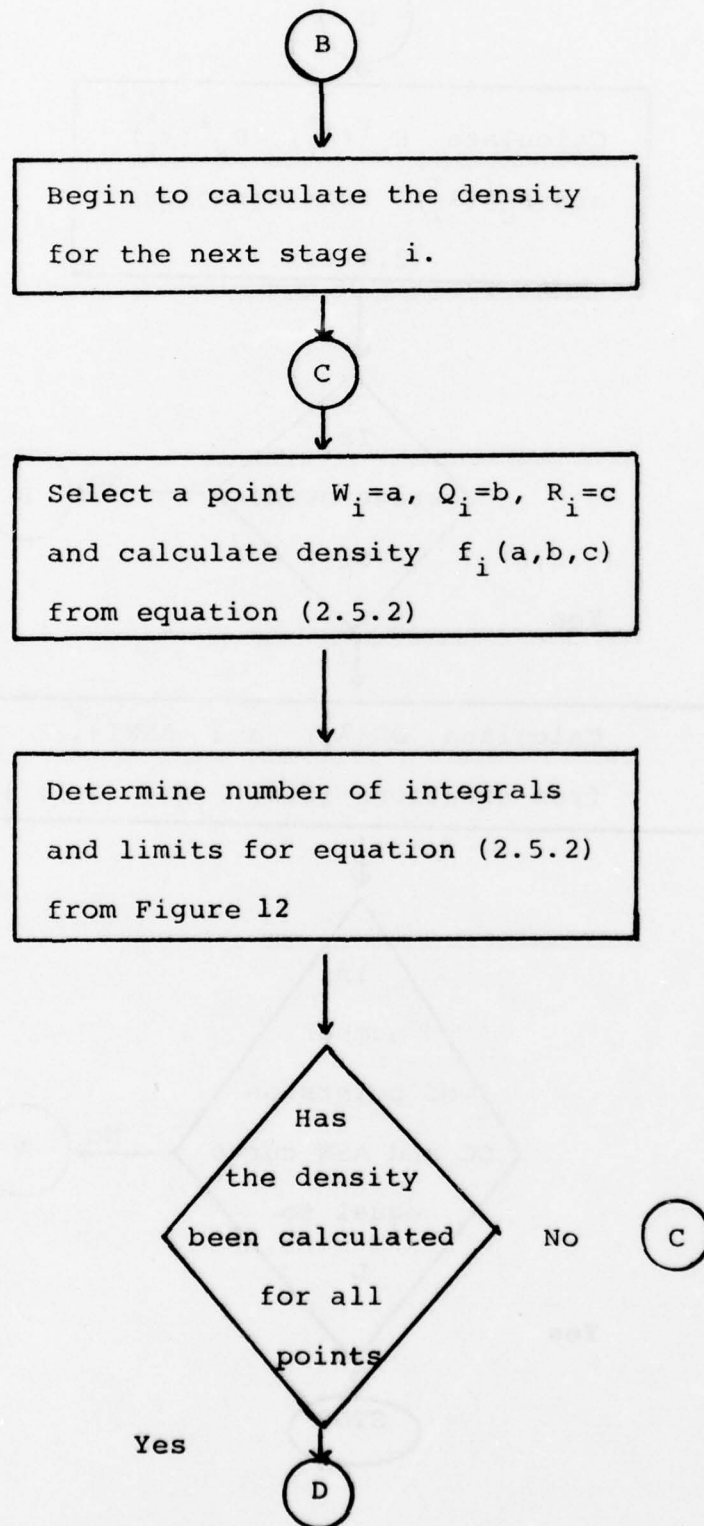
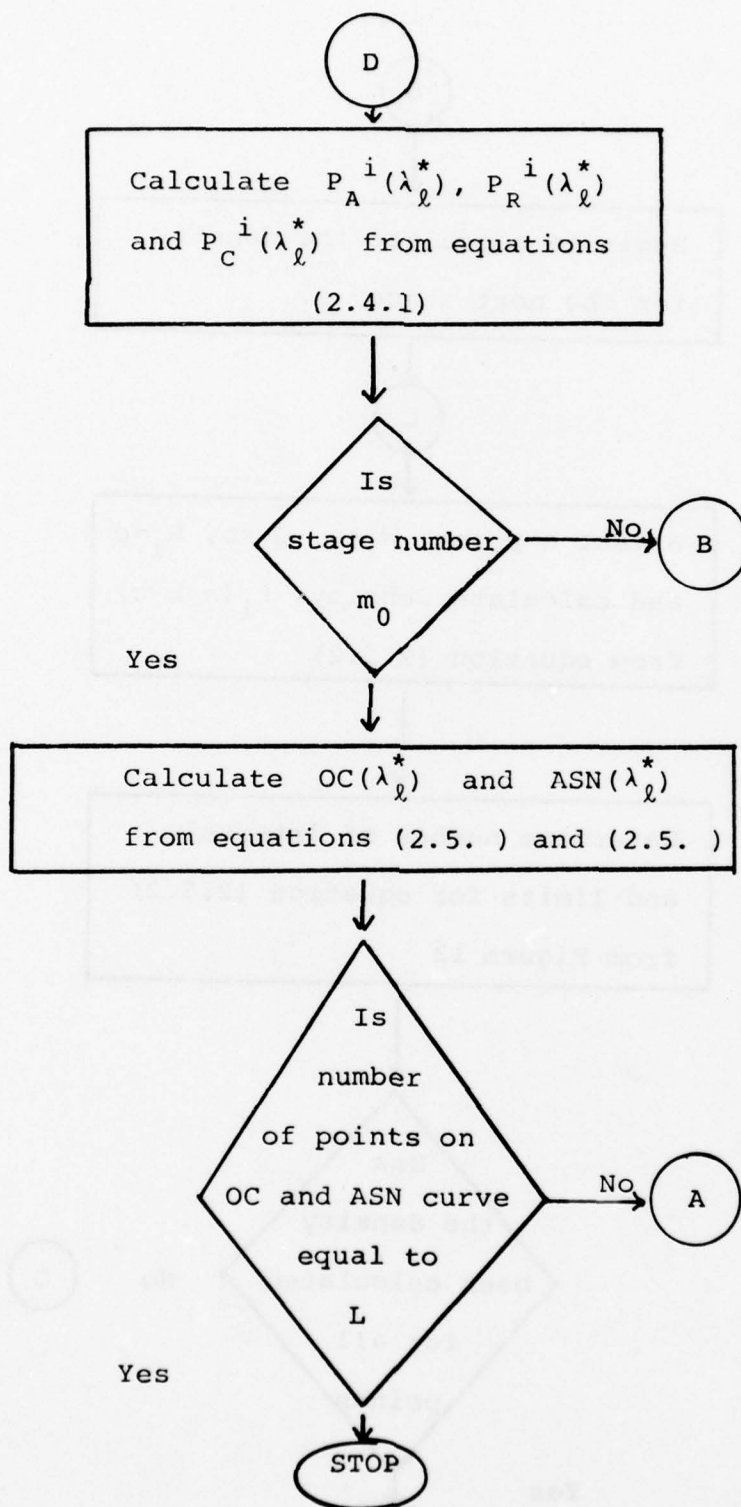


FIGURE 13 (Continued)



## 2.6 Numerical Methods

The previous sections have given a detailed description and derivation for obtaining the properties of a  $K=2$  SANOVA test by the direct method.

In summary the procedure requires the following steps:

1. For a given value of  $\lambda = \lambda^*$ , determine the joint density at the first stage at which a decision can be made;  $f_{n_1}(W_{n_1}, Q_{n_1}, R_{n_1})$ .
2. Calculate the joint density  $f_{n_1+1}(W_{n_1+1}, Q_{n_1+1}, R_{n_1+1})$ , for all values of  $W_{n_1+1}, Q_{n_1+1}, R_{n_1+1}$ . This requires:
  - a. Forming the five dimensional joint density  $f_{n_1}^P(W_{n_1}, Q_{n_1}, R_{n_1}, X_{1n_2}, X_{2n_2})$  as given in equation (2.5.2).
  - b. Performing the bivariate integration on this five dimensional joint density given in equation (2.5.3).
3. Performing a trivariate integration of the density  $f_{n_1+1}(W_{n_1+1}, Q_{n_1+1}, R_{n_1+1})$  to obtain the probabilities of acceptance  $(P_A^{n_1+1})$ , rejection  $(P_R^{n_1+1})$ , and continuation  $(P_C^{n_1+1})$ .

4. Iterating steps 2 and 3 on the density  
 $f_i (W_i, Q_i, R_i)$  for all  $i = n_1+2, \dots, M_0$ .
5. Calculating the OC and ASN for  $\lambda = \lambda^*$ .
6. Repeating steps 1 through 5 for all values  
of  $\lambda^*$  of interest.

This section will discuss the practical evaluation of the integrals required in steps 2 and 3 of the above procedure.

These integrals will generally be very complicated expressions. For example, wherever no decision can be made, the  $U, Z$  region of integration required for step 2 consists of all  $U, Z$  contained inside the circle given in equation (2.5.4). The actual  $U, Z$  integration limits required are given in equations (2.3.6) and (2.3.7). This amounts to integrating a five dimensional joint density composed of the product of a  $\chi^2$  and four normal densities. This integration can be evaluated analytically, yielding the density given at the top of page 2-20. The cases which require integrating around ellipses (e.g., equations (2.3.12) - (2.3.14) ) or those that require breaking the integral up into several pieces (e.g., equations (2.3.25) - (2.3.28) ), generally can not be evaluated analytically.

One approach is to develop a numerical approximation to these bivariate integrals (e.g., series, partial fraction, or continued fraction expansions). Since the integration region required is dependent upon the point  $a, b, c$  (for a given set of regions), this approach would yield the following type of piecewise trivariate density for stage  $n_1+1$ :

$$f_{n_1+1}(W_{n_1+1}, Q_{n_1+1}, R_{n_1+1}) = \begin{cases} \text{Expression 1 all } W_{n_1+1}, Q_{n_1+1}, R_{n_1+1} \in R_1 \\ \vdots \\ \text{Expression K all } W_{n_1+1}, Q_{n_1+1}, R_{n_1+1} \in R_K \end{cases}$$

An analytic expression for the integral required in step 3 with this type of piecewise trivariate density function would probably not exist. Also, if one were to continue along these lines, the density at later stages;  $f_i(W_i, Q_i, R_i)$ ,  $i = n_1 + 2, \dots, m_0$ ; would become a piecewise function with an infeasible number of pieces.

An alternative method for evaluating these integrals is via numerical integration. The analytic density  $f_n(W_n, Q_n, R_n)$  may be represented by a discrete three dimensional grid of points;  $f_n(W_{n_i}, Q_{n_j}, R_{n_k})$ ,  $i = 1, \dots, N_W$ ,  $j = 1, \dots, N_Q$ ,  $k = 1, \dots, N_R$ ; so that for a

given point on this grid;  $W_{n_{l+1}} = a = W_{n_{i*}}$ ,

$Q_{n_{l+1}} = b = Q_{n_{j*}}$ ,  $R_{n_{l+1}} = c = R_{n_{k*}}$ ; the joint density

may be approximated by the following expression:

$$f_{n_{l+1}}(a,b,c) \approx \sum_m \sum_\ell \omega_{1\ell} \omega_{2m} f_{n_{l+1}}^P(a-z_\ell, b-u_m, c-z_\ell^2-u_m^2, z_\ell, u_m)$$

The quantities  $\omega_{1\ell}$ ,  $\omega_{2m}$  and  $z_\ell$ ,  $u_m$  are the required weights and coordinates of the integration scheme employed and depend upon the  $U$ ,  $Z$  region of integration.

Repeating this procedure for all  $a$ ,  $b$ ,  $c$  contained on this grid yields a new grid representing the density at stage  $n_{l+1}$ ,  $f_{n_{l+1}}(W_{n_i}, Q_{n_j}, R_{n_k})$ . From this new grid the probabilities  $P_A^{n_{l+1}}$ ,  $P_R^{n_{l+1}}$ ,  $P_C^{n_{l+1}}$  must be obtained. Obtaining these probabilities requires a trivariate integration which can also be done numerically. For example

$$P_A^{n_{l+1}} \approx \sum_m \sum_\ell \sum_p \omega_{1m} \omega_{2\ell} \omega_{3p} f_{n_{l+1}}(W_m, Q_\ell, R_p). \quad (2.6.2)$$

This new grid can again be manipulated to obtain the density at stage  $n_{l+2}$  and ultimately the probabilities  $P_A^{n_{l+2}}$ ,  $P_R^{n_{l+2}}$  and  $P_C^{n_{l+2}}$ . Repeating the procedure to obtain a new grid  $f(W_{n_i}, Q_{n_j}, R_{n_k})$  and  $P_A^n, P_R^n, P_C^n$  for all  $n = n_{l+2}, \dots, m_0$ , allows the calculation of a point on the ASN and OC curves.

In general, the density at any point not on the grid; say  $f_i (W_i^*, Q_i^*, R_i^*)$ ,  $i = n_1+2, \dots, M_0$ ; must be found by interpolation. Note that this could require the formidable task of interpolating in three dimensions. Thus, it would be desirable to use a grid scheme and integration rule that required a minimum amount of interpolation to evaluate equations (2.4.1) and (2.5.3).

First, consider the following grid scheme:

$$\begin{aligned} W_{n_i} &= \left[ W_S + (i-1)\alpha_i \right] h_W & i &= 1, \dots, N_W \\ Q_{n_j} &= \left[ Q_S + (j-1)\beta_j \right] h_Q & j &= 1, \dots, N_Q \\ R_{n_k} &= \left[ R_S + (k-1)\gamma_k \right] h_R & k &= 1, \dots, N_R \end{aligned} \quad (2.6.3).$$

The quantities  $\alpha_i, \beta_j, \gamma_k$  are all integers chosen such that:

$$\begin{aligned} W_{n_1} &< W_{n_2} < \dots < W_{nn_W} \\ Q_{n_1} &< Q_{n_2} < \dots < Q_{nn_Q} \\ R_{n_1} &< R_{n_2} < \dots < R_{nn_R} \end{aligned}$$

The choice of the quantities  $W_S, Q_S, R_S, h_W, h_Q$ , and  $h_R$  will be discussed later.

Many integration rules are available (Davis and Rabinowitz (1967)); but to avoid excessive amounts of interpolation a rule should be chosen which allows the majority of the points to be located on the grid.

For the integration given in (2.6.1) this requires that not only  $a - z_\ell$  and  $b - U_m$  be located on  $W_n, Q_n$  grid points, but also that  $c - z_\ell^2 - U_m^2$  be located on an  $R_n$  grid point. This can be guaranteed if the quantities  $h_W, h_Q$ , and  $h_R$  are chosen such that:

$$h_R = \Lambda_1 h_W^2 + \Lambda_2 h_Q^2$$

or

$$h_W^2 = \Lambda_3 h_R \quad \text{and} \quad h_Q^2 = \Lambda_4 h_R, \quad (2.6.4)$$

where

$\Lambda_1, \Lambda_2, \Lambda_3$ , and  $\Lambda_4$  are integers.

Using this type of grid and the trapezoid integration rule, equation (2.6.1) becomes:

$$f_i(a,b,c) \simeq \sum_{m=0}^{n_Q} \sum_{\ell=0}^{n_W} \omega_{1\ell} \omega_{2m} f_{i-1}^P(a-z_\ell, b-U_m, c-z_\ell^2-U_m^2, z_\ell, U_m) \quad (2.6.5)$$

where the coordinates  $z_\ell$  and  $U_m$  are given by the following scheme:

$$z_0 = z_L$$

$$z_S = \left[ z_L / h_W \right]$$

$$z_F = \left[ z_U / h_W \right]$$

$$U_0 = U_L$$

$$U_S = \left[ U_L / h_Q \right]$$

$$U_F = \left[ U_U / h_Q \right]$$

$$N_W - 1 = Z_F - Z_S + 1$$

$$N_Q - 1 = U_F - U_S + 1$$

$$Z_{\ell} - 1 = Z_S + (\ell - 1)h$$

$$\ell = 1, \dots, N_W - 2$$

$$Z_{n_W - 1} = Z_F$$

$$Z_{n_W} = Z_U$$

$$U_m = U_S + (m - 1)h_W$$

$$m = 1, \dots, N - 2$$

(2.6.6)

$$U_{n_Q - 1} = U_F$$

$$U_{n_Q} = U_U$$

with

$$[X] \equiv \text{sign}(X) \cdot \{\text{greatest integer in } |X| \}.$$

The weights  $\omega_{1\ell}$  and  $\omega_{2m}$  are given by:

$$\omega_{10} = \frac{1}{2} |Z_L - Z_0|$$

$$\omega_{11} = \frac{1}{2} |Z_S - Z_0| + \frac{1}{2} h_W$$

$$\omega_{1\ell} = \frac{1}{2} h_W$$

$$\ell = 2, \dots, N_W - 2$$

$$\omega_{1\ell} = \frac{1}{2} h_W + \frac{1}{2} |Z_U - Z_F|$$

$$\ell = N_W - 1$$

$$\omega_{1\ell} = \frac{1}{2} |Z_U - Z_F|$$

$$\ell = N_W$$

and

$$\omega_{20} = \frac{1}{2} |(U_L - U_S)|$$

$$\omega_{21} = \frac{1}{2} |(U_S - U_0)| + \frac{1}{2} h_W$$

$$\omega_{2m} = \frac{1}{2} h_Q \quad m = 2, \dots, N_Q - 2$$

$$\omega_{2m} = \frac{1}{2} h_Q + \frac{1}{2} |(U_U - U_F)| \quad m = N_W - 1$$

$$\omega_{2m} = \frac{1}{2} |(U_U - U_F)| \quad m = N_W$$

With this grid structure and integration scheme the density of some points may still need to be obtained by interpolation. Any values of  $z^*$ ,  $U^*$  that result in the point  $(a-z^*, b-U^*, c-z^{*2}-U^{*2})$  not to be on a  $(W, Q, R)$  grid point will require that the five dimensional density  $f_i^P(\quad)$  be obtained by interpolation. For example, there is no guarantee that the endpoints  $z_L$ ,  $z_U$ ,  $U_L$  and  $U_U$  will lie on a grid point. However, in such cases, the task of interpolation may be simplified by considering the form of the five dimensional density  $f_i^P(\quad)$ .

As shown in equation (2.5.2) the five dimensional joint density is given by:

$$\begin{aligned} f_i^P(a-z, b-U, c-z^2-U^2, z, U) \\ = f_{i-1}(a-z, b-U, c-z^2-U^2) \cdot \phi(z) \cdot \phi(U - \sqrt{\lambda_\ell^*}). \end{aligned}$$

Whenever interpolation is required to evaluate  $f_i^P(\quad)$ , it need only be performed in two or three dimensions on the

density  $f_{i-1}(\quad)$ , since both  $\phi$ 's can be calculated exactly for any value of  $U$  and  $Z$ .

In other words, when interpolation is required

$$f_i^P(a-Z, b-U, c-Z^2-U^2, Z, U) \approx E^* \phi(Z) \cdot \phi\left(U - \sqrt{\lambda_\ell^*}\right)$$

where  $E^*$  is the interpolated value of the density  $f_{i-1}(a-Z, b-U, c-Z^2-U^2)$ .

For a given point  $a^*, b^*, c^*$  not on a  $(W, Q, R)$  grid point at stage  $i-1$ , the density  $f_{i-1}(a^*, b^*, d^*)$  may be approximated by trivariate linear interpolation. This involves the following approximation:

$$f_{i-1}(a^*, b^*, c^*) = P^* \approx \sum_{\ell=1}^2 \sum_{j=1}^2 \sum_{k=1}^2 f_{i-1}(a_\ell, b, c) \alpha_\ell \beta_j \gamma_k \quad (2.6.8)$$

where

$$a_1 = a^*/h_w + 1 \text{ (sign } (a^*))$$

and

$$a_2 = a^*/h_w$$

and

$$\alpha_1 = \frac{a^* - a_2}{a_1 - a_2}, \quad \alpha_2 = \frac{a^* - a_1}{a_2 - a_1}$$

and analogous expressions for the other quantities.

This should give fairly good approximations for small values of  $h_w$ ,  $h_Q$ , and  $h_R$ . For large values of these quantities the result could be meaningless (i.e.,  $f_i(a^*, b^*, c^*) < 0$  or  $f_i(a^*, b^*, c^*) > 1$ ), and should be modified in such cases. The modifications are of the following form:

$$f_i(a^*, b^*, c^*) = \begin{cases} P^* & \text{if } 0 \leq P^* \leq 1 \\ 0 & \text{if } P^* < 0 \\ \max(f_i(a_\ell, b_j, c_k)) & \text{if } P^* \geq 1 \end{cases}$$

By using the trapezoid rule and trivariate interpolation, the density  $f_i(a, b, c)$  may be calculated. This must be repeated for all  $a, b, c$  contained on the grid. This will result in a new grid representing the density at stage  $i$ . From this new grid, the probabilities  $P_h^i$ ,  $P_R^i$ , and  $P_C^i$  must be calculated. These probabilities can also be calculated with a trapezoid rule integration scheme as given in (2.6.2).

In practice the following quantities must be specified:

- (1) The grid sizes  $h_W, h_Q, h_R$ .
- (2) The end points of the grid:  $W_S, W_F, Q_S, Q_F, R_S, R_F$ .

As in most numerical problems, the best choice of the grid sizes will depend upon the particular problem (i.e.,  $V_A^i, V_R^i$ , and  $m_0$ ). One approach to this problem is to start the procedure with a coarse grid and obtain answers; the procedure may then be redone using a finer grid and new answers obtained. This process is iterated until the results converge to answers accurate to the desired number of digits. One should note that the number of calculations required for each additional iteration increases exponentially. For example, suppose a grid is constructed, using grid sizes  $h_W, h_Q$ , and  $h_R = h_W^2 + h_Q^2$  and  $\alpha_i, \beta_j, \gamma_k$  of (2.6.3) all equal to unity. Halving the  $h_W$  and  $h_Q$  grid sizes will result in an eight-fold increase in the total number of points on the grid. The density for each of these points must be calculated for each stage, which requires a bivariate integration for each point at each stage.

The grid end points must be chosen so as to exclude only a minute fraction of the density for all stages:  
 $i = n_1, \dots, m_0$ . This amounts to choosing the quantities

$W_S, W_F, Q_S, Q_F$  and  $R_S, R_F$  such that all points,  $W_n, Q_n, R_n$ , on the grid lie within these ranges, i.e.,

$$W_S \leq W_b \leq W_F$$

$$Q_S \leq Q_n \leq Q_F$$

$$R_S \leq R_n \leq R_F .$$

In most cases, the size of the required grid (i.e.,  $W_S, W_F, Q_S, Q_F, R_S$  and  $R_F$ ) is directly proportional to the value of  $m_0$ .

Since  $W_{n_1}$  ( $n_1$  being the first stage at which a decision can be made) is distributed normally with mean zero and standard deviation  $\sqrt{n_1}$ , a  $W_n$  range of the following type:

$$\begin{aligned} W_S &= -6 \left[ \sqrt{n_1} / h_w \right] * h_w \\ W_F &= 6 \left[ \sqrt{n_1} / h_w \right] * h_w , \text{ where } \left[ \right] \equiv \text{greatest integer} \end{aligned}$$

should be sufficient for the grid at stage  $n_1$ . However, if the regions were such that no decision could be made until stage  $m_0$ ,  $W_{m_0} \sim N(0, \sqrt{m_0})$ . Thus in order to insure that the grid is large enough, the following range should be used:

$$\begin{aligned} W_S &= -6 \left[ \sqrt{m_0} / h_w \right] * h_w \\ W_F &= +6 \left[ \sqrt{m_0} / h_w \right] * h_w \end{aligned}$$

(2.6.9).

Employing similar logic to the  $Q$  dimension yields the following range:

$$\begin{aligned} Q_S &= \min \left\{ \left[ (\sqrt{n_1 \lambda} - 6\sqrt{n_1}) / h_Q \right] * h_Q, \left[ (\sqrt{m_0 \lambda} - 6\sqrt{m_0}) / h_Q \right] * h_Q \right\} \\ Q_F &= \max \left\{ \left[ (\sqrt{n_1 \lambda} + 6\sqrt{n_1}) / h_Q \right] * h_Q, \left[ (\sqrt{m_0 \lambda} + 6\sqrt{m_0}) / h_Q \right] * h_Q \right\} \\ \text{where } \left[ \right] &\equiv \text{greatest integer.} \end{aligned} \quad (2.6.10).$$

Since  $R$  must always be greater than the quantity  $1/n(W^2 + Q^2)$ , the  $R$  points for which

$$R_{m_0} < \frac{1}{m_0} (W_0^2 + Q_{m_0}^2),$$

need not be contained on the grid. Thus the range of  $R$  will depend upon the values of  $W$  and  $Q$ , and the overall grid structure becomes that of a cone as shown in Figure 14. An  $R$  range sufficient for the density  $f_i(W_i, Q_i, R_i)$  for all  $i$ , is given by:

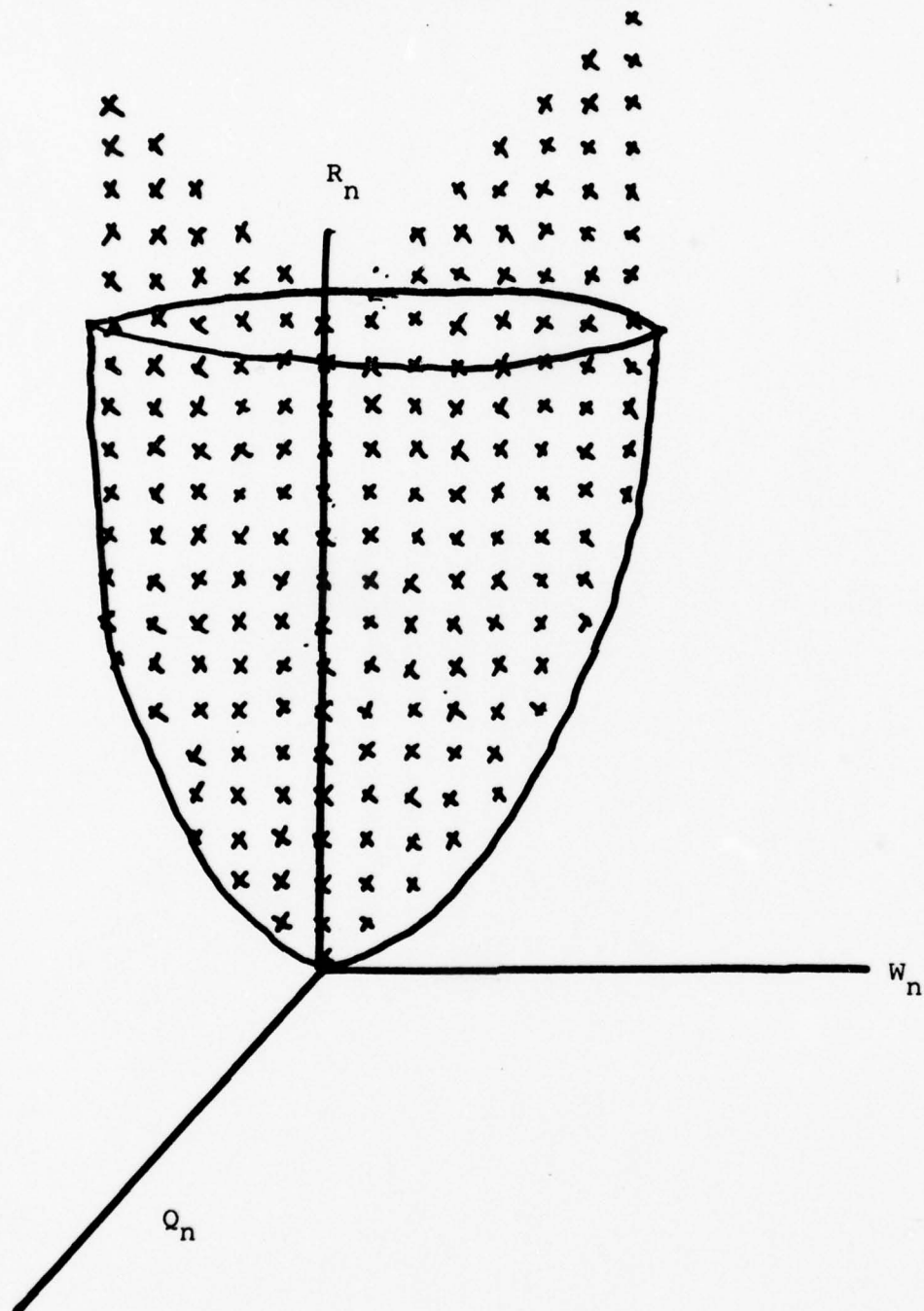
$$\begin{aligned} R_S &= \left\lceil \frac{1}{m_0} (W_{n_K}^2 + Q_{n_j}^2) / h_R \right\rceil * h_R \\ R_F &= R_S + \left\lceil \chi_{99.9}^2 (2m_0 - 2) / h_R \right\rceil * h_R \end{aligned} \quad (2.6.11).$$

where  $\left[ \right] \equiv$  greatest integer.

A grid of this form and size will allow for sufficient accuracy in the calculation of the OC and ASN curves.

In conclusion, this section has presented a procedure for implementing the theory of the previous sections.

FIGURE 14  
STRUCTURE OF NUMERICAL GRID  
FOR DIRECT METHOD IMPLEMENTATION



Since the density  $f_i(W_i, Q_i, R_i)$  can not be expressed in a closed form for  $i > n_1$ , this section has discussed a numerical procedure which allows the implementation of the theory. The numerical procedure consists of:

1. Representing the density  $f_i(W_i, Q_i, R_i)$  by a discrete 3-dimensional grid of points. The grid is shown in Figure 14 and is described mathematically by equations (2.6.3). The quantities  $R_S, R_F, Q_S, Q_F, W_S, W_F, h_R, h_W, h_a$  are given by equations (2.6.4) and (2.6.9) - (2.6.11).
2. "Carrying" this grid from stage to stage. The grid at stage  $i-1$  is used to calculate a new grid for stage  $i$ , which represents the density  $f_i(W_i, Q_i, R_i)$ . To calculate the density of any point on this grid at stage  $i$  requires performing the bivariate integration of equation (2.5.3). However, the integration is now performed numerically. When the trapezoid integration rule is used, the calculation is given by equations (2.6.5) - (2.6.7).
3. After the density of all points at stage  $i$  has been calculated, the grid is then again numerically integrated to obtain  $P_A^i, P_R^i, P_C^i$ . This is calculated by the procedure shown in equation (2.6.2).

Since the density at stage  $i-1$  is known only at the points on the grid, the density at points not on the grid must be obtained by interpolation. This can be done by three dimensional linear interpolation as given in equation (2.6.8).

The methods discussed in this section are only feasible if performed on an electronic computer. Appendix C discusses a program developed to calculate several points on the OC and ASN curves for any  $k=2$  SANOVA test.

## 2.7 CONCLUSION

This chapter of the thesis has derived a procedure for obtaining the OC and ASN curves of a  $k=2$  SANOVA test. The procedure is the first to yield exact results.

Section (2.3) involved the theoretical derivation of the procedure, which has been summarized in Figures 12 and 15 of Section (2.5). Also, Section (2.6) contained a discussion of a numerical approach for implementing the procedure. Appendix C contains a computer program which calculates the OC and ASN curves via the methods discussed in this chapter.

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## APPENDIX A

## POWER CALCULATIONS FOR A FIXED SAMPLE ANOVA TEST

As shown in Section (1.1) of the thesis, the fixed sample test utilizes the statistic  $F_{cal}$ , where

$$F_{cal} = \frac{\sum_{i=1}^K n_i (\bar{X}_i - \bar{\bar{X}})^2 / (K - 1)}{\sum_{i=1}^K \sum_{j=1}^{n_i} (X_{ij} - \bar{X}_i)^2 / (N - K)}$$

with

$$\begin{aligned} N &= \sum_{i=1}^K n_i \\ \bar{X}_i &= n_i^{-1} \sum_{j=1}^{n_i} X_{ij} \\ \bar{\bar{X}} &= N^{-1} \sum_{i=1}^K \sum_{j=1}^{n_i} X_{ij} \end{aligned}$$

For a test of  $K$  means with  $n_i = n$  observations from each population

$$F_{cal} \sim F_{K-1, K(n-1)}(n\lambda)$$

where

$$\lambda = \frac{\sum_{i=1}^K (\mu_i - \bar{\mu})^2}{\sigma^2}$$

$$\bar{\mu} = \sum_{i=1}^K \mu_i / K$$

and  $F_{K-1, K(n-1)}(n\lambda)$  is a noncentral  $F$  variate as defined in Section (1.1).

The ANOVA test is usually a test of the following hypotheses:

$$H_0: \lambda = 0 \quad \text{vs.} \quad H_1: \lambda \geq \lambda'$$

The decision criterion of the test is as follows:

$$(1) \text{ Accept } H_0 \text{ if } F_{\text{CAL}} < F_{K-1, K(n-1), \alpha}^* = \alpha.$$

The quantity  $\alpha$  corresponds to the acceptable probability of a Type-I error.

The choice of any two of the three quantities ( $\beta$  (magnitude of the Type-II error),  $n$ ,  $\lambda'$ ) completely determines the third.

The OC curve of the test is in terms of the parameter  $\lambda$ , and is defined as:

$$\begin{aligned} OC(\lambda^*) &= \Pr(\text{accepting } H_0 | \lambda = \lambda^*) \\ &= \Pr(F_{\text{CAL}} < F_{K-1, K(n-1), \alpha}^* | \lambda = \lambda^*) \\ &= \Pr(F_{\text{CAL}} < F_{K-1, K(n-1), \alpha}^* | F_{\text{CAL}} \sim F_{K-1, K(n-1)}(n\lambda^*)) \\ &= \int_0^{F_{K-1, K(n-1), \alpha}^*} f(F_{K-1, K(n-1)}(n\lambda^*)) dF_{K-1, K(n-1)}(n\lambda^*) \end{aligned}$$

where  $f(F_{K-1, K(n-1)}(n\lambda^*))$  is the density of a noncentral F variate with  $K-1, K(n-1)$  degrees of freedom and noncentral parameter  $n\lambda^*$ .

In order to calculate this integral the noncentral F distribution must be integrated. This integration can be expressed in terms of an infinite series of multiples of incomplete beta function ratios in the following manner:

$$OC(\lambda^*) = \sum_{j=0}^{\infty} \left( \frac{[\frac{1}{2}n\lambda^*]^j}{j!} e^{-\frac{1}{2}n\lambda^*} \right) I_g(\frac{1}{2}(K-1)+j, \frac{1}{2}K(n-1))$$

$$\text{where } g = \frac{(K-1)F_{K-1, K(n-1), \alpha}^*}{\left[ K(n-1) + (K-1)F_{K-1, K(n-1), \alpha}^* \right]} \quad (A.1)$$

and

$$I_x(a,b) = \frac{\Gamma(a+b)}{\Gamma(a)\Gamma(b)} \int_0^x t^{a-1}(1-t)^{b-1} dt$$

the incomplete beta function.

Thus  $OC(\lambda^*)$  may be calculated by summing terms in the series until the magnitude of a term is less than or equal to some  $\epsilon$ .

The incomplete beta function cannot be evaluated analytically, so must be done numerically. One method is that of continued fractions. The incomplete beta function's continued fraction expansion was obtained by Aroian (1941) and is given in Abramowitz and Stegun (1969).

An approximation to the cumulative distribution function of the noncentral  $F$  distribution was given by Tiku (1966). His approximation consists of fitting the distribution of  $F_{v_1, v_2}(\lambda)$  by that of  $(b + cF_{v_1', v_2'})$ ; choosing  $b$ ,  $c$ , and  $v_1'$  so as to make the first three moments agree. The values which do this are:

$$v_1' = \frac{1}{2} (v_2 - 2) \left[ \sqrt{\frac{H^2}{H^2 - 4K^3}} - 1 \right]$$

(A.2)

$$c = (v_1'/v_1) (2v_1 + v_2 - 2)^{-1} (H/K)$$

$$b = -v_2 (v_2 - 2)^{-1} (c - 1 - \lambda v_1^{-1})$$

where

$$H = 2(v_1 + \lambda)^3 + 3(v_1 + \lambda)(v_1 + 2\lambda)(v_2 - 2) + (v_1 + 3\lambda)(v_2 - 2)^3$$

and

$$K = (v_1 + \lambda)^2 + (v_2 - 2)(v_1 + 2\lambda)$$

so that

$$\begin{aligned} \Pr(F_{v_1, v_2}(\lambda) \leq f_0) &\approx \Pr(b + cF_{v_1, v_2} \leq f_0) \\ &= \Pr(F_{v_1, v_2} \leq \frac{f_0 - b}{c}) \end{aligned}$$

(A.3)

This approximation simply requires a method for evaluating the cumulative distribution function of a central  $F$  with  $v_1'$  and  $v_2$  degrees of freedom, which from above can be calculated as:

$$\Pr(F_{\hat{v}_1, v_2} \leq X) = I_{v_1 X / (v_2 + v_1 X)}^{(\frac{1}{2}v_1, \frac{1}{2}v_2)} . \quad (\text{A.4})$$

The computer program contained at the end of Appendix B uses this approximation to calculate the OC curve of a fixed sample test with specified values of  $\alpha$ ,  $\beta$  and  $\lambda'$ .

## APPENDIX B

## OBTAINING WALD REGIONS FOR A SANOVA TEST

As discussed in the thesis, a SANOVA test is conducted using the test statistic  $F_n$  of equation (1.2.1) or the simpler statistic  $V_n$ , where

$$V_n = \frac{(K-1)}{(N-K)} F_n .$$

At each stage this statistic is calculated and compared with the quantities  $V_A^n$  and  $V_R^n$ ; such that at any stage  $i$ :

- (1)  $H_0$  is accepted if  $V_i \leq V_A^i$
- (2)  $H_1$  is accepted if  $V_i \geq V_R^i$ .

The regions  $V_A^i, V_R^i$ , are usually chosen so that the Type-I and Type-II errors are approximately equal to the risks acceptable to the experimenter ( $\alpha$  and  $\beta$ ). The regions developed by Wald are the most commonly used.

For a given set of quantities  $\alpha, \beta, K, \lambda_0$ , and  $\lambda_1$ , Wald regions  $V_A^n$  and  $V_R^n$  are obtained as the solutions of the following equations:

$$\frac{\exp \left\{ -\frac{n}{2} (\lambda_1 - \lambda_0) \right\} M \left[ \frac{Kn-1}{2}, \frac{K-1}{2}, \frac{m\lambda_1 V_A^n}{2(1+V_A^n)} \right]}{M \left[ \frac{Kn-1}{2}, \frac{K-1}{2}, \frac{m\lambda_0 V_A^n}{2(1+V_A^n)} \right]} = \frac{\beta}{1-\alpha}$$

and

$$\frac{\exp \left\{ -\frac{n}{2} (\lambda_1 - \lambda_0) \right\} M \left[ \frac{Kn-1}{2}, \frac{K-1}{2}, \frac{m\lambda_1 V_R^n}{2(1+V_R^n)} \right]}{M \left[ \frac{Kn-1}{2}, \frac{K-1}{2}, \frac{m\lambda_0 V_R^n}{2(1+V_R^n)} \right]} = \frac{1-\beta}{\alpha}$$

where  $M(X, Y, Z)$  is the confluent hypergeometric function given in Section (1.1) and discussed by Stater (1960).

These quantities are obtained by solving the above equations by a Newton-Raphson root solving technique (Carnahan, et al (1969)).

In some cases, i.e., for small values of  $n$ , a root does not exist for the equations above. In such cases it is not possible to make a decision at that stage.

The following pages contain a listing of a computer program which will calculate regions for any given values of  $\alpha$ ,  $\beta$ ,  $K$ ,  $\lambda_0$  and  $\lambda_1$ .

Tables of such regions have been worked out by Ghosh and West (1967) for selected values of  $\alpha$ ,  $\beta$ ,  $\lambda_0$ , and  $\lambda$ . These regions however are only given for every fifth stage. Thus the following computer program also allows the Ghosh regions to be read in, and the missing region values calculated via Lagrangian interpolation (Ghosh and West (1967)).

```
FILE 5=CARD,UNIT=READER
FILE 6=PRINTER,UNIT=PRINTER
```

```
C *****
C          THIS PROGRAM ALLOWS
C          DETERMINATION OF FIXED SIZE ANOVA TEST
C          THIS PROGRAM WILL FIND A CRITICAL VALUE
C          C20 AND THE SMALLEST INTEGER N FOR GIVEN
C          VALUES OF ALPHA AND BETA
C          IF V<C THEN H0 IS ACCEPTED AND IF V>C H0 IS REJECTED
C *****
```

START OF SEGMENT

```

DIMENSION BOUND(2),XLIN(2),REG(50,2)
DOUBLE PRECISION VAL0,HYP1,HYP2,HYP3,HYP4,VAL2,VALST,FX,XLN,AUX1
1  ,AUX2 ,XNXT,FXNXT,XEVAL ,FPX
REAL LAM0,LAM1
COMMON EPS
TAU(Z)=((Z-0.5)*ALOG(Z))-Z*(0.5*ALOG(6.283185))+(1.0/(12.0*Z))
1=(1.0/(360.0*(Z**3.0)))+(1.0/(1260.0*(Z**5.0)))-(1.0/(1680.0*(Z**7.0
2)))
H1(GRN,SS,CP)=2.0*(((GRN-1.0)+(SS*CP))*3.0)
H2(GRN,SS,CP)=3.0*(((GRN-1.0)+(SS*CP))*((GRN-1.0)+(2.0*SS*CP))*(((G
1RN*(SS-1.0))-2.0))
H3(GRN,SS,CP)=(((GRN-1.0)+(3.0*SS*CP))*(((GRN*(SS-1.0))-2.0))*2.0)
CON2(GRN,SS,CP)=(((GRN-1.0)+(SS*CP))*2.0)+(((GRN*(SS-1.0))-2.0)
2*(((GRN-1.0)+(2.0*SS*CP))))
CON3(GRN,SS,CP,H)=(((GRN*(SS-1.0))/((GRN*(SS-1.0))-2.0))*(H-(((GRN-
31.0)+(SS*CP))/(GRN-1.0)))
EPS=1.0 E-8
IREAD=5
IRITE=6
READ(IREAD,1) ALPHA,BETA,LAM0,LAM1,DEGF
1  FORMAT(5F10.4)
WRITE(IRITE,701)
01  FORMAT(1H1,20X,"FIXED SAMPLE ANOVA TEST")
WRITE(IRITE,702)
02  FORMAT(/,20X,"*****")
WRITE(IRITE,703) DEGF
03  FORMAT(///,24X,"K=",F3.1,2X,"GROUPS")
READ(IREAD,713) SAM
13  FORMAT(F8.2)
IF(LAM1=0.0 .AND. SAM .GT. 0.0) GO TO 21
WRITE(IRITE,704) LAM0,LAM1
04  FORMAT(////,13X,9HHD,LAM0 =,F6.2,2X,"VS",2X,9HHI,LAM1 =,F6.2)
WRITE(IRITE,705) ALPHA,BETA
705  FORMAT(//,20X,"ALPHA =",F5.2,6X,"BETA =",F5.2)
DO 10 N=3,1000
SAM=FLD0AT(N)
IF(LAM0=0.0) GO TO 5
H=H1(DEGF,SAM,LAM0)+H2(DEGF,SAM,LAM0)+H3(DEGF,SAM,LAM0)
CONK=CON2(DEGF,SAM,LAM0)
E=(H**2.0)/(CONK**3.0)
B=((DEGF*(SAM-1.0))-2.0)*(SQRT(E/(E-4.0))-1.0)
B=B*0.5
V=(B/(DEGF-1.0))*(H/CONK)*(1.0/((2.0*B)+(DEGF*(SAM-1.0))-2.0) )
C=CON3(DEGF,SAM,LAM0,V)
T1=(DEGF*(SAM-1.0))/2.0
T2=B/2.0
GO TO 7
5  T1=0.5*DEGF*(SAM-1.0)
```

CCCCCCCCCCCC

```

21 T1=0.5*DEGF*(SAM=1.0)
   T2=0.5*(DEGF-1.0)
   Y0=BETINC(1,T1,T2,ALPHA)
   F0=(DEGF*(SAM=1.0)*(1.0-Y0))/((DEGF-1.0)*Y0)
   T1=(DEGF*(SAM=1.0))/2.0
   DO 625 LM=1,200
     ALTLAM=0.1*LM
     HP=H1(DEGF,SAM,ALTLAM)+H2(DEGF,SAM,ALTLAM)+H3(DEGF,SAM,ALTLAM)
     CONKP=CON2(DEGF,SAM,ALTLAM)
     EP=(HP**2.0)/(CONKP**3.0)
     BP=((DEGF*(SAM=1.0))-2.0)*(SQRT(EP/(EP-4.0))-1.0)
     BP=BP*0.5
     VP=(BP/(DEGF-1.0))*(HP/CONKP)*(1./((2.*BP)+(DEGF*(SAM=1.0))-2.0))
     CP=CON3(DEGF,SAM,ALTLAM,VP)
     T3=BP/2.0
     Y1=1.0/(1.0+((BP/(DEGF*(SAM=1.0)))*((F0+ CP )/VP)) )
     PROB=BETINC(0,T1,T3,Y1)
     A4=1.0-BETA
     IF(PROB .GE. A4) GO TO 27
625 CONTINUE
27 LAM1=ALTLAM
   WRITE(IRITE,704) LAM0,LAM1
   WRITE(IRITE,705) ALPHA,BETA
   WRITE(IRITE,706) SAM
13 CONTINUE

```

C \*\*\*\*\*

C

C THIS PART OF THE PROGRAM CALCULATES THE OC FUNCTION  
C FOR THE FIXED SIZE TEST

C \*\*\*\*\*

C

```

C
WRITE(IRITE,707)
707  FORMAT(///,20X,"OC FUNCTION FOR THE TEST")
WRITE(IRITE,708)
708  FORMAT(///,14X,"LAMDA",10X,"PROB OF ACCEPTING H0")
DO 401 IPGW=1,10
  APLAM=LAM0+(((LAM1-LAM0)/9.0)*FLOAT(IPGW-1))
  IF(APLAM>0.0) GO TO 403
  ANOC=BETINC(0,T1,T2,Y0)
  ANOC=1.0-ANOC
  GO TO 402
403  HP=H1(DEGF,SAM,APLAM)+H2(DEGF,SAM,APLAM)+H3(DEGF,SAM,APLAM)
  CONKP=CON2(DEGF,SAM,APLAM)
  EP=(HP**2.0)/(CONKP**3.0)
  BP=((DEGF*(SAM-1.0))-2.0)*(SQRT(EP/(EP-4.0))-1.0)
  BP=BP*0.5
  VP=(BP/(DEGF-1.0))*(HP/CONKP)*(1./((2.+BP)+(DEGF*(SAM-1.0))-2.0))
  CP=CON3(DEGF,SAM,APLAM,VP)
  T3=BP/2.0
  Y1=1.0/(1.0+((BP/(DEGF*(SAM-1.0)))+(FO+CP)/VP))
  ANOC=BETINC(0,T1,T3,Y1)
  ANOC=1.0-ANOC
402  WRITE(IRITE,709) APLAM,ANOC
709  FORMAT(/,14X,F5.2,17X,F6.4)
401  CONTINUE
WRITE(IRITE,710) FO
710  FORMAT(///,16X,"CRITICAL VALUE OF F =",F7.2)
  CVV=(FO*(DEGF-1.0))/(DEGF*(SAM-1.0))
  WRITE(IRITE,711) CVV
711  FORMAT(///,16X,"CRITICAL VALUE OF V =",F10.5)
  READ(IREAD,101) IREG
101  FORMAT(I2)
  IF(IREG=0) GO TO 160

```

C \*\*\*\*\*

C

C THIS PART OF THE PROGRAM WILL FIND WALD REGIONS FOR  
C EVERY NSNO (THE FIXED SIZE TEST) BY INTERPOLATION  
C OF THE GHOSH AND WEST TABLES

C \*\*\*\*\*

C

```

30  CONTINUE
WRITE(IRITE,715)
715  FORMAT(1H1,20X,"SEQUENTIAL ANOVA TEST")
WRITE(IRITE,702)
WRITE(IRITE,703) DEGF
WRITE(IRITE,704) LAM0,LAM1
WRITE(IRITE,705) ALPHA,BETA
WRITE(IRITE,716)
716  FORMAT(///,20X,"THE WALD REGIONS ARE")
WRITE(IRITE,717)
717  FORMAT(///,10X,"STEP",10X,"LOWER VN",10X,"UPPER VN")
  NSAM=IFIX(SAM)
306  READ(IREAD,25) I,AL1,AL2
25  FORMAT(I3,2F10.5)

```

```

IF(I.LE. NSAM) GO TO 35
ICOUNT=ICOUNT+1
IF(ICOUNT>2) GO TO 40
35  REG(I,1)=AL1
    REG(I,2)=AL2
    GO TO 306
40  DO 150  INDX=1,2
    N1SS=1
    N2SS=1
    N3SS=1
41  IF(REG(N1SS,INDX)>0) GO TO 42
    N1SS=N1SS+1
    GO TO 41
42  N2SS=N2SS+1
43  IF(REG(N2SS,INDX)>0) GO TO 44
    N2SS=N2SS+1
    GO TO 43
44  IF(N2SS>N1SS+1) GO TO 46
    N1SS=N2SS
    GO TO 42
46  N3SS=N2SS+1
47  IF(REG(N3SS,INDX)>0) GO TO 48
    N3SS=N3SS+1
    GO TO 47
48  L1=N1SS+1
    L2=N2SS+1
    IF(L2>NSAM) L2=NSAM
    S1=FLOAT(N1SS)
    S2=FLOAT(N2SS)
    S3=FLOAT(N3SS)
    AN=S1+S2+S3
    DO 140  INBT=L1,L2
    SB=FLOAT(INBT)
    Z1=(((AN/SB)-(AN/S2))*((AN/SB)-(AN/S3)))/(((AN/S1)-(AN/S2))
1 * ((AN/S1)-(AN/S3)))
    Z2=(((AN/SB)-(AN/S1))*((AN/SB)-(AN/S3)))/(((AN/S2)-(AN/S1))
2 * ((AN/S2)-(AN/S3)))
    Z3=(((AN/SB)-(AN/S1))*((AN/SB)-(AN/S2)))/(((AN/S3)-(AN/S1))
3 * ((AN/S3)-(AN/S2)))
    REG(INBT,INDX)=Z1*REG(N1SS,INDX)+Z2*REG(N2SS,INDX)
4 +Z3*REG(N3SS,INDX)
140  CONTINUE
    IF(L2=NSAM) GO TO 150
    N1SS=N2SS
    GO TO 42
150  CONTINUE
155  DO 156  JMF=1,NSAM
    IF(REG(JMF,1)=0.0) REG(JMF,1)=99999.
    IF(REG(JMF,2)=0.0) REG(JMF,2)=99999.
    WRITE(IRITE,301) JMF,REG(JMF,1),REG(JMF,2)
156  CONTINUE
    WRITE(IRITE,721)
721  FORMAT(/,80X,"INTERPOLATED")
    GO TO 445

```

```

C
C
C *****
C               THIS PART OF THE PROGRAM WILL CALCULATE REGIONS FOR
C               TESTS NOT CONTAINED IN THE GHOSH + WEST TABLES
C
C
C *****

```

```

160  W2=(DEGF-1.0)/2.0
      NSAM=IFIX(SAM)
      WRITE(IRITE,715)
      WRITE(IRITE,702)
      WRITE(IRITE,703)  DEGF
      WRITE(IRITE,704)  LAM0,LAM1
      WRITE(IRITE,705)  ALPHA,BETA

                                                                    SE
                                                                    START OF

      WRITE(IRITE,716)
      WRITE(IRITE,717)
      BOUND(1)=      ALOG(BETA/(1.0-ALPHA))
      BOUND(2)=      ALOG((1.0-BETA)/ALPHA)
      XLIN(1)= (2.0*BOUND(1)+(LAM1-LAM0))/(-2.0*BOUND(1))
      XLIN(2)= (2.0*BOUND(2)+(LAM1-LAM0))/(-2.0*BOUND(2))
      DO 220  NSZ=2,NSAM
      ECON=-(FLOAT(NSZ)*(LAM1-LAM0))/2.0
      W1=((DEGF*FLOAT(NSZ))-1.0)/2.0
      ZCON1=(FLOAT(NSZ)*LAM1)/2.0
      ZCON0=(FLOAT(NSZ)*LAM0)/2.0
      DO 210  IB=1,2
      XEVAL=0.0
      IF( XLIN(IB) .GT. 0.0 .AND. XLIN(IB) .GT. 1.0) GO TO 297
      IF(XLIN(IB) .GT. 0.0) GO TO 170
      VAL0= EXP(ECON) - EXP(BOUND(IB))
      DO 296  ISR=1,9
      XSR= -(ISR*0.1)
      SEAR= ( XSR/(1.0+XSR))
      W3=ZCON1*SEAR
      W4=ZCON0*SEAR
      HYP1= CONHYP(W1,W2,W3)
      HYP2= CONHYP(W1,W2,W4)
      VAL2= ( EXP(ECON)*HYP1) -( EXP(BOUND(IB))*HYP2)
      IF( (VAL0*VAL2) .LE. 0.0 .AND. XLIN(IB) .LT. 0.0) GO TO 210
296  CONTINUE
      SEAR=0.99
      W3= ZCON1*SEAR
      W4=ZCON0*SEAR
      HYP1= CONHYP(W1,W2,W3)
      HYP2= CONHYP(W1,W2,W4)
      VAL2= ( EXP(ECON)*HYP1) -( EXP( BOUND(IB))*HYP2)
      IF( (VAL0*VAL2) .GT. 0.0) GO TO 210
297  W3=ZCON1*0.5
      W4=ZCON0*0.5
      HYP1= CONHYP(W1,W2,W3)
      HYP2= CONHYP(W1,W2,W4)
      VALST=( EXP(ECON)*HYP1) -( EXP(BOUND(IB))*HYP2)
      IF( (VALST*VAL0) .GT. 0.0) GO TO 197
      XLIN(IB)=1.0
      GO TO 170
197  DO 386  IFND=10,60 ,10
      SEARS=IFND/(1.0+IFND)
      W3=ZCON1*SEARS
      W4=ZCON0*SEARS
      HYP1= CONHYP(W1,W2,W3)
      HYP2= CONHYP(W1,W2,W4)
      VALS= ( EXP(ECON)*HYP1) -( EXP(BOUND(IB))*HYP2)
      IF((VALST*VALS)) 387,386,386
387  XLIN(IB)=IFND*5.0
      GO TO 170
386  CONTINUE
      XI TN( TR)=IFND

```

```

170  CONTINUE
    IF(XLIN(IB) .GT. 0.0) GO TO 195
    XLIN(IB)= XLIN(IB)+XLN
    IF( XLIN(IB) .EQ. -1.0) XLIN(IB)=-0.5
    GO TO 170
195  W3= ZCON1*(XLIN(IB)/(1.0+XLIN(IB)))
    W4=ZCON0*(XLIN(IB)/(1.0+XLIN(IB)) )
    HYP1=CONHYP(W1,W2,W3)
    HYP2=CONHYP(W1,W2,W4)
    Y1=W1+1.0
    Y2=W2+1.0
    HYP3=CONHYP(Y1,Y2,W3)
    HYP4=CONHYP(Y1,Y2,W4)
    AUX1=(FLOAT(NSZ)*W1)/((2.0*W2*((1.0+XLIN(IB))**2.0))
    AUX2=((LAM1*HYP3)/HYP1)-((LAM0*HYP4)/HYP2)
    FPX=AUX1*AUX2
    HYP1= DLOG(HYP1)
    HYP2= DLOG(HYP2)
    FX=ECON+HYP1-HYP2-BOUND(IB)
    IF( DABS(FPX) .LE. 2.0) GO TO 501
503  XLN= XLIN(IB)-(FX/FPX)
    IF( DABS(XLIN(IB)-XLN) .LE. EPS ) GO TO 210
    XINT=XLIN(IB)
    XLIN(IB)=XLN
    XLN=XINT
    XEVAL=FX
    GO TO 170
501  IF( (XEVAL*FX)) 502,503,503
502  XNXT= ( XLIN(IB)+XLN)*0.5
    W3=ZCON1*(XNXT/(1.0+XNXT))
    W4= ZCON0*(XNXT/(1.0+XNXT))
    HYP1= CONHYP( W1,W2,W3)
    HYP2= CONHYP(W1,W2,W4)
    FXNXT= ECON+ DLOG(HYP1)- DLOG(HYP2) -BOUND(IB)
    IF((XEVAL*FXNXT)) 505,210,506
505  XLIN(IB)=XNXT
    FX=FXNXT
    GO TO 507
506  XLN=XNXT
    XEVAL=FXNXT
507  IF( DABS(XLIN(IB)-XLN) .LE. EPS) GO TO 210
    GO TO 502
210  CONTINUE
    WRITE(IRITE,301) NSZ,XLIN(1),XLIN(2)
301  FORMAT(11X,I2,10X,F8.4,10X,F8.4)

220  CONTINUE
    WRITE(IRITE,720)
720  FORMAT(//,80X,"CALCULATED")

445  CONTINUE
    STOP
    END

```

START OF SE

```

FUNCTION ZI(X,A,B)
  FN=.7*(ALOG(15.+A+B))**2+AMAX1(X*(A+B)-A,0.0)
  N=INT(FN)
  C=1.+(A+B)*X/(A+2.*FN)
  ZI=2./(C+SQRT(C**2-4.*FN*(FN-B)*X/(A+2.*FN)**2))
  DO 60 J=1,N
    FN=FN+1-J
    A2N=A+2.*FN
    ZI=(A2N-2.)*(A2N-1.-FN*(FN-B)*X*ZI/A2N)
    ZI=1./(1.-(A+FN-1.)*(A+FN-1.+B)*X/ZI)
60  CONTINUE
    RETURN
  END

```

SEG

```

FUNCTION CGAM(A)
  AA=A
  CAC=0.0
  IF(A=2.)2,8,8
  IF(A=1.)4,6,6
  CAC=-2.+(A+.5)*ALOG(1.+1./A)+(A+1.5)*ALOG(1.+1./(A+1.))
  AA=A+2.
  GO TO 8
  CAC=-1.+(A+.5)*ALOG(1.+1./A)
  AA=A+1.
  CA=2.269489/AA
  CA=.52560647/(AA+1.0115231/(AA+1.5174737/(AA+CA)))
  CA=.0833333333/(AA+.03333333/(AA+.25238095/(AA+CA)))
  CGAM=CA+CAC
  RETURN
  END

```

START OF SE

```

      FUNCTION BETINC(IND,A,B,X)
C      INCOMPLETE BETA FUNCTION AND ITS INVERSE
C      MARK=1 FOR INVERSE (SEND DOWN PROB)
      CAB=CGAM(A+B)-CGAM(A)-CGAM(B)-.5*ALOG((A+B)*6.28318531)
      IF(IND)10,10,20
10     EP=CAB+A*ALOG(X*(1.+B/A))+B*ALOG((1.-X)*(1.+A/B))
      IF(X=A/(A+B))12,12,14
12     BETINC=ZI(X,A,B)*EXP(EP+.5*ALOG(B/A))
      RETURN
14     BETINC=1.-ZI(1.-X,B,A)*EXP(EP+.5*ALOG(A/B))
      RETURN
20     IF(X=.5)22,22,24
22     QZ=ALOG(X)
      IGO=1
      AA=A
      BB=B
      GO TO 26
24     QZ=ALOG(1.-X)
      IGO=2
      AA=B
      BB=A
26     XT=AA/(AA+BB)
      CABB=CAB+.5*ALOG(BB/AA)+AA*ALOG(1.+BB/AA)+BB*ALOG(1.+AA/BB)
      DO 40 NC=1,100
      ZZ=ZI(XT,AA,BB)
      QX=CABB+AA*ALOG(XT)+BB*ALOG(1.-XT)+ALOG(ZZ)
      XC=(QZ-QX)*(1.-XT)*ZZ/AA
      XC=AMAX1(XC,.99)
      XC=AMIN1(XC,.5/XT-.5)
      XT=XT*(1.+XC)
      IF(ABS(XC)-1.E-6)42,40,40
40     CONTINUE
42     GO TO (44,46),IGO
44     BETINC=XT
      RETURN
46     BETINC=1.-XT
      RETURN
      END

```

```

FUNCTION CONHYP(XF,YF,UF)
COMMON EPS
DOUBLE PRECISION TSUM
TAU(AR)=ALGAMA(AR)
X=XF
Y=YF
U=UF
PMULT=1.0
TSUM=1.0
IF(X=Y) 101,100,101
100 CONHYP= EXP(U)
RETURN
101 IF(U) 103,102,104
102 CONHYP= 1.00
RETURN
103 X=Y-X
PMULT= EXP(U)
U= *U
104 IF(X) 105,102,106
105 ICHK=-IFIX(X)
TEST=ICHK*X
IF(TEST) 111,108,111
108 IF( ICHK=1) 111,107,109
107 CONHYP=(1.0-(U/Y))*PMULT
RETURN
109 INDX=ICHK
XSTAR=1.0
DO 110 N=1,INDX
XSTAR= XSTAR*( X+N-1.0)
T1= Y+N
T2= FLUAT(N+1)
T3= FLUAT(N)
YSTAR= (TAU(Y)-TAU(T1)-TAU(T2))+(T3* ALOG(U))
TSUM= TSUM+ (XSTAR* EXP(YSTAR))
110 CONTINUE
CONHYP= PMULT*TSUM
RETURN
111 DO 125 IT=1,50
T=FLOAT(IT)
T1=T*X
T2=T*Y
T3=T+1.0
PS= ( GAMMA(Y) / GAMMA(X))*( GAMMA(T1) /GAMMA(T2))
PF= (T* ALOG(U))-TAU(T3)
PS=PS * EXP(PF)
TSUM= TSUM+PS
IF( ABS(PS) .LE. EPS) GO TO 112
125 CONTINUE
112 CONHYP= TSUM* PMULT
RETURN
106 DO 115 IT=1,50
T= FLUAT(IT)
T1=T*X
T2=T*Y
T3=T+1.0
PS=TAU(Y)+TAU(T1)-TAU(X)-TAU(T2)-TAU(T3)
PS= EXP(PS)*(U**T)
TSUM= TSUM+PS
IF ( ABS(PS) .LE. EPS) GO TO 120
115 CONTINUE
120 CONHYP= TSUM* PMULT
RETURN

```

## FIXED SAMPLE ANOVA TEST

\*\*\*\*\*

K=2.0 GROUPS

H0: LAM0 = 0.00 VS H1: LAM1 = 1.00

ALPHA = 0.01 BETA = 0.01

REQUIRED SAMPLE SIZE IS 27.0

## OC FUNCTION FOR THE TEST

LAMDA	PROB OF ACCEPTING H0
0.00	0.9900
0.11	0.8180
0.22	0.5793
0.33	0.3673
0.44	0.2154
0.56	0.1192
0.67	0.0631
0.78	0.0323
0.89	0.0160
1.00	0.0078

CRITICAL VALUE OF F = 7.15

CRITICAL VALUE OF V = 0.13748

---

 SEQUENTIAL ANOVA TEST
 

---

\*\*\*\*\*

---

 K=2.0 GROUPS
 

---



---

 H0: LAM0 = 0.00 VS H1: LAM1 = 1.00
 

---



---

 ALPHA = 0.01      BETA = 0.01
 

---



---

 THE WALD REGIONS ARE
 

---

STEP	LOWER VN	UPPER VN
2	-0.8912	-1.1088
3	-0.8912	-1.1088
4	-0.8912	-1.1088
5	-0.8912	42.7986
6	-0.8912	3.5556
7	-0.8912	1.8734
8	-0.8912	1.2850
9	-0.8912	0.9872
10	0.0049	0.8082
11	0.0104	0.6891
12	0.0156	0.6044
13	0.0204	0.5412
14	0.0250	0.4924
15	0.0293	0.4535
16	0.0333	0.4219
17	0.0371	0.3956
18	0.0406	0.3736
19	0.0438	0.3548
20	0.0468	0.3385
21	0.0497	0.3244
22	0.0523	0.3120
23	0.0548	0.3010
24	0.0571	0.2912
25	0.0593	0.2824
26	0.0614	0.2745
27	0.0633	0.2674

---

## APPENDIX C

A COMPUTER PROGRAM FOR  $k=2$  SANOVA

Chapter 2 of this thesis derived a procedure for obtaining the properties of a  $k=2$  SANOVA test. The procedure has been summarized in Figures 12 and 13. As previously discussed, this procedure cannot feasibly be performed analytically. Section (2.6) considered an alternative, a numerical implementation of the theory. This appendix contains a computer program for obtaining the properties of a  $k=2$  SANOVA test utilizing the approach discussed in Section (2.6).

The program is written in Fortran IV for use on a Burroughs or CDC computer. Its implementation on other machines may require modifications, specifically the statements involving a read or write from disc.

To use the program, the user must supply the following information:

- 1)  $\lambda_0, \lambda_1, k, m_0$

On one card in a (3F10.5,I3) format.

Note  $k$  is the number of means and should always be input as 2;  $m_0$  is the truncation point.

- 2)  $V_A^i, V_R^i, i=1, \dots, m_0$ .

Two numbers per card ( $V_A^i$  being the acceptance region and  $V_R^i$  the rejection) in a (2F15.0) format. Any time acceptance is not possible at a given stage  $j$ ,  $V_A^j$  should be input as a negative number. Similarly, any time rejection is not possible,  $V_R^j$  should be input as a number greater than  $10^{10}$ . Note that the first region card should always be of the form  $V_A^1 = -1, V_R^1 = 10^{10}$ , since no decision can be made at this stage.

- 3) Gridsize in an (F10.0) format.

This represents the coarseness of the grid or the quantities  $h_Q$  and  $h_W$  of Section (2.6). The program assumes that  $h_Q = h_W$ . It is best to select this number as a power of 2, e.g., 0.5, 0.25, etc. In general, the smaller this number, the more accurate the results but the larger the amount of computation required. As discussed in Section (2.6), the most efficient approach is to perform several runs, using a finer grid size on each run.

The program uses two random access disc files (files 1 and 2). These files represent the density at stages  $i$  and  $i+1 (i=n_1, \dots, m_0-1)$ . The first file is used to compute the second file as discussed in Section (2.6). The size of these files is dependent upon the choice of the gridsize parameter. However, 125,000 words per file should be sufficient for most problems.

The program output consists of the probability of acceptance, rejection and continuation ( $P_A^i, P_R^i, P_C^i$ ) for each stage for every value of  $\lambda$ . These quantities are then used to compute summary OC and ASN curves.

Currently, the program is being implemented on a CDC computer by Mr. Kent Kaufmann of Western Illinois University. The program will be used to generate a brief set of OC and ASN curves for several  $k=2$  SANOVA tests.

C-5

FILE 1=ST1/MIL,UNIT=DISK,SAVE=99,LOCK,RANDOM,BLOCKING=30,RECORD=1  
 FILE 2=ST2/MIL,UNIT=DISK,SAVE=99,LOCK,RANDOM,BLOCKING=30,RECORD=1  
 FILE 10=RES/MIL,UNIT=DISK,SAVE=99,LOCK,RANDOM,RECORD=32  
 FILE 11=CUR/MIL,UNIT=DISK,SAVE=99,LOCK,RANDOM,BLOCKING=5,RECORD=6  
 FILE 5=CARD,UNIT=READER  
 FILE 6=OUTPUT,UNIT=PRINTER  
 FILE 7=DEBUG,UNIT=PRINTER  
 FILE 8=TEMP,UNIT=PRINTER

00000500  
 00000600  
 00000700  
 00000800  
 00000900  
 00001000  
 00001100  
 00001200  
 00001300  
 00001400  
 00001500  
 00001600  
 00001700  
 00001800  
 00001900  
 00002000  
 00002100

SEQUENTIAL ANALYSIS OF VARIANCE  
 R. MILLER

THIS PROGRAM CALCULATES THE AVERAGE SAMPLE NUMBER,  
 MEDIAN SAMPLE SIZE, AND OPERATING CHARACTERISTIC FUNCTION FOR  
 A SEQUENTIAL TEST OF THE EQUALITY OF K MEANS  
 THE TEST IS CHARACTERIZED BY A LAM0, LAM1, AND REGIONS

## START OF SEGMENT

COMMON /CB10/ CA, PA, CR, PR, A, B, C 00002200  
 COMMON /CB1/ GRIDW, GRIDQ, GRIDR 00002300  
 COMMON /CB2/ JREC, TSTAT 00002400  
 COMMON /CB3/ NCONW, NCONQ, NSIRI 00002500  
 COMMON /CB5/ REG(30,2) 00002600  
 COMMON /CB4/ DEGF, ALAM 00002700  
 COMMON /CB6/ IMAXW, IMINW, IMAXQ, TMINQ 00002800  
 COMMON /CB8/ JOINT1, ICAL 00002900  
 COMMON /CB11/ SINE45 00003000  
 COMMON /CB12/ NUMW, NUMQ, NUMR 00003100  
 COMMON /CB14/ XMEAN(2), XBR1, XBR2, VAR, DGF 00003200  
 COMMON /CB7/ LSTP, ISUR 00003300  
 COMMON /CB15/ GREGC(14,14) 00003400  
 COMMON /CB20/ RECMAX  
 COMMON /ERR/ IRP1, IRP2 00003500  
 REAL LAM0, LAM1 00003600

THIS IS NECESSARY FOR START-RESTART

COMMON /RESTAR/ OC(30,2), ASN(30), NTESTS  
 COMMON /RESTAR/ KTEST, NUC, NSTP, I1, I2, I3, KREC, IRAC, NPFLAC, IRNK  
 COMMON /RESTAR/ NPFINR, PROBAC, PROBNR, PRRAC, PRQAC, PRNR, PRQNR  
 COMMON /RESTAR/ RVALAC, RVALNR, RACBEG, SPRUAC, RNBEG, SPRUNK  
 COMMON /RESTAR/ WN, WN, RN  
 EQUIVALENCE (RNBEG, RNRBEG)

ELIPFI(Q,W,R,N,VR)=(((Q\*COS(45.))-W\*SIN(45.))\*\*2.)/(R\*FLOAT(N)+RAD) 00003800  
 1 )+(((Q\*SIN(45.))+W\*COS(45.))\*\*2.)/(((R\*FLOAT(N)\*VR)/(2.\*(FLOAT(N) 00003900  
 2 \*\*4.0)\*VR))+RAD))-1.0 00004000  
 PARAR(XC,XP,QC,WC)=(XC\*((QC-(XP\*WC/XC))\*\*2.))+(XC\*(WC\*\*2.)) 00004100  
 1 -(((XP\*WC)\*\*2.)/XC) 00004200  
 DATA IRLAD,IRITE/5.0/ 00004300  
 EPS=1.0E-6 00004400  
 NPFI=6 00004500  
 SINE45=SIN(0.78539816) 00004600  
 READ(10=1) NTKYS,ITLST,KOC,MSTP  
 NTRY5=NTRY5+1  
 READ(IRLAD,199) NTESTS 00004700

	C-6	
C		00004900
C	INPUT TO THIS PROGRAM CONSISTS OF LAM0•LAM1•K=NUMBER OF MEANS	00005000
C	AND THE TRUNCATION POINT AS WELL AS THE REGIONS	00005100
C		00005200
	DO 9112 KTEST=1•NTESTS	00005300
	READ(IRLAD,205) LAM0•LAM1•DEGF•MTP	00005400
205	FORMAT(3F10.5,I3)	00005500
C		00005600
C	REG(1,1)=VALUE OF V1 FOR WHICH ANY VSV1 RESULTS IN ACCEPTANCE	00005700
C	REG(1,2)=VALUE OF V1 FOR WHICH ANY VZV1 RESULTS IN REJECTION	00005800
C		00005900
C		00006000
C	IF IT IS NOT POSSIBLE TO ACCEPT AT STEP 1 REG(1,1)=0.0	00006100
C	IF IT IS NOT POSSIBLE TO REJECT AT STEP 1 REG(1,2)=1.E10	00006200
C		00006300
	READ (IRLAD,206) ((REG(J1,1)•REG(J1,2))•J1=1•MTP)	00006400
206	FORMAT(2F15.0)	00006500
	NUM=FIX(DEGF)-1	00006600
	DO 20 M=1•NUM	00006700
	XMEAN(M)=0.0	00006800
20	CONTINUE	00006900
	NUM=NUM+1	00007000
C		00007100
C		00007200
C	A SEARCH IS MADE TO DETERMINE THE FIRST STEP AT	00007300
C	WHICH A DECISION IS POSSIBLE	00007400
C		00007500
	DO 35 NSTP=1•MTP	00007600
	IF( REG(NSTP,1) .LE. 0.0 .AND. REG(NSTP,2) .GE. 1.E10) GO TO 25	00007800
	ISUR=NSTP	00007900
	NCAL=ISUR+1	00008000
	GO TO 40	00008100
25	CALL FSTEPROB(DC(NSTP,1)•DC(NSTP,2)•ASN(NSTP)•NSTP)	00007700
	IF( KTEST .GT. ITEST .OR. NDC .GT. KDC)	
	1WRITE(11=((NSTP+((NDC-1)•NTESTS)+(KTEST-1)•NTESTS*10)) DC(NSTP,1),	
	2 DC(NSTP,2)•ASN(NSTP)•NSTP•ALAM•KTEST	
35	CONTINUE	00008200
40	READ(IRLAD,207) GRIDSZ	00008300
207	FORMAT(F10.0)	00008400
	IF(ITEST .GT. KTEST) GO TO 9112	
	GRIDW=GRIDSZ	00008500
	GRIDQ=GRIDSZ	00008600
	GRIDR=GRIDW**2.0	00008700
	RAD=(3.0*(GRIDW**2.0+GRIDQ**2.0))**0.5	00008800
C		00008900
C	THE DIMENSIONS OF THE GRID ARE CALCULATED	00009000
C		00009100
	XVAL= 10.0*((0.4)**DEGF)**0.5)	00009200
	MAXVAL=XVAL*((2.0*DEGF*FLOAT(ISUR-1))**0.5)+(DEGF*(FLOAT(ISUR-1)))	00009300
	STORE= MAXVAL/GRIDR	00009400
	NUMR=FIX(STORE)+1	00009500
	VAR= 4.0*(FLOAT(ISUR)**0.5)	00009600
	NUMW=((FIX(VAR/GRIDW)+1)*2)+1	00009700
	NUMQ=((FIX(VAR/GRIDQ)+1)*2)+1	00009800
	RECMAX=NUMQ*NUMR*NUMW	00010000
	VAR= (FLOAT(ISUR)**0.5)	00010100
	DGF=DEGF*FLOAT(ISUR-1)	00010200
	NSTRI=ISUR	00010210
	WRITE(IRITE,1401)	00010300
1401	FORMAT(1H1,10X,"SEQUENTIAL ANALYSIS OF VARIANCE")	00010400
	WRITE(IRITE,1402)	00010500
1402	FORMAT(//,20X,"THE TEST IS")	00010600
	WRITE(IRITE,1403) LAM0•LAM1	00010700

1404	FORMAT(//,15X,"WITH K ="*F2.0) C-7	00011000
	WRITE(IRITE,1405)	00011100
1405	FORMAT(//,15X,"AND THE FOLLOWING REGIONS")	00011200
	WRITE(IRITE,1406)	00011300
1406	FORMAT(12X,"STEP",5X,"VN ACCEPT",5X,"VN REJECT")	00011400
	DO 1407 IAM=1,MTP	00011500
	IF(REG(IAM,1).LE.0.0) REG(IAM,1)=-9999.99	00011600
	WRITE(IRITE,1407) IAM,REG(IAM,1),REG(IAM,2)	00011700
1407	FORMAT(13X,12.6X,F8.4,6X,F8.4)	00011800
1409	CONTINUE	00011900
	WRITE(IRITE,1410) GRIDW,GRIDQ,GRIDR	00012000
1410	FORMAT(//,12X,"GRIDW=",F6.3,3X,"GRIDQ=",F6.3,3X,"GRIDR=",F6.3)	00012100
	WRITE(IRITE,1411) NUMW,NUMQ,NUMR	00012200
1411	FORMAT(12X,"SIZEW=",14.5X,"SIZEQ=",14.5X,"SIZER=",14)	00012300
	WRITE(IRITE,1412) RLCMAX	00012400
1412	FORMAT(//,12X,"TOTAL NUMBER OF GRID POINTS USED=",19)	00012500
	CALL BOOK(1,1,1,0,WN,QN,RN)	00012600
	PRB1=PHI(WN,0,VAR)	00012700
	VALUE=AMAX1(GRIDR,POSROB(WN,QN,RN,ISUR))	00012800
	PRB2=CHISQ(VALUE,DGF)	00012900
	CALL PCAL(1,1,NUMR,0,WN,QN,RN)	00013000
	PRB3=CHISQ((POSROB(WN,QN,RN,ISUR)),DGF)	00013100
	WRITE(IRITE,1413) PRB1,PRB2,PRB3	00013200
1413	FORMAT(12X,"MIN W PROB ="*E15.5,7,12X,"RANGE OF R PROB ="*E15.5,	00013300
	1 5X,*E15.5)	00013400
	WRITE(IRITE,202)	00013500
202	FORMAT(1H1,30X,"SEQUENTIAL ANOVA")	00013600
	WRITE(IRITE,203)	00013700
203	FORMAT(///,5X,"LAMBDA",10X,"MSN",10X,"ASN",10X,"UC",10X,"POW")	00013800
C		00014000
C	SEVERAL POINTS ON THE UC CURVE	00014100
C	ARE CALCULATED FOR A SEQUENTIAL TEST	00014200
C	WITH THESE REGIONS	00014300
C		00014400
	SEGMENT	
	DO 500 NUC=1,10,9	00014500
	IF(NUC.GT. NDC) GO TO 500	
	ALAM=LAM0+ ((LAM1-LAM0)/9.0)*FLOAT(NDC-1)	00014600
	WRITE(7,204) ALAM	00014700
204	FORMAT(1H1,30X,"LAMBDA= ",F6.3)	00014800
		00014900
C		00015000
C	FOR A GIVEN LAMBDA VALUES OF MEAN1 AND MEAN2 CAN BE	00015100
C	CALCULATED. THESE ARE NEEDED FOR THE BOOKING	00015200
C	SUBROUTINE AND TO CALCULATE CERTAIN PROBABILITIES	00015300
C	SUCH AS THE F(W,0,P) AT THE FIRST STEP	00015400
C	AND FOR PHI(Z) AND PHI(U)	00015500
C		00015600
		00015700
	XMEAN(NUM)= SORT((DEGF*ALAM)/(DEGF-1.0))	00015800
	XBR1=XMEAN(1)*FLOAT(ISUR)	00015900
	XBR2=XMEAN(2)*FLOAT(ISUR)	00016000
	NCONW=FIX((ISUR*XMEAN(1))/GRIDW)-FIX(NUMW/2.)	00016100
	NCONQ=FIX((ISUR*XMEAN(2))/GRIDQ)-FIX(NUMQ/2.)	00016200
	JOINT=1	00016300
	ICAL=2	00016400
	CALL BOOK(1,1,1,0,TMINW,TMINQ,TMINR)	00016500
	CALL BOOK(NUMW,NUMQ,NUMR,0,TMAXW,TMAXQ,TMAXR)	00016600
	WRITE(7,72) XMEAN(1),XMEAN(2),VAR,XBR1,XBR2	00016700
972	FORMAT(///,5X,"MEAN1=",E15.7,2X,"MEAN2=",E15.7,2X,"VAR=",E15.7,2X,	00016800
	1"SMEAN1=",E15.7,2X,"SMEAN2=",E15.7)	00016900
	WRITE(7,801) NUMR,NUMQ,NUMW	00017000
801	FORMAT(20X,31/)	00017100
	WRITE(7,802) TMINQ,TMINW,TMAXQ,TMAXW,TMAXR	00017200
		00017300

```

241  FORMAT(777,8X,"STEP",10X,"PROB. ACCEPT",13X,"PROB. REJECT",11X, 00017500
      1"PROB. CONTINUE") 00017600
      CALL FSLPPROB( UC(ISUR,1),UC(ISUR,2),ASN(ISUR),ISUR)
      IF( KTEST .GT. ITEST .OR. NUC .GT. KUC)
      1WRITE(11=(ISUR+((NUC-1)*NTESTS)+(KTEST-1)*NTESTS*10))UC(ISUR,1),
      2 UC(ISUR,2),ASN(ISUR),ISUR, ALAM,KTEST
      WRITE(7,208) ISUR,UC(ISUR,1),UC(ISUR,2),ASN(ISUR) 00017700
      LSTP=ISUR 00017800
      CR=1./ISUR 00017900
      PR=0.0 00018000
      CA=0.0 00018100
C 00018200
C THIS PART OF THE PROGRAM CALCULATES 00018300
C F(WN,QN,RN) FROM G( W(N-1), Q(N-1), R(N-1), Z, U) 00018400
C WHERE G(W(N-1),Q(N-1),R(N-1),Z,U)=F(W(N-1),Q(N-1),R(N-1))*P(Z)*P(U) 00018500
C 00018600
C IN ORDER TO FIND THE QUANTITIES OF INTEREST IN 00018700
C SEQUENTIAL ANALYSIS, NAMELY THE ASN AND UC CURVE 00018800
C THE PROBABILITY DISTRIBUTION MUST BE FOUND 00018900
C AT EVERY STEP N 00019000
C THEN THIS DISTRIBUTION CAN BE INTEGRATED TO FIND 00019100
C THE PROBABILITIES OF ACCEPTING, REJECTING AND CONTINUING AT 00019200
C EVERY STEP 00019300
C 00019400
      WRITE(8,777)
777  FORMAT(1H1)
      DO 400 NSTP=NCAL,MTP 00019500
      IF( MSTP .GT. NSTP) GO TO 399
      LSTP=NSTP-1 00019600
      IF( REG(LSTP,1) .LE. 0.0) GO TO 131 00019700
      CA=((2.0*REG(LSTP,1))+1.0)/(2.0*LSTP*REG(LSTP,1)) 00019800
      PA=1.0/(2.0*LSTP*REG(LSTP,1)) 00019900
131  IF( REG(LSTP,2) .GE. 1.E6) GO TO 132 00020000
      CR=((2.0*REG(LSTP,2))+1.0)/(2.0*LSTP*REG(LSTP,2)) 00020100
      PR=1.0/(2.0*LSTP*REG(LSTP,2)) 00020200
      GO TO 133 00020300
132  CR=1.0/FLOAT(LSTP) 00020400
      PR=0.0 00020500
133  PROBAC=0.0 00020600
      PROBNR=0.0 00020700
      PRAC=0.0 00020800
      PRQAC=0.0 00020900
      PRNR=0.0 00021000
      PRQNR=0.0 00021100
      DO 1130 I1=1,NUMW 00021200
      PRQAC=0.0 00021300
      PRQNR=0.0 00021400
      DO 1131 I2=1,NUMQ 00021500
      CALL BNRK(I1,I2,1.0,WN,QN,RN) 00021600
      IRAC=0 00021700
      IRNR=0 00021800
      RVALAC=1.E30 00021900
      IF( CA .LE. 0) GO TO 1121 00022000
      RVALAC=PARAK(CA,PA,QN,WN) 00022100
      RVALNR=PARAK(CR,PR,QN,WN) 00022200
1121  PRAC=0.0 00022300
      PRNR=0.0 00022400
      DO 5132 I3=1,NUMR
      IF( NTRY5 .GT. 1 .AND. PTIM1 .LE. 0.0)
      1 CALL RESUME( PTIM1,PTIM2,PTIM3,$5132)
      IF( I3 .LE. 1) GO TO 1122 00022600
      CALL RCAL(I1,I2,I3,0,WN,QN,RN) 00022700
1122  A=WN 00022800

```

KREC=JREC

C-9

IF( POSPROB(WN,QN,RN,NSIP) .LT. 0.0) GO TO 1132

THIS STATEMENT CALCULATES THE DENSITY AT POINT A,B,C  
AT NSTP BY INTEGRATING OVER A TWO DIMENSIONAL REGION IN LSTP

PROBTS=DENSTS(A,B,C,KREC)

IF( C .LT. RVALAC) GO TO 1124

IRAC=IRAC+1

IF( IRAC .GT. 1) GO TO 1123

NPF1AC=NUMR-13+1

RACBEG=C

SPROAC=PROBTS

THIS PART OF THE PROGRAM CALCULATES  
THE PROBABILITIES OF ACCEPTING, REJECTING, AND CONTINUING  
AT STEP NSTP

THESE ARE OBTAINED BY PERFORMING A THREEE DIMENSIONAL INTEGRATI

THIS THREE DIMENSIONAL INTEGRATION IS IS DONE NUMERICALLY  
BY THREE SUCCESSIVE 1 DIMENSIONAL INTEGRALS  
EACH 1 DIMENSIONAL INTEGRATION IS DONE VIA  
A 14 POINT(IF POSSIBLE) NEWTON-GREGORY FORMULA

1123 PRRAC=PRRAC+WLIGHT(NPF1AC,IRAC)\*PROBTS

1124 IF( C .LT. RVALNR) GO TO 1132

IRNR=IRNR+1

IF( IRNR .GT. 1) GO TO 1125

NPF1NR=NUMR-13+1

RNRBEG=C

SPRUNR=PROBTS

1125 PRRNR=PRRNR+WLIGHT(NPF1NR,IRNR)\*PROBTS

1132 TMEL1=PTIM1+TIME(2)/3600.0

TMEL2=PTIM2+TIME(3)/3600.0

TMEL3=PTIM3+TIME(4)/3600.0

WRITE(10=1) NTRY5,NTEST,NDC,NSIP,JOINT,ICAL,I1,I2,I3,KREC,IRAC,

1 NPF1AC,IRNR,NPF1NR,A,B,C,PROBAC,PROBNR,PRRAC,PRQAC,PRRNR,PRQNR,

2 RVALAC,RVALNR,RACBEG,SPROAC,RNBEG,SPRUNR, TMEL1,TMEL2,TMEL3

5132 CONTINUE

IF( IRAC .EQ. 0) GO TO 1126

Y1=TERPOCA(B,RVALAC,ICAL)

ADDA=ABS(RVALAC-RACBEG)\*0.5\*(SPRUAC+Y1)

PRRAC=GRIDR\*PRRAC+ADDA

PRQAC=PRQAC+WLIGHT(NUMQ,I2)\*PRRAC

1126 IF( IRNR .EQ. 0) GO TO 1131

Y1=TERPO(A,B,RVALNR,ICAL)

ADDR=ABS(RVALNR-RNRBEG)\*0.5\*(SPRUNR+Y1)

PRRNR=GRIDR\*PRRNR+ADDR

PRQNR=PRQNR+WLIGHT(NUMQ,I2)\*PRRNR

1131 CONTINUE

PRQNR=PRQNR\*GRIDQ

PRQAC=PRQAC\*GRIDQ

PROBAC=PROBAC\*WEIGHT(NUMW,I1)\*PRQAC

PROBNR=PROBNR\*WEIGHT(NUMW,I1)\*PRQNR

1130 CONTINUE

PROBNR=PROBNR\*GRIDW

PROBAC=PROBAC\*GRIDW

JOINT=ICAL

ICAL=INTER

S  
START OF

```

C      UC(NSTP,1)=PROBABILITY OF ACCEPTING AT STEP NSTP
C      UC(NSTP,2)=PROBABILITY OF REJECTING AT STEP NSTP
C      ASN(NSTP)=PROBABILITY OF CONTINUING AT STEP NSTP

      ASN(NSTP)=PROBNR-PROBAC
      UC(NSTP,1)=PROBAC
      UC(NSTP,2)=ASN(NSTP-1)-ASN(NSTP)-UC(NSTP,1)
      WRITE(11=(NSTP+((NDC-1)*NTESTS)+(KTES-1)*NTESTS*10)) UC(NSTP,1),
2      UC(NSTP,2),ASN(NSTP),NSTP,ALAM,KTEST
399  IF( NTRY5 .GT. 1 .AND. P(1M1) .LE. 0.0)
1  READ(11=(NSTP+((NDC-1)*NTESTS)+(KTES-1)*NTESTS*10))
2  UC(NSTP,1),UC(NSTP,2),ASN(NSTP),NCARE,GLAM,LOSCAS
      WRITE(7,208) NSTP,UC(NSTP,1),UC(NSTP,2),ASN(NSTP)
208  FORMAT(5X,15,5X,E20.10,5X,E20.10,5X,E20.10)

400  CONTINUE
C
C      THIS PART OF THE PROGRAM CALCULATES
C      E(NJALAM)=AVERAGE SAMPLE NUMBER WHEN LAMDA=ALAM
C      AND
C      M(NJALAM)=MEDIAN SAMPLE NUMBER WHEN LAMDA=ALAM
C      AS WELL AS
C      UC(ALAM)=PROB( REJECTING H0 | LAMDA=ALAM )
C      B(ALAM)=1-UC(ALAM)
C
      OCF=0.0
      AVR=1.0
      POW=0.0
      TMED=0.0
      DO 490 IN=1,MIP
      AVR=AVR+ASN(IN)
      OCF=OCF+UC(IN,1)
      POW=POW+UC(IN,2)
      TES=IN-1.0-AVR
      IF(TES .LT. 0.5 .OR. ( TMED .GT. 0.0 .AND. TES .GT. 0.5))GO TO 490
      TMED=IN
      IF(TES .GT. 0.5) TMED=IN-0.5
490  CONTINUE
      WRITE(IRITE,209) ALAM, TMED, AVR, OCF, POW
209  FORMAT(5X,F6.4,9X,F6.2,8X,F6.4,8X,F6.4,8X,F6.4)
500  CONTINUE
9112 CONTINUE
9113 CONTINUE
      WRITE(8,9117) IRP1,IRP2
9117  FORMAT(1H1,20X,"MISTAKES IN THEORY",18,5X,18)
      STOP
      END

```

THE SUBROUTINES CALLED FOLLOW

SUBROUTINE FSTEPROB(PACC,PREJ,PCON,N)

START OF SEGMENT

C		0003690
C		0003700
C	THIS SUBROUTINE CALCULATES	0003710
C	THE PROBABILITIES OF ACCEPTING, REJECTING,	0003720
C	AND CONTINUING FOR STEPS	0003730
C	FOR STEPS LESS THAN AND EQUAL TO THE FIRST	0003740
C	STEP AT WHICH A DECISION CAN BE MADE	0003750
C	THIS IS ACCOMPLISHED BY MEANS OF AN INFINITE	0003760
C	SUM OF INCOMPLETE BETA FUNCTIONS	0003770
C		0003780
	COMMON /CB4/DEGF,ALAM	0003790
	COMMON /CB5/ REG(30,2)	0003800
	DO 50 IB=1,2	0003810
	TSUM=0.0	0003820
	IF( IB .EQ. 1 .AND. REG(N,1) .LE. 0.0) GO TO 30	0003830
	IF( IB .EQ. 2 .AND. REG(N,2) .GE. 1.E6) GO TO 30	0003840
	F0=((DEGF*(FLOAT(N)-1.))/(DEGF-1.))*REG(N,IB)	0003850
	U0=1.0/(1.0+(((DEGF-1.0)/(DEGF*(FLOAT(N)-1.)))*F0))	0003860
	W1=(DEGF*(FLOAT(N)-1.))*0.5	0003870
	W2=(DEGF-1.)*0.5	0003880
	TSUM=BETINC(U,W1,W2,U0)	0003890
	IF( ALAM .LE. 0.0) GO TO 20	0003900
	DO 10 JR=1,101	0003910
	W2=((DEGF-1.)*0.5)+FLOAT(JR)	0003920
	TOT=(FLOAT(JR)*ALOG(0.5*FLOAT(N)*ALAM))+ALOG(BETINC(U,W1,W2,U0))	0003930
	1 ) -ALGAMA(FLOAT(JR+1))	0003940
	TOT=EXP(TOT)	0003950
	TSUM=TSUM+TOT	0003960
	IF( TOT .LE. 1.E-06) GO TO 20	0003970
10	CONTINUE	0003980
20	TSUM=TSUM*EXP(-.5*FLOAT(N)*ALAM)	0003990
30	IF( IB .GT. 1) GO TO 40	0004000
	PACC=1.-TSUM	0004010
	GO TO 50	0004020
40	PREJ=TSUM	0004030
50	CONTINUE	0004040
51	PCON=1.-PACC-PREJ	0004050
	RETURN	0004060
	END	0004070

SEGMENT

START OF SEGMENT

	FUNCTION BETINC(IND,A,B,X)	00040800
C	INCOMPLETE BETA FUNCTION AND ITS INVERSE	00040900
C	MARK=1 FOR INVERSE (SEND DOWN PROB)	00041000
C		00041100
C	THIS SUBFUNCTION CALCULATES THE INCOMPLETE BETA FUNCTION	00041200
C	THIS IS NEEDED TO CALCULATE THE PA,PR,PC AT THE FIRST STEP	00041300
C	A DECISION CAN BE MADE	00041400
C		00041500
	CAB=CGAM(A+B)-CGAM(A)-CGAM(B)-.5*ALOG((A+B)*6.28318531)	00041600
	IF(IND)10,10,20	00041700
10	EP=CAB+A*ALOG(X*(1.+B/A))+B*ALOG((1.-X)*(1.+A/B))	00041800
	IF(X-A/(A+B))12,12,14	00041900
12	BETINC=Z1(X,A,B)*EXP(EP+.5*ALOG(B/A))	00042000
	RETURN	00042100
14	BETINC=1.-Z1(1.-X,B,A)*EXP(EP+.5*ALOG(A/B))	00042200
	RETURN	00042300
20	IF(X=.5)22,22,24	00042400
22	QZ=ALOG(X)	00042500
	IG0=1	00042600
	AA=A	00042700
	BB=B	00042800
	GO TO 26	00042900
24	QZ=ALOG(1.-X)	00043000
	IG0=2	00043100
	AA=B	00043200
	BB=A	00043300
26	XT=AA/(AA+BB)	00043400
	CABB=CAB+.5*ALOG(BB/AA)+AA*ALOG(1.+BB/AA)+BB*ALOG(1.+AA/BB)	00043500
	DO 40 NC=1,100	00043600
	ZZ=Z1(X1,AA,BB)	00043700
	QX=CABB+AA*ALOG(XT)+BB*ALOG(1.-XT)+ALOG(ZZ)	00043800
	XC=(QZ-QX)*(1.-XT)*ZZ/AA	00043900
	XC=AMAX1(XC,-.99)	00044000
	XC=AMIN1(XC,.5/XT-.5)	00044100
	XT=XT*(1.+XC)	00044200
	IF(ABS(XC)-1.E-6)42,40,40	00044300
40	CONTINUE	00044400
42	GO TO (44,46),IG0	00044500
44	BETINC=XT	00044600
	RETURN	00044700
46	BETINC=1.-XT	00044800
	RETURN	00044900
	END	00045000

SEGMENT

SUBROUTINE BOOK (L1,L2,L3,LN,WN,QN,RN)

START OF SEGMENT

THIS SUBROUTINE IS A BOOK KEEPING ROUTINE

THIS ROUTINE CONVERTS A POINT IN THE GRID F(W,Q,R) TO  
A POINT IN THE RANDOM ACCESS DISK FILE  
THE POINT IN THAT FILE FOR A PARTICULAR POINT  
IS TERMED JREC

COMMON /CB2/JREC,TSIAT  
COMMON /CB1/GRIDW,GRIDQ,GRIDR  
COMMON /CB3/NCUNW,NCUNQ,NCSTR  
COMMON /CB12/NUMW,NUMQ,NUMR

WN=(L1-1+NCUNW)\*GRIDW

QN=(L2-1+NCUNQ)\*GRIDQ

ENTRY RCAL(L1,L2,L3,LN,WN,QN,RN)

RN=(IFIX((WN\*\*2.+QN\*\*2.)/(NCSTR\*GRIDR))+L3)\*GRIDR

IF(LN.LE.0) GO TO 10

ENTRY CRITV(WN,QN,RN,LN)

DBLCHK=((LN\*RN)-(WN\*\*2.)-(QN\*\*2.))\*2.0

IF(DBLCHK.LE.0.0) GO TO 5

TSTAT=((WN-QN)\*\*2.0)/DBLCHK

RETURN

TSTAT=1.0 L20

RETURN

ENTRY JENT(L1,L2,L3,WN,QN,RN)

L1=(WN/GRIDW)+1-NCUNW

L2=(QN/GRIDQ)+1-NCUNQ

L3=(RN/GRIDR)-IFIX((WN\*\*2.+QN\*\*2.)/(NCSTR\*GRIDR))

SZCHK=L1+((L2-1)\*NUMW)+((L3-1)\*NUMW\*NUMQ)

IF(ABS(SZCHK).LT.549755813886) GO TO 30

JREC=541111111111

RETURN

JREC=IFIX(SZCHK)

RETURN

JREC=L1+((L2-1)\*NUMW)+((L3-1)\*NUMW\*NUMQ)

RETURN

END

SEGMENT

FUNCTION POSPROB(NV,QV,RV,N)

START OF SEGMENT

THIS IS A FUNCTION TO DETERMINE IF  
A POINT IS ALLOWABLE AT STEP N

POSPROB=RV-((NV\*\*2.+QV\*\*2.)/FLOAT(N))  
IF(ABS(POSPROB) .LE. 1.E-4) POSPROB=0.0  
RETURN  
END

00034400  
00034500  
00034600  
00034700  
00034800  
00034900  
00035000  
00035100  
00035200  
SEGMENT

FUNCTION PHI(Y,XBAR,SIG)

START OF SEGMENT

THIS SUBFUNCTION CALCULATES THE NORMAL DENSITY FUNCTION

PHI=0.39894228\*EXP(-.5\*(((Y-XBAR)/SIG)\*\*2.))\* (1./SIG)  
RETURN  
END

00035300  
00035400  
00035500  
00035600  
00035700  
00035800  
00035900  
SEGMENT

FUNCTION CHISQ(Y,DOF)

START OF SEGMENT

THIS SUBFUNCTION CALCULATES THE CHISQUARE DENSITY FUNCTION

CHISQ = ((Y\*\*((DOF/2.)-1.))\*EXP(-Y/2.))/((2.\*\*((DOF/2.))  
1 \* GAMMA(DOF/2.0))  
IF( Y .EQ. 0.0 .AND. DOF .EQ. 2.0) CHISQ=0.5  
RETURN  
END

00036000  
00036100  
00036200  
00036300  
00036400  
00036500  
00036600  
00036700  
00036800  
SEGMENT

FUNCTION DENSTS(A,B,C,KREC)

C-15

START OF SEGMENT

C		00052400
C	THIS SUBROUTINE CALCULATES FN(A,B,C)	00052500
C	FROM G(A-Z,R-U,R-Z**2-U**2)*P(U)*P(Z)	00052600
C	BY INTEGRATING OVER THE APPROPRIATE REGIONS	00052700
	COMMON /CB1/ GRIDW,GRIDQ,GRIDR	00052800
	COMMON /CB6/ TMAXW,TMINW,TMAXQ,TMINQ	00052900
	COMMON /CB7/ LSTP,ISUR	00053000
	COMMON /CB8/ JOINT,ICAL	00053100
	COMMON /CB9/ NIP,RINT,CUR	00053200
	COMMON /CB5/ REG(30,2)	00053300
	DIMENSION POINT(4,4),FVAL(4),RINT(5,4)	00053400
	VOLUME=0.0	00053500
C		00053600
C	THIS NUMERICAL INTEGRATION INVOLVES SUMMING THE VOLUMES	00053700
C	OF TRAPEZOIDSC	00053800
C	U=ODIMENSION = MEAN Z	00053900
C	Z= N DIMENSION = MEAN 1	00054000
C		00054100
	CALL DROUND(A,B,C,REG(LSTP,1),REG(LSTP,2),NREG,RINT)	00054200
	IF( NREG .EQ. 0) GO TO 230	00054300
	DO 229 NIP=1,NREG	00054400
	CALL ZRANGE(RINT(NIP,1),RINT(NIP,3),RINT(NIP,4),TMX,TMIN)	00054500
	USTRT= (IFIX(RINT(NIP,1)/GRIDW)+1)*GRIDW	00054600
	IF(RINT(NIP,1) .LT. 0.0 .AND. RINT(NIP,1) .NE. (USTRT-GRIDW))	00054700
	1 USTRT=IFIX(RINT(NIP,1)/GRIDW)*GRIDW	00054800
	UFIN=IFIX(RINT(NIP,2)/GRIDW)*GRIDW	00054900
	IF(RINT(NIP,2) .LT. 0.0) UFIN=(IFIX(RINT(NIP,2)/GRIDW)-1)*GRIDW	00055000
	IF( UFIN .EQ. RINT(NIP,2)) UFIN=UFIN-GRIDW	00055100
	IF( UFIN .LE. USTRT ) GO TO 220	00055200
	IF( LSTP .EQ. ISUR) GO TO 157	00055300
	IF( (B-UFIN) .GT. TMAXQ .AND. (B-USTRT) .GT. TMAXQ) GO TO 220	00055400
	IF( (B-UFIN) .LT. TMINQ .AND. (B-USTRT) .LT. TMINQ) GO TO 220	00055500
	IF( (B-USTRT) .LT. TMINQ) USTRT=B-TMINQ	00055600
	IF( (B-USTRT) .GT. TMAXQ) USTRT=B-TMAXQ	00055700
	IF( (B-UFIN) .LT. TMINQ) UFIN=B-TMINQ	00055800
	IF( (B-UFIN) .GT. TMAXQ) UFIN=B-TMAXQ	00055900
	IF( USTRT .GE. UFIN ) GO TO 220	00056000
157	U1=USTRT	00056100
	U2=USTRT+GRIDW	00056200
	CALL ZRANGE(U1,RINT(NIP,3),RINT(NIP,4),ZMAX1,ZMIN1)	00056300
	POINT(1,1)=RINT(NIP,1)	00056400
	POINT(1,2)=TMX	00056500
	POINT(2,1)=U1	00056600
	POINT(2,2)=ZMAX1	00056700
	POINT(3,1)=RINT(NIP,1)	00056800
	POINT(3,2)=TMIN	00056900
	IF( TMX .EQ. TMIN) GO TO 158	00057000
	POINT(4,1)=U1	00057100
	POINT(4,2)=ZMIN1	00057200
	CUR=RINT(NIP,3)	00057300
	CALL RESVOL(A,B,C,VOLUME,4,4,POINT,FVAL)	00057400
	VOLUME=VOLUME+	00057500
	Z(AREA(RINT(NIP,4),A-POINT(4,2),B-POINT(4,1),RINT(NIP,4),A-POINT(3,	00057600
	52),B-POINT(3,1))*(FVAL(3)+FVAL(4))*0.5)	00057700
	NSIDES=4	00057800
	GO TO 159	00057900
158	POINT(3,1)=U1	00058000
	POINT(3,2)=ZMIN1	00058100
	CALL RESVOL(A,B,C,VOLUME,3,3,POINT,FVAL)	00058200
	NSIDES=3	00058300
159	ZBEG1= IFIX(ZMIN1/GRIDQ)*GRIDQ	00058400
	ZFIN1=IFIX( ZMAX1/GRIDQ)*GRIDQ	00058500
		00058600

160	CALL 7RANGE(U2,RINT(NIP,3),RINT(NIP,4),ZMAX2,ZMIN2)	00058900
	ZBEG2=IFIX(ZMIN2/GRIDQ)*GRIDQ	00059000
	ZFIN2=IFIX(ZMAX2/GRIDQ)*GRIDQ	00059100
	IF(ZMIN2.GT.0.0) ZBEG2=(IFIX(ZMIN2/GRIDW)+1)*GRIDW	00059200
	IF(ZMAX2.LT.0.0) ZFIN2=(IFIX(ZMAX2/GRIDW)-1)*GRIDW	00059300
	ZBEG=AMAX1(ZBEG1,ZBEG2)	00059400
	ZFIN=AMIN1(ZFIN1,ZFIN2)	00059500
	IF(ZBEG.GE.ZFIN) GO TO 197	00059600
	IF(LSTP.EQ.ISUR) GO TO 168	00059700
	IF((A-ZBEG).GT.TMAXW.AND.(A-ZFIN).GT.TMAXW) GO TO 197	00059800
	IF((A-ZBEG).LT.TMINW.AND.(A-ZFIN).LT.TMINW) GO TO 197	00059900
	IF((A-ZBEG).LT.TMINW) ZBEG=A-TMAXW	00060000
	IF((A-ZBEG).LT.TMINW) ZBEG=A-TMINW	00060100
	IF((A-ZFIN).GT.TMAXW) ZFIN=A-TMAXW	00060200
	IF((A-ZFIN).LT.TMINW) ZFIN=A-TMINW	00060300
	IF(ZBEG.GE.ZFIN) GO TO 197	00060400
168	ZINT=ZBEG	00060500
170	Y1=TERPUS(U1,ZINT)	00060600
	Y2=TERPUS(U2,ZINT)	00060700
1178	IF(ZINT.NE.ZBEG.AND.ZINT.NE.ZFIN) GO TO 180	00060800
	ZDET=ZMIN2	00060900
	NPFI=1	00061000
	IF(ZINT.NE.ZBEG.OR.U1.NE.USTRT) GO TO 174	00061100
	UBFU=U1	00061200
	ZBFU=ZMAX1	00061300
	FBFU=FVAL(2)	00061400
	CUR=RINT(NIP,4)	00061500
	IF(NSIDES.EQ.3) GO TO 173	00061600
	POINT(2,1)=POINT(4,1)	00061700
	POINT(2,2)=POINT(4,2)	00061800
	FVAL(2)=FVAL(4)	00061900
	GO TO 176	00062000
173	POINT(2,1)=U1	00062100
	POINT(2,2)=ZMIN1	00062200
	FVAL(2)=FVAL(3)	00062300
	IF(POINT(3,1).NE.U1.OR.POINT(3,2).NE.ZMIN1)	00062400
	1 FVAL(2)=TERPUS(U1,ZMIN1)	00062500
	IF(POINT(2,1).NE.U1.OR.POINT(2,2).NE.ZMAX1)	00062600
	2 FBFU=TERPUS(U1,ZMAX1)	00062700
	GO TO 176	00062800
174	IF(ZINT.NE.ZBEG) GO TO 175	00062900
	POINT(2,1)=UBFL	00063000
	POINT(2,2)=ZBFL	00063100
	FVAL(2)=FVFL	00063200
	CUR=RINT(NIP,4)	00063300
	GO TO 176	00063400
175	POINT(2,1)=UBFU	00063500
	POINT(2,2)=ZBFU	00063600
	FVAL(2)=FBFU	00063700
	ZDET=ZMAX2	00063800
	CUR=RINT(NIP,3)	00063900
176	POINT(1,1)=U2	00064000
	POINT(1,2)=ZDET	00064100
	POINT(3,1)=U2	00064200
	POINT(3,2)=ZINT	00064300
	FVAL(3)=Y2	00064400
	POINT(4,1)=U1	00064500
	POINT(4,2)=ZINT	00064600
	FVAL(4)=Y1	00064700
	NSIDES=4	00064800
	CALL RESVOL(A,B,C,VOLUME,NSIDES,NPFI,POINT,FVAL)	00064900
	IF(ZINT.NE.ZBEG) GO TO 177	00065000
	UBFL=POINT(1,1)	00065100

	GO TO 178	C-17	00065400
177	UBFU=POINT(1,1)		00065500
	ZBFU=POINT(1,2)		00065600
	FBFU=FVAL(1)		00065700
178	VOLUME=VOLUME+GRIDW*GRIDQ*1.5*(1.0/6.0)*(Y1+Y2)		00065800
	IF(ZINT.EQ.ZFIN) GO TO 200		00065900
	GO TO 190		00066000
180	VOLUME=VOLUME+(1.0/5.0)*GRIDQ*GRIDW*3.0*(Y1+Y2)		00066100
190	ZINT=ZINT+GRIDQ		00066200
	IF(ZINT.LE.ZFIN) GO TO 170		00066300
	GO TO 200		00066400
197	IF( (ZMAX2.EQ.ZMIN2).AND.U2.EQ.UFIN) GO TO 201		00066500
	POINT(1,1)=U1		00066600
	POINT(1,2)=ZMAX1		00066700
	POINT(2,1)=U2		00066800
	POINT(2,2)=ZMAX2		00066900
	POINT(3,1)=U1		00067000
	POINT(3,2)=ZMIN1		00067100
	POINT(4,1)=U2		00067200
	POINT(4,2)=ZMIN2		00067300
	CUR=RINT(NIP,3)		00067400
	CALL RESVOL(A,B,C,VOLUME,4,4,POINT,FVAL)		00067500
	VOLUME=VOLUME+		00067600
	Z(CAREA(RINT(NIP,4),A=POINT(4,2),B=POINT(4,1),RINT(NIP,4),A=POINT(3,1),B=POINT(3,1))*(FVAL(3)+FVAL(4))*0.5)		00067700
	UBFU=U2		00067800
	ZBFU=ZMAX2		00067900
	FBFU=FVAL(2)		00068000
	UBFL=U2		00068100
	ZBFL=ZMIN2		00068200
	FBFL=FVAL(4)		00068300
200	U1=U2		00068400
	U2=U2+GRIDW		00068500
	ZBEG1=ZBEG2		00068600
	ZFIN1=ZFIN2		00068700
	ZMIN1=ZMIN2		00068800
	ZMAX1=ZMAX2		00068900
	IF( U2 .LE. UFIN) GO TO 180		00069000
201	CALL ZRANGE(RINT(NIP,2),RINT(NIP,3),RINT(NIP,4),TMX,TMIN)		00069100
	POINT(1,1)=RINT(NIP,2)		00069200
	POINT(1,2)=TMX		00069300
	POINT(2,1)=U1		00069400
	POINT(2,2)=ZMAX1		00069500
	POINT(3,1)=RINT(NIP,2)		00069600
	POINT(3,2)=TMIN		00069700
	IF(TMX.EQ.TMIN) GO TO 219		00069800
	POINT(4,1)=U1		00069900
	POINT(4,2)=ZMIN1		00070000
	CUR=RINT(NIP,3)		00070100
	CALL RESVOL(A,B,C,VOLUME,4,4,POINT,FVAL)		00070200
	VOLUME=VOLUME+		00070300
	Z(CAREA(RINT(NIP,4),A=POINT(4,2),B=POINT(4,1),RINT(NIP,4),A=POINT(3,1),B=POINT(3,1))*(FVAL(3)+FVAL(4))*0.5)		00070400
	GO TO 229		00070500
219	POINT(3,1)=U1		00070600
	POINT(3,2)=ZMIN1		00070700
	CALL RESVOL(A,B,C,VOLUME,3,3,POINT,FVAL)		00070800
	GO TO 229		00070900
220	UINI=(RINT(NIP,2)-RINT(NIP,1))*0.5+RINT(NIP,1)		00071000
	NTC=1		00071100
	CALL ZRANGE(POINT,RINT(NIP,3),RINT(NIP,4),ZX,ZM)		00071200
221	IF( TMX .EQ. TMIN) GO TO 222		00071300
	NSIDES=4		00071400
	POINT(1,1)=RINT(NIP,NTC)		00071500
			00071600
			00071700
			00071800

	POINT(2,1)=UINI	0007190
	POINT(2,2)=ZX	0007200
	POINT(3,1)=RINT(NIP,NTC)	0007210
	POINT(3,2)=TMIN	0007220
	POINT(4,1)=UINI	0007230
	POINT(4,2)=ZM	0007240
	CUR=RINT(NIP,3)	0007250
	CALL RESVOL(A,B,C,VOLUME,NSIDES,4,POINT,FVAL)	0007260
	VOLUME=VOLUME+	0007270
	2(AR1A(PINT(NIP,4),A-POINT(4,2),B-POINT(4,1),RINT(NIP,4),A-POINT(3,	0007280
	52),B-POINT(3,1)))+(FVAL(3)+FVAL(4))*0.5)	0007290
	GO TO 223	0007300
222	NSIDES=3	0007310
	POINT(1,1)=RINT(NIP,NTC)	0007320
	POINT(1,2)=TMX	0007330
	POINT(2,1)=UINI	0007340
	POINT(2,2)=ZX	0007350
	POINT(3,1)=UINI	0007360
	POINT(3,2)=ZM	0007370
	CALL RESVOL(A,B,C,VOLUME,NSIDES,3,POINT,FVAL)	0007380
223	IF(NTC.GE. 2) GO TO 229	0007390
	CALL ZRANGE(RINT(NIP,2),RINT(NIP,3),RINT(NIP,4),TMX,TMIN)	0007400
	NTC=NTC+1	0007410
	GO TO 221	0007420
229	CONTINUE	0007430
230	DENSIS=VOLUME	0007440
	WRITE(ICAL=KKLC) VOLUME	0007450
	RETURN	0007460
	END	0007470

SEGMENT

## FUNCTION CGAM(A)

START OF SEGMENT

C		00046700
C	THIS SUBROUTINE IS NEEDED FOR THE INCOMPLETE BETA FUNCTION CALC	00046800
C		00046900
	AA=A	00047000
	CAC=0.0	00047100
	IF(A=2.)2,8,8	00047200
2	IF(A=1.)4,6,6	00047300
4	CAC=-2.+(A+.5)*ALOG(1.+1./A)+(A+1.5)*ALOG(1.+1./(A+1.))	00047400
	AA=A+2.	00047500
	GO TO 8	00047600
6	CAC=-1.+(A+.5)*ALOG(1.+1./A)	00047700
	AA=A+1.	00047800
8	CA=2.269489/AA	00047900
	CA=.52560647/(AA+1.0115231/(AA+1.5174737/(AA+CA)))	00048000
	CA=.0833333333/(AA+.03333333/(AA+.25238095/(AA+CA)))	00048100
	CGAM=CA+CAC	00048200
	RETURN	00048300
	END	00048400
		00048500

SEGMENT

```

SUBROUTINE UBOUND( A,B,C,VAN,VRN,NREG,RINT)      00074800
COMMON /CB7/ NSTP                                00074900
COMMON /CB10/ CA,PA,CR,PR                        00075000
COMMON /CB11/ SINE45                             00075100
DIMENSION RINT(5,5)                             00075200
C      THIS SUBROUTINE CALCULATES THE INTEGRATION 00075300
C      LIMITS OF U, AND ALSO DETERMINES THE      00075400
C      NUMBER OF INTEGRATION REGIONS AND TYPE    00075500
C      SO AS TO ALLOW DETERMINATION OF THE Z RANGE 00075600
C      THESE ARE NEEDED TO OBTAIN THE DENSITY F(W,O,R) AT STEP 00075700
C      N FROM THE DENSITY AT STEP N-1            00075800
C      THE FOLLOWING CODE IS EMPLOYED              00075900
C      1=REJECTION ELLIPSE LOWER                  00076000
C      2=REJECTION ELLIPSE UPPER                  00076100
C      3=ACCEPTANCE ELLIPSE LOWER                 00076200
C      4=ACCEPTANCE ELLIPSE UPPER                 00076300
C      5=CIRCLE LOWER                             00076400
C      6=CIRCLE UPPER                             00076500
C      RINT(1,3)= UPPER Z CURVE ( LOWER W)        00076600
C      RINT(2,4)= LOWER Z CURVE ( UPPER W)        00076700
C      TERM2(XCR,XA,XB,XPR)=(XB*(XCR+1.0)+XA*XPR)/(((XCR+1.0)**2.0)-(XPR 00076800
1 **2.0))                                          00076900
DISCR(XCR,XA,XB,XPR,XC)= SQRT((TERM2(XCR,XA,XB,XPR)**2.0)-(((XA** 00077000
1 2.0)-(XCR+1.0)*(XA**2.0+XB**2.0-XC))/((XPR**2.0)-((XCR+1.0)**2.0) 00077100
2 )))                                          00077200
IF( VAN .LE. 0.0) GO TO 5                      00077300
DA=(C-A**2.-B**2.+((.5*((A+B)**2.)*NSTP)/(NSTP+1.))+((.5*((A-B)**2. 00077400
5 ))/(CA+PA+1.0))                          00077500
IF( VRN .LE. 0.0) GO TO 7                      00077600
DR=(C-A**2.-B**2.+((.5*((A+B)**2.)*NSTP)/(NSTP+1.))+((.5*((A-B)**2. 00077700
7 ))/(CA+PA+1.0))                          00077800
IF( VAN .LE. 0.0) GO TO 60                     00077900
IF( VRN .LE. 0.0) GO TO 70                     00078000
IF( DR .LE. 0.0 .AND. DA .LE. 0.0) GO TO 15    00078100
IF( DA .LE. 0.0 .AND. DR .GT. 0.0) GO TO 60    00078200
DR1=SQRT((DR*NSTP)/(NSTP+1.0))                 00078300
DR2=SQRT(DR/(CR+PR+1.0))                       00078400
DA1= SQRT((DA*NSTP)/(NSTP+1.0))                 00078500
DA2=SQRT(DA/(CA+PA+1.0))                       00078600
HA=( SINE45 *(A+B)*NSTP)/(NSTP+1.0)            00078700
HR=(SINE45 *(A+B)*NSTP)/(NSTP+1.0)            00078800
TKA=(SINE45 *(A-B))/(CA+PA+1.0)                00078900
TKR=(SINE45 *(A-B))/(CR+PR+1.0)                00079000
CHK=.5*((A+B)*NSTP)**2.0-NSTP*(NSTP+1.)*(A**2.+B**2.-C) 00079100
IF(CHK)20,10,10                                00079200
10 TLOC=((CHR-HA)**2.)/(DR1**2.))+((TKR-TKA)**2.)/(DR2**2.) -1. 00079300
IF( TLOC .GT. 0.0) GO TO 60                     00079400
TLOC=((CHR-HR)**2.)/(DA1**2.))+((TKA-TKR)**2.)/(DA2**2.) -1. 00079500
TSPEC= (((CHR-HR)**2.)/(DA1**2.))+((TKR+DR2-TKA)**2.)/(DA2**2.) -1. 00079600
IF( TLOC .LT. 0.0 .AND. TSPEC .GT. 0.0) GO TO 20 00079700
15 NREG=0                                        00079800
RETURN                                          00079900
20 CON=TERM2(CR,A,B,PR)                        00080000
QUAD=DISCR(CR,A,B,PR,C)                        00080100
QNLR=CON-QUAD                                   00080200
QNUR=CON+QUAD                                   00080300
QUAD=DISCR(CA,A,B,PA,C)                        00080400
CON=TERM2(CA,A,B,PA)                           00080500
QNLA=CON-QUAD                                   00080600
QNUA=CON+QUAD                                   00080700
IF(CHK) 30,30,40                               00080800
30 NREG=4                                       00080900
RINT(1,1)=B-QNLA                               00081000
                                           00081100

```

RINT(1,3)=2.

C-20

00081200

RINT(1,4)=1.

00081300

RINT(2,1)=B-QNUA

00081400

RINT(2,2)=B-QNLA

00081500

RINT(2,3)=4.

00081600

RINT(2,4)=2.

00081700

RINT(3,1)=RINT(2,1)

00081800

RINT(3,2)=RINT(2,2)

00081900

RINT(3,3)=3.

00082000

RINT(3,4)=1.

00082100

RINT(4,1)=B-QNUR

00082200

RINT(4,2)=B-QNUA

00082300

RINT(4,3)=2.

00082400

RINT(4,4)=1.

00082500

RETURN

00082600

40 NREG=5

00082700

RINT(1,1)=B-QNLA

00082800

RINT(1,2)=B-QNLR

00082900

RINT(1,3)=2.

00083000

RINT(1,4)=1.

00083100

RINT(2,1)=B-QNLA

00083200

RINT(2,2)=B-QNLA

00083300

RINT(2,3)=2.

00083400

RINT(2,4)=4.

00083500

RINT(5,1)=B-QNUR

00083600

RINT(5,2)=B-QNUA

00083700

RINT(5,3)=2.

00083800

RINT(5,4)=1.

00083900

CON= SINE45 \*(A+B)\*NSTP

00084000

QUAD=SQRT(CNR)

00084100

QN1=(1./(NSTP+1.))\*(CON+QUAD)\* SINE45

00084200

QN2=(1./(NSTP+1.))\*(CON-QUAD)\*SINE45

00084300

RINT(3,1)=B-QN1

00084400

RINT(3,2)=B-QNLA

00084500

RINT(4,1)=B-QNLA

00084600

RINT(4,2)=B-QN2

00084700

IF(1KR .LT. 1KA) GO TO 50

00084800

RINT(3,3)=3.

00084900

RINT(3,4)=1.

00085000

RINT(4,3)=3.

00085100

RINT(4,4)=1.

00085200

RETURN

00085300

50 RINT(3,3)=1.

00085400

RINT(3,4)=3.

00085500

RINT(4,3)=1.

00085600

RINT(4,4)=3.

00085700

RETURN

00085800

60 IF( DR .LE. 0.0) GO TO 15

00085900

NREG=1

00086000

CON=TERMZ(CR,A,B,PR)

00086100

QUAD=DISCR(CR,A,B,PR,C)

00086200

QNLR=CON-QUAD

00086300

QNUR=CON+QUAD

00086400

RINT(1,1)=B-QNUR

00086500

RINT(1,2)=B-QNLR

00086600

RINT(1,3)=2.

00086700

RINT(1,4)=1.

00086800

RETURN

00086900

70 IF(DA .GT. 0.0) GO TO 80

00087000

NREG=1

00087100

RINT(1,1)=- SQRT(C)

00087200

RINT(1,2)=SQRT(C)

00087300

RINT(1,3)=6.

00087400

RINT(1,4)=5.

00087500

80	NREG=4	00087700
	CON=TERM2(CA,A,B,PA)	00087800
	QUAD=DISCR(CA,A,B,PA,C)	00087900
	QNLA=CON-QUAD	00088000
	QNUA=CON+QUAD	00088100
	RINT(1,1)=B-QNLA	00088200
	RINT(1,2)=SQRT(C)	00088300
	RINT(1,3)=6.	00088400
	RINT(1,4)=5.	00088500
	RINT(2,1)=B-QNUA	00088600
	RINT(2,2)=B-QNLA	00088700
	RINT(2,3)=6.	00088800
	RINT(2,4)=4.	00088900
	RINT(3,1)=B-QNUA	00089000
	RINT(3,2)=B-QNLA	00089100
	RINT(3,3)=3.	00089200
	RINT(3,4)=5.	00089300
	RINT(4,1)=SQRT(C)	00089400
	RINT(4,2)=B-QNUA	00089500
	RINT(4,3)=6.	00089600
	RINT(4,4)=5.	00089700
	RETURN	00089800
	END	00089900
		SEGMENT

		START OF SEGMENT
	FUNCTION Z1(X,A,B)	00045100
C		00045200
C	THIS SUBROUTINE IS NEEDED FOR THE INCOMPLETE BETA FUNCTION CALC	00045300
C		00045400
	FN=.7*(ALOG(15.+(A+B))**2+AMAX1(X*(A+B)-A,0.0)	00045500
	N=INT(FN)	00045600
	C=1.-(A+B)*X/(A+2.*FN)	00045700
	ZI=2./(C+SQRT(C**2-4.*FN*(FN-B)*X/(A+2.*FN)**2))	00045800
	DO 60 J=1,N	00045900
	FN=FN+1-J	00046000
	A2N=A+2.*FN	00046100
	ZI=(A2N-2.)*(A2N-1.-FN*(FN-B)*X/ZI/A2N)	00046200
	ZI=1./(1.-(A+FN-1.)*(A+FN-1.+B)*X/ZI)	00046300
60	CONTINUE	00046400
	RETURN	00046500
	END	00046600
		SEGMENT

## C-22

	SUBROUTINE RESVOL(A,B,C,VOLUME,NSIDES,NPNTBT,POINT,FVAL)	00093000
	COMMON /CB9/NIP,RINT,CUR	00093400
	COMMON /CB1/ GRIDW,GRIDQ,GRIDR	00093500
	DIMENSION POINT(4,4),FVAL(4),RINT(5,4),S(4)	00093600
	TLINE(X1,Y1,X2,Y2,X)=((Y2-Y1)*(X-X1)/(X2-X1))+Y1	00093700
		00093800
	DO 10 IP=1,NPNTBT	00093900
	FVAL(IP)=TERPOS(POINT(IP,1),POINT(IP,2))	00094000
10	CONTINUE	00094100
	GO TO (40,40,20,30),NSIDES	00094200
20	PIEC1=AREA(RINT(NIP,3),A-POINT(1,2),B-POINT(1,1),RINT(NIP,3),A-	00094300
1	POINT(2,2),B-POINT(2,1))	00094400
	PIEC2=AREA(RINT(NIP,4),A-POINT(1,2),B-POINT(1,1),RINT(NIP,4),A-	00094500
1	POINT(3,2),B-POINT(3,1))	00094600
	VOLUME=VOLUME+(PIEC1*(FVAL(1)+FVAL(2))+PIEC2*(FVAL(1)+FVAL(3)))*.5	00094700
	CURQ=IFIX(((POINT(2,2)-POINT(3,2))*0.5+POINT(3,2))/GRIDQ)*GRIDQ	00094800
	FIMP=TERPOS(POINT(2,1),CURQ)	00094900
	DO 21 I=1,2	00095000
	DO 21 J=1,3	00095100
	IF(FVAL(I).GE.FVAL(J)) GO TO 21	00095200
	AIN1=FVAL(I)	00095300
	FVAL(I)=FVAL(J)	00095400
	FVAL(J)=AIN1	00095500
	AIN1=POINT(I,1)	00095600
	AIN2=POINT(I,2)	00095700
	POINT(I,1)=POINT(J,1)	00095800
	POINT(I,2)=POINT(J,2)	00095900
	POINT(J,1)=AIN1	00096000
	POINT(J,2)=AIN2	00096100
21	CONTINUE	00096200
	S(1)=SQRT(((POINT(1,1)-POINT(2,1))*2.)+((POINT(1,2)-POINT(2,2))	00096300
1	**2.0))	00096400
	S(2)=SQRT(((POINT(1,1)-POINT(3,1))*2.)+((POINT(1,2)-POINT(3,2))	00096500
1	**2.0))	00096600
	S(3)=SQRT(((POINT(2,1)-POINT(3,1))*2.)+((POINT(2,2)-POINT(3,2))	00096700
1	**2.0))	00096800
	SPER=0.5*(S(1)+S(2)+S(3))	00096900
	BSAREA=(SPER*(SPER-S(1))*(SPER-S(2))*(SPER-S(3)))	00097000
	IF(BSAREA.LE.0.0) BSAREA=0.0	00097100
	BSAREA=SQRT(BSAREA)	00097200
		00097300
	IF(FVAL(1).LE.0.0) GO TO 25	00097400
	RVOL=((FVAL(1)-FVAL(2)+FVAL(1)-FVAL(3))*BSAREA)/3.0	00097500
	VOLUME=VOLUME+((BSAREA*FVAL(1))-RVOL)	00097600
25	EXTRA=(BSAREA+PIEC1+PIEC2)*(FIMP-AMIN1(FVAL(1),FVAL(2),FVAL(3)))	00097700
1	* 0.5	00097800
	EXTRA=AMAX1(0.0,EXTRA)	00097900
	VOLUME=VOLUME+EXTRA	00098000
40	RETURN	00098100
30	H=ABS(POINT(1,1)-POINT(2,1))	00098200
	IF(POINT(1,1).EQ.POINT(2,1).OR.POINT(3,1).EQ.POINT(4,1))	00098300
1	RETURN	00098400
	B1=0.5*ABS(POINT(2,2)-POINT(4,2))*(FVAL(2)+FVAL(4))	00098500
	BP=0.5*ABS(POINT(1,2)-POINT(3,2))*(FVAL(1)+FVAL(3))	00098600
	X=0.5*(POINT(2,1)-POINT(1,1))+POINT(1,1)	00098700
	Y1=TLINE(POINT(1,1),POINT(1,2),POINT(2,1),POINT(2,2),X)	00098800
	Z1=TLINE(POINT(1,1),FVAL(1),POINT(2,1),FVAL(2),X)	00098900
	X=0.5*(POINT(4,1)-POINT(3,1))+POINT(3,1)	00099000
	Y2=TLINE(POINT(3,1),POINT(3,2),POINT(4,1),POINT(4,2),X)	00099100
	Z2=TLINE(POINT(3,1),FVAL(3),POINT(4,1),FVAL(4),X)	00099200
	BH=ABS(Y1-Y2)	00099300
	BMID=0.5*BH*(Z1+Z2)	00099400
		00099500

VOLUME=VOLUME+

00099600

1 (AREA(CUR,A-POINT(2,2),B-POINT(2,1),CUR,A-POINT(1,2),B-POINT(1,1)))00099700

2 \*(FVAL(1)+FVAL(2))\*0.5)00099800

RETURN00099900

END00100000

SEGMENT

SUBROUTINE ZRANGE(UVAL,TCL,TCU,ZMAX,ZMIN)  
COMMON /CB10/CA,PA,CR,PR,A,B,C

START OF SEGMENT

00090000

00090100

00090200

00090300

THIS SUBROUTINE CALCULATES THE Z INTEGRATION LIMITS  
FOR A GIVEN U VALUE

00090400

00090500

00090600

00090700

00090800

ELLIPS(XPR,XCR,QP,PUM)=((A+XPR\*QP)/(XCR+1.))+((-1.)\*PUM)\*

00090900

1 SQRT(FCHECK(1,(((A+XPR\*QP)/(XCR+1.))\*2.-(A\*\*2.+B\*\*2.-C-2.\*B\*QP

00091000

2 +((XCR+1.)\*(QP\*\*2.)))/(XCR+1.))))

00091100

CIRCLE(QP,PUM)=((-1.)\*PUM)\*

00091200

1 SQRT(FCHECK(2,(C-(QP\*\*2.))))

00091300

MTYP=IFIX(TCU)

00091400

LTYP=IFIX(TCL)

00091500

QNP=3-UVAL

00091600

GO TO (10,10,20,20,30,30),MTYP

00091700

ZCAL=ELLIPS(PR,CR,QNP,TCU)

00091800

GO TO 40

00091900

ZCAL=ELLIPS(PA,CA,QNP,TCU)

00092000

GO TO 40

00092100

ZCAL=CIRCLE(UVAL,TCU)

00092200

ZMAX=A-ZCAL

00092300

GO TO (50,50,60,60,70,70),LTYP

00092400

ZCAL=ELLIPS(PR,CR,QNP,TCL)

00092500

GO TO 80

00092600

ZCAL=ELLIPS(PA,CA,QNP,TCL)

00092700

GO TO 80

00092800

ZCAL=CIRCLE(UVAL,TCL)

00092900

ZMIN=A-ZCAL

00093000

RETURN

00093100

END

SEGMENT

AD-A072 641

UNION COLL AND UNIV SCHENECTADY NY INST OF ADMINISTR--ETC F/G 12/1  
AN EXACT TEST FOR THE SEQUENTIAL ANALYSIS OF VARIANCE.(U)

AUG 79 R W MILLER

N00014-77-C-0438

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AES-7906

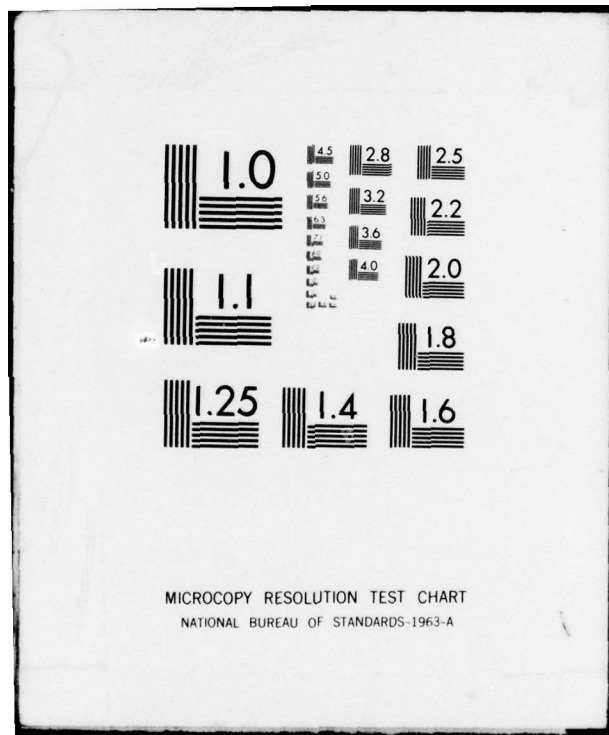
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3 OF 3

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END  
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9-79  
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FUNCTION TERPU(W,Q,R,IREAD)
C      THIS ROUTINE ESTIMATES THE DENSITY F(W,Q,R)
C      FOR POINTS NOT LYING ON THE TRIVARIATE GRID
C      THIS SUBPROGRAM PERFORMS INTERPOLATION IN
C      ONE, TWO, OR THREE DIMENSIONS
COMMON/GB1/GRIDW,GRIDQ,GRIDR
COMMON /GB3/NCNW,NCNQ,NSTRT
COMMON/GB14/XMEAN(2),XBR1,XBR2,VAR,DGF
COMMON/GB7/ LSTP,ISUR
COMMON /GB6/ IMAXW,IMINW,IMAXQ,IMINQ
COMMON /GB12/ NUMW,NUMQ,NUMR
COMMON /GB13/ QBEG,WBEG
COMMON /GB2/ JREC,TSTAT
COMMON /GB5/ REG(30,2)
COMMON /GB20/ RECMAX
DIMENSION CUORD(8,4),XVAL(10),YVAL(10)
DET2(A,B,C,D)=A*B-C*D
TERP0=0.0

IF( POSPROB(W,Q,R,LSTP+1) .LT. 0.0) RETURN
10 LB1=(W/GRIDW)+IFIX(NUMW/2)+1-IFIX((ISUR*XMEAN(1))/GRIDW)
WBEG=(LB1-1-IFIX(NUMW/2)+IFIX((ISUR*XMEAN(1))/GRIDW))*GRIDW
LB2=(Q/GRIDQ)+IFIX(NUMQ/2)+1-IFIX((ISUR*XMEAN(2))/GRIDQ)
QBEG=(LB2-1-IFIX(NUMQ/2)+IFIX((ISUR*XMEAN(2))/GRIDQ))*GRIDQ
ENTRY TERPU(W,Q,R,IREAD)
JF=2
JS=1
JI=1
NPSF=1
NPNA=0
IF(WBEG .EQ. W .AND. QBEG .EQ. Q) GO TO 15
IF(WBEG .EQ. W) GO TO 45
IF(QBEG .EQ. Q) GO TO 80
GO TO 95
15 IF((W .GT. IMAXW .OR. W .LT. IMINW)
1 .AND. (Q .GT. IMAXQ .OR. Q .LT. IMINQ)) GO TO 95
IF(W .GT. IMAXW .OR. W .LT. IMINW) GO TO 80
IF(Q .GT. IMAXQ .OR. Q .LT. IMINQ) GO TO 45

C      INTERPOLATION IN ONE DIMENSION(RN)
C      VIA 4TH DEGREE LAGRANGE
C
L4=(R/GRIDR)-IFIX(((W**2.)+(Q**2.))/(NSTRT*GRIDR))
L5=L4+2
POW=-1.0
IF(L5 .GT. NUMR) L5=NUMR
IF(L4) 16,16,17
16 L5=-1
POW=1.0
17 WN=W
QN=Q
NP=1
NTT=NUMR/2
DENS=0.0
18 DO 20 I=1,NTT
L6=L5+1+(POW*1)
IF(L6 .LE. 0 .OR. L6 .GT. NUMR) GO TO 19
CALL RCAL(0,0,L6,LSIP,WN,QN,RN)
IF( TSTAT .GE. REG(LSTP,2)) GO TO 20
CALL IENT(LJ1,LJ2,LJ3,WN,QN,RN)
READ(IREAD=JREC) YVAL(NP)
XVAL(NP)=RN
IF(NP .GE. 4) GO TO 21

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19	POW=(-1.0)*POW	0010660
	GO TO 18	0010670
21	DENS=POLY(XVAL,YVAL,R,NP)	0010680
40	IF( DENS .LT. 1.0E-35) DENS=0.0	0010690
	TERPD=DENS	0010700
	RETURN	0010710
45	IF(W .GT. TMAXW .OR. W .LT. TMINW) GO TO 95	0010720
	V1=0	0010730
C		0010740
C	TWO DIMENSIONAL INTERPOLATION (QN,RN)	0010750
C	USING A 4 POINT LATTICE FOR LAGRANGE	0010760
C	OR USING 3 POINT PLANAR IF ALL	0010770
C	POINTS ARE NOT AVAILABLE	0010780
C		0010790
	IF(QN .LT. 0.0) QBEG=QBEG-GRIDQ	0010800
	IF(QBEG .LT. TMINQ) QBEG=TMINQ+GRIDQ	0010810
	IF((QBEG+GRIDQ) .GT. TMAXQ) QBEG=TMAXQ-GRIDQ	0010820
	RBEG=IFIX(R/GRIDR)*GRIDR	0010830
47	DO 50 I1=1,JF,JS	0010840
	QN=QBEG+(I1-J1)*GRIDQ	0010850
	IF(QN .LT. TMINQ .OR. QN .GT. TMAXQ) GO TO 48	0010860
	DO 50 I2=1,JF,JS	0010870
	RN=RBEG+(I2-J1)*GRIDR	0010880
	L4=(RN/GRIDR)-IFIX(((W**2.)+(QN**2.))/(NSTRT*GRIDR))	0010890
	IF( L4 .LE. 0 .OR. L4 .GT. NUMR .OR. RN .LT. 0.0) GO TO 48	0010900
	CALL CRITV(WN,QN,RN,LSTP)	0010910
	IF(TSTAT .GE. REG(LSTP,2)) GO TO 48	0010920
	CALL IENT(JLW,JLQ,JLR,WN,QN,RN)	0010930
	READ(IREAD,JRLC) COORD(NPSF,1)	0010940
	COORD(NPSF,2)=QN	0010950
	COORD(NPSF,3)=RN	0010960
	IF(NPSF .GE. 3 .AND. NPNA .GE. 1) GO TO 60	0010970
	NPSE=NPSE+1	0010980
	GO TO 50	0010990
48	NPNA=NPNA+1	0011000
50	CONTINUE	0011010
	IF( NPSE .LE. 4) GO TO 70	0011020
	IF( JF .GT. 1) GO TO 55	0011030
	JF=4	0011040
	J1=2	0011050
	J5=2	0011060
	GO TO 47	0011070
55	RETURN	0011080
60	PLANE=DET2((COORD(2,3)-COORD(1,3))*(COORD(3,1)-COORD(1,1))+(COORD(1,3)-COORD(1,3))*(COORD(2,1)-COORD(1,1))+(V1-COORD(1,2))	0011090
	PLANE=PLANE+((DET2((COORD(2,1)-COORD(1,1))*(COORD(3,2)-COORD(1,2))+(COORD(3,1)-COORD(1,1))*(COORD(2,2)-COORD(1,2)))+(R-COORD(3,1))	0011100
	PMULT=DET2((COORD(2,2)-COORD(1,2))*(COORD(3,3)-COORD(1,3))+(COORD(3,2)-COORD(1,2))*(COORD(3,3)-COORD(1,3))+(COORD(1,2)-COORD(1,2))	0011110
	IF(PMULT .EQ. 0.0) GO TO 65	0011120
	DENS=COORD(1,1)-(PLANE/PMULT)	0011130
	GO TO 40	0011140
65	DENS=COORD(1,1)	0011150
	GO TO 40	0011160
70	DO 75 I=2,4	0011170
	IF( COORD(I,2) .NE. COORD(1,2)) X1=COORD(I,2)	0011180
	IF( COORD(I,3) .NE. COORD(1,3)) Y1=COORD(I,3)	0011190
	IF((COORD(I,2) .NE. COORD(1,2))	0011200
1	.AND. (COORD(I,3) .EQ. COORD(1,3))) F1=COORD(I,1)	0011210
	IF((COORD(I,2) .NE. COORD(1,2))	0011220
1	.AND. (COORD(I,3) .NE. COORD(1,3))) F3=COORD(I,1)	0011230
75	CONTINUE	0011240
	DENS=(1./((COORD(1,2)-X1)*(COORD(1,3)-Y1)))	0011250
		0011260
		0011270
		0011280

	1 *((V1-X1)*(R-Y1)*COORD(1,1)-((V1-COORD(1,2))*(R-Y1)*F1)-((V1-X1)*	0011290
	2 *(R-COORD(1,3))*F2)+(V1-COORD(1,2))*(R-COORD(1,3))*F3)	0011300
	GO TO 40	0011310
80	IF( Q .GT. TMAXQ .OR. Q .LT. TMINQ) GO TO 95	0011320
	V1=W	0011330
C		0011340
C	TWO DIMENSIONAL INTERPOLATION	0011350
C	WN,QN	0011360
	IF( W .LT. 0.0) WBEG=WBEG-GRIDW	0011370
	IF( WBEG .LT. TMINW) WBEG=TMINW+GRIDW	0011380
	IF((WBEG+GRIDW) .GT. TMAXW) WBEG=TMAXW-GRIDW	0011390
	WBEG=IFIX(R/GRIDW)*GRIDW	0011400
83	DO 90 I1=1,JF,JS	0011410
	WN=WBEG+(I1-J1)*GRIDW	0011420
	IF( WN .LT. TMINW .OR. WN .GT. TMAXW) GO TO 85	0011430
	DO 90 I2=1,JF,JS	0011440
	L4=(RN/GRIDR)-IFIX(((Q**2.)+(WN**2.))/(NSTRT*GRIDR))	0011450
	IF( L4 .LE. 0 .OR. L4 .GT. NUMR .OR. RN .LT. 0.0) GO TO 85	0011460
	CALL CRITV(WN,QN,RN,LSTP)	0011470
	IF( TSTAT .GE. REG(LSTP,2)) GO TO 85	0011480
	CALL IENT(JLW,JLQ,JLR,WN,QN,RN)	0011490
	READ(IRLAD=JRLC) COORD(NPSF,1)	0011500
	COORD(NPSF,2)=WN	0011510
	COORD(NPSF,3)=RN	0011520
	IF(NPSF .GE. 3 .AND. NPNA .GE. 1) GO TO 60	0011530
	NPSF=NPSF+1	0011540
	GO TO 90	0011550
85	NPNA=NPNA+1	0011560
90	CONTINUE	0011570
	IF( NPSF .EQ. 4) GO TO 70	0011580
	IF( JF .GT. 1) GO TO 55	0011590
	JF=4	0011600
	J1=2	0011610
	JS=2	0011620
	GO TO 83	0011630
C		0011640
C	THREE DIMENSIONAL INTERPOLATION	0011650
C	VIA AN . POINT LATTICE FOR LAGRANGE	0011660
C	OR HYPERPLANAR INTERPOLATION	0011670
C	IF POINTS ARENT AVAILABLE	0011680
C		0011690
95	IF(W .LT. 0.0) WBEG=WBEG-GRIDW	0011700
	IF(Q .LT. 0.0) QBEG=QBEG-GRIDQ	0011710
	IF(WBEG .LT. TMINW) WBEG=TMINW	0011720
	IF(QBEG .LT. TMINQ) QBEG=TMINQ	0011730
	IF((WBEG+GRIDW) .GT. TMAXW) WBEG=TMAXW-GRIDW	0011740
	IF((QBEG+GRIDQ) .GT. TMAXQ) QBEG=TMAXQ-GRIDQ	0011750
	WBEG=IFIX(R/GRIDR)*GRIDR	0011760
100	DO 120 I1=1,JF,JS	0011770
	WN=WBEG+(I1-J1)*GRIDW	0011780
	IF( WN .LT. TMINW .OR. WN .GT. TMAXW) GO TO 110	0011790
	DO 120 I2=1,JF,JS	0011800
	QN=QBEG+(I2-J1)*GRIDQ	0011810
	IF( QN .LT. TMINQ .OR. QN .GT. TMAXQ) GO TO 110	0011820
	DO 120 I3=1,JF,JS	0011830
	RN=RBEG+(I3-J1)*GRIDR	0011840
	IF(RN .LE. 0.0) GO TO 110	0011850
	L4=(RN/GRIDR)-IFIX(((WN**2.)+(QN**2.))/(NSTRT*GRIDR))	0011860
	IF( L4 .LE. 0 .OR. L4 .GT. NUMR) GO TO 110	0011870
	NPSF=NPSF+1	0011880
	CALL IENT(JLW,JLQ,JLR,WN,QN,RN)	0011890
	READ(IRLAD=JRLC) COORD(NPSF,1)	0011900
	COORD(NPSF,2)=WN	0011910
	COORD(NPSF,3)=QN	0011920

GO TO 120

00119500

110 NPNA=NPNA+1

00119600

120 CONTINUE

00119700

IF( NPST .EQ. 8) GO TO 130

00119800

IF( JF .GT. 1) GO TO 55

00119900

JF=4

00120000

JI=2

00120100

JS=2

00120200

GO TO 150

00120300

130 DENS=0.0

00120400

DO 190 I=1.0

00120500

DO 181 J1=1.0

00120600

IF( COORD(J1,2) .NE. COORD(I,2)) GO TO 182

00120700

181 CONTINUE

00120800

182 DO 183 J2=1.0

00120900

IF( COORD(J2,3) .NE. COORD(I,3)) GO TO 184

00121000

183 CONTINUE

00121100

184 DO 185 J3=1.0

00121200

IF( COORD(J3,4) .NE. COORD(I,3)) GO TO 186

00121300

185 CONTINUE

00121400

186 DENS=DENS+(((X-COORD(I,2))\*(Y-COORD(I,3))\*(Z-COORD(I,4))))

00121500

1 / ((COORD(I,2)-COORD(J1,2))\*(COORD(I,3)-COORD(J2,3))\*(COORD(I,4)-

00121600

2 COORD(J3,3))))\*COORD(I,1)

00121700

190 CONTINUE

00121800

GO TO 40

00121900

245 CONTINUE

00122000

RETURN

00122100

END

00122200

SEGMENT

FUNCTION AREA(WHR1,CORW1,CORQ1,WHR2,CORW2,CORQ2)	00122300
COMMON /CB10/ CA,PA,CR,PR,A,B,C	00122400
Q1=CORQ1	00122500
Q2=CORQ2	00122600
W1=CORW1	00122700
W2=CORW2	00122800
AREA=0.0	00122900
IF( (WHR1 .EQ. WHR2)	00123000
1 .OR.	00123100
2 ((AMOD(WHR1,2) .EQ. 0.0) .AND. (WHR2 .EQ. (WHR1+1.)))	00123200
4 .OR.	00123300
5 ((AMOD(WHR1,2) .EQ. 1.) .AND. (WHR2 .EQ. (WHR1-1.))) ) GO TO 100	00123400
RETURN	00123500
10 IGO=IFIX(WHR2)	00123600
GO TO (20,20,30,30,30,30) ,IGO	00123700
20 XC=CR	00123800
XP=PR	00123900
GO TO 40	00124000
30 XC=CA	00124100
XP=PA	00124200
40 IF((W1*W2) .LT. 0.0) GO TO 75	00124300
EPART1=((A*(Q2-Q1)+0.5*XP*(Q2**2.-Q1**2.))/(XC+1.))	00124400
45 C1=(XP**2.)-(XC+1.)*2.)	00124500
C2=2.*(A*XP+B*(XC+1.))	00124600
C3=A**2.-(XC+1.)*(A**2.+B**2.-C)	00124700
TCURV=ABS(0.5*(Q2-Q1)*(W1+W2))	00124800
TRM1=C1*(Q2**2.)+C2*Q2+C3	00124900
IF(TRM1 .LT. 0.0 .AND. ABS(TRM1) .LT. 1.E-04) TRM1=0.0	00125000
TRM1=(2.*C1*Q2+C2)*SQRT(TRM1)	00125100
TRM2=C1*(Q1**2.)+C2*Q1+C3	00125200
IF( TRM2 .LT. 0.0 .AND. ABS(TRM2) .LT. 1.E-04) TRM2=0.0	00125300
TRM2=(2.*C1*Q1+C2)*SQRT(TRM2)	00125400
FINT1=(TRM1-TRM2)/(4.*C1)	00125500
FINT2=(4.*C1*C3-C2**2.)/(8.*C1*SQRT(-C1))	00125600
TRM3=SQRT(C2**2.-4.*C1*C3)	00125700
ARG1=(2.*C1*Q1+C2)/TRM3	00125800
IF( ABS(ARG1) .GT. 1.) ARG1=SIGN(1.,ARG1)	00125900
ARG2=(2.*C1*Q2+C2)/TRM3	00126000
IF( ABS(ARG2) .GT. 1.) ARG2=SIGN(1.,ARG2)	00126100
FINT3=ARCSIN(ARG1)-ARCSIN(ARG2)	00126200
EINTG=(FINT1+FINT2+FINT3)/7*(XC+1.)	00126300
ELCURV=ABS(EPART1+((-1.)*(WHR2-1.))*EINTG)	00126400
IF( ( W2 .GT. 0.0) .AND. (AMOD(WHR2,2) .EQ. 1.)	00126500
1 .OR.	00126600
2 ( (W2 .LT. 0.0) .AND. (AMOD(WHR2,2) .EQ. 0.0) ) ) GO TO 60	00126700
IF( W2 .NE. 0.0) GO TO 50	00126800
IF( ( (W1 .GT. 0.0) .AND. (AMOD(WHR1,2) .EQ. 1.))	00126900
1 .OR.	00127000
2 ( (W1 .LT. 0.0) .AND. (AMOD(WHR1,2) .EQ. 0.0)) ) GO TO 60	00127100
50 AREA=TCURV-ELCURV	00127200
55 AREA=AMAX1(0.0,AREA)	00127300
RETURN	00127400
60 AREA=ELCURV-TCURV	00127500
GO TO 55	00127600
75 IF( CORW2 .LT. 0.0) GO TO 76	00127700
G=0.5+CORW2	00127800
W2=-0.5	00127900
W1=CORW1-G	00128000
GO TO 77	00128100
76 G=0.5+CORW1	00128200
W1=-0.5	00128300
W2=CORW2-G	00128400

30 CONTINUE

00128700

RETURN

00128800

END

00128900

SEGMENT

FUNCTION WEIGHT( NPA,NAN)  
 COMMON /CBB/ GREGC(14,14)  
 IF( NPA .GE. 15) GO TO 10  
 WEIGHT=GREGC(NPA,NAN)

START OF SEGMENT

00140100

00140200

00140300

00140400

RETURN

00140500

10 IF( NAN .GT. 7) GO TO 20

00140600

WEIGHT=GREGC(14,NAN)

00140700

RETURN

00140800

20 IF( NAN .LE. (NPA-7)) GO TO 30

00140900

INDX=14-NPA+NAN

00141000

WEIGHT=GREGC(14,INDX)

00141100

RETURN

00141200

30 WEIGHT=1.

00141300

RETURN

00141400

END

00141500

SEGMENT

FUNCTION TERP05(UCOR,ZCOR)	00129000
COMMON /CB7/ LSTP,ISUR	00129100
COMMON /CB1/ GRIDW,GRIDQ,GRIDR	00129200
COMMON /CB12/ NUMW,NUMQ,NUMR	00129300
COMMON /CB6/ TMAXW,TMINW,TMAXQ,TMINQ	00129400
COMMON /CB2/ JREC,TSTAT	00129500
COMMON /CB13/ QBEG,WBEG	00129600
COMMON /CB14/ XMEAN(2),XBR1,XBR2,VAR,DGI	00129700
COMMON /CB10/ EXCES1,EXCES2,EXCES3,EXCES4,A,B,C	00129800
COMMON /CB3/ NCONW,NCONQ,NSTRT	00129900
COMMON /CB8/ JOINT	00130000
COMMON /CB20/ RECMAX	
DIMENSION XVAL(10),YVAL(10)	00130100
TERP05=0.0	00130200
INZER=0	00130300
IDID=0	00130400
TERP05=0.0	00130500
W=A-ZCOR	00130600
Q=B-UCOR	00130700
R=C-(UCOR**2.+ZCOR**2.)	00130800
VCH=POSPROB(W,Q,R,LSTP)	00130900
IF( VCH .LT. 0.0) RETURN	00131000
IF( LSTP .GT. ISUR) GO TO 5	00131100
TERP05=CHISQ(VCH,DGI)*PHI(W,XBR1,VAR)*PHI(Q,XBR2,VAR)*	00131200
1 PHI(UCOR,XMEAN(2),1.)*PHI(ZCOR,XMEAN(1),1.)	00131300
RETURN	00131400
5 LB1=(W/GRIDW)+IFIX(NUMW/2.)*1-IFIX((ISUR*XMEAN(1))/GRIDW)	00131500
WBEG=(LB1-1-IFIX(NUMW/2.)*1-IFIX((ISUR*XMEAN(1))/GRIDW))*GRIDW	00131600
LB2=(Q/GRIDQ)+IFIX(NUMQ/2.)*1-IFIX((ISUR*XMEAN(2))/GRIDQ)	00131700
QBEG=(LB2-1-IFIX(NUMQ/2.)*1-IFIX((ISUR*XMEAN(2))/GRIDQ))*GRIDQ	00131800
IF(( W .GT. TMAXW .OR. W .LT. TMINW) .AND.	00131900
1 ( Q .GT. TMAXQ .OR. Q .LT. TMINQ)) GO TO 55	00132000
IF( WBEG .EQ. W .AND. QBEG .EQ. Q) GO TO 15	00132100
IF( WBEG .EQ. W) GO TO 30	00132200
IF( QBEG .EQ. Q) GO TO 40	00132300
GO TO 50	00132400
15 IF( W .GT. TMAXW .OR. W .LT. TMINW) GO TO 40	00132500
IF( Q .GT. TMAXQ .OR. Q .LT. TMINQ) GO TO 30	00132600
WN=W	00132700
QN=Q	00132800
20 L4=(R/GRIDR)-IFIX((W**2.+Q**2.)/(NSTRT*GRIDR))	00132900
IF( L4 .LE. 0 .OR. L4 .GT. NUMR) GO TO 25	00133000
CALL RCAL(LB1,LB2,L4,0,WN,QN,RN)	00133100
IF( RN .NE. R) GO TO 25	00133200
IF( JREC .LE. 0.0 .OR. JREC .GT. RECMAX) GO TO 25	00133250
READ(JOINT=JREC) PROB3	00133300
TERP05=PROB3*PHI(UCOR,XMEAN(2),1.)*PHI(ZCOR,XMEAN(1),1.)	00133400
RETURN	00133500
25 TERP05=TERP01(W,Q,R,JOINT)	00133600
1 *PHI(UCOR,XMEAN(2),1.)*PHI(ZCOR,XMEAN(1),1.)	00133700
RETURN	00133800
30 LB=LB2	00133900
IF((LB-1) .LE. 0) LB=2	00134000
IF((LB+1) .GT. NUMQ) LB=NUMQ-1	00134100
L9=LB-1	00134200
L10=LB+1	00134300
OPFI=0	00134600
ZPT=A-W	00134700
DO 35 L11=L9,L10	00134800
QH=(L11-1-IFIX(NUMQ/2.)*1-IFIX((ISUR*XMEAN(2))/GRIDQ))*GRIDQ	00134900
UPT=H-QH	00135000
IDID=IDID+1	00135100
	00135200

C-31

IF( YVAL(IDID) .GT. 0.0) INZER=INZER+1

00135400

35 CONTINUE

00135500

CALL BESTINTERP(XVAL,YVAL,IDID,INZER,QPFI,TERP05)

00135600

IF( TERP05 .LT. 0.0) TERP05=0.0

00135700

RETURN

00135800

40 M8=LH1

00135900

IF((M8-1) .LE. 0) M8=2

00136000

IF((M8+1) .GT. NUMW) M8=NUMW-1

00136100

M9=M8-1

00136200

M10=M8+1

00136300

WPF1=W

00136400

QH=Q

00136500

UPT=H-QH

00136600

DO 45 M11=M9,M10

00136700

WH=(M11-1-IFIX(NUMW/2.))+IFIX((ISUR\*XMEAN(1))/GRIDW))\*GRIDW

00136800

ZPT=A-WH

00136900

IDID=IDID+1

00137000

XVAL(IDID)=WH

00137100

YVAL(IDID)=1LKPU5(UPT,ZPT)

00137200

IF( YVAL(IDID) .GT. 0.0) INZER=INZER+1

00137300

45 CONTINUE

00137400

CALL BESTINTERP(XVAL,YVAL,IDID,INZER,WPF1,TERP05)

00137500

IF( TERP05 .LT. 0.0) TERP05=0.0

00137600

RETURN

00137700

50 OPT1=QREG

00137800

WPT1=WREG

00137900

OPT2=OPT1+GRIDQ

00138000

WPT2=WPT1+GRIDW

00138100

QI=Q

00138200

WI=W

00138300

CALL OVERFL(IND)

00138400

TLAGR1=(QI-QPT2)\*(WI-WPT2)\*TERP05(B-QPT1,A-WPT1)

00138500

TLAGR2=(QI-QPT2)\*(WI-WPT1)\*TERP05(H-QPT1,A-WPT2)

00138600

TLAGR3=(QI-QPT1)\*(WI-WPT2)\*TERP05(B-QPT2,A-WPT1)

00138700

TLAGR4=(QI-QPT1)\*(WI-WPT1)\*TERP05(B-QPT2,A-WPT2)

00138800

DVAL=TLAGR1+TLAGR2+TLAGR3+TLAGR4

00138900

IF( DVAL .LT. 0.0 .OR. IND .EQ. 3) GO TO 51

00139000

TERP05=DVAL/(GRIDQ\*GRIDW)

00139100

51 RETURN

00139200

55 TERP05=TERP01(W,Q,R,JOINT)

00139300

1 \*PHI(UCOR,XMEAN(2),1.)\*PHI(ZCOR,XMEAN(1),1.)

00139400

RETURN

00139500

END

00140000

SEGMENT

	BLOCK DATA	START OF SEGMENT
	COMMON /C88/GREGC(14,14)	00141600
C		00141700
C	THESE ARE THE WEIGHTS FOR THE NEWTON-GREGORY INTEGRATION FORMUL	00141800
C		00141900
	DATA GREGC(1,1)/0.0/	00142000
	DATA (GREGC(3,1),I=1,3)/.4166667,1.1166666,.4166667/	00142100
	DATA(GREGC(4,1),I=1,4)/.375,1.125,1.125,.375/	00142200
	DATA(GREGC(5,1),I=1,5)/.348611,1.2722222,.7583333,1.272222,	00142300
	1 .348611/	00142400
	DATA(GREGC(6,1),I=1,6)/.3298611,1.3020833,.8680555,.8680555,	00142500
	1 1.3020833,.3298611/	00142600
	DATA(GREGC(7,1),I=1,7)/.3298611,1.3020833,.7479167,1.2027777	00142700
	1,.7479167,1.3020833,.3298611/	00142800
	DATA(GREGC(8,1),I=1,8)/.3155919,1.3921792,.6382440,1.1539848,	00142900
	11.1539848,.6382440,1.3921792,.3155919/	00143000
	DATA(GREGC(9,1),I=1,9)/.3155919,1.3921792,.6239749,1.2583499,	00143100
	1.8198082,1.2583499,.6239749,1.3921792,.3155919/	00143200
	DATA(GREGC(10,1),I=1,10)/.3155919,1.3921792,.6239749,1.2440807,	00143300
	1.9241733,.9241733,1.2440807,.6239749,1.3921792,.3155919/	00143400
	DATA(GREGC(11,1),I=1,11)/.3155919,1.3921792,.6239749,1.2440807,	00143500
	1.9099041,1.0285384,.9099041,1.2440807,.6239749,1.3921792,.3155919/	00143600
	DATA(GREGC(12,1),I=1,12)/.3155919,1.3921792,.6239749,1.2440807,	00143700
	1.9099041,1.0142692,1.0142692,.9099041,1.2440807,.6239749,1.3921792,	00143800
	2,.3155919 /	00143900
	DATA(GREGC(13,1),I=1,13)/.3042245,1.4603836,.4534640,1.4714286,	00144000
	1.7393932,1.0824735,.9772652,1.0824735,.7393932,1.4714286,.4534640,	00144100
	21.4603836,.3042245/	00144200
	DATA(GREGC(14,1),I=1,14)/.3042245,1.4603836,.4534640,1.4714286,	00144300
	1.7393932,1.0824735,.9886326,.9886326,1.0824735,.7393932,1.4714286,	00144400
	3.4534640,1.4603836,.3042245/	00144500
	END	00144600
		SEGMENT

C-35

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SUBROUTINE BESTINTERP(X,Y,IDON,INOTZ,XINT,YINT)
DIMENSION X(10),Y(10),EXT(10),WH(10)
YINT=0.0

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      THIS SUBROUTINE DECIDES WHICH TYPE
      OF INTERPOLATION IS MOST APPROPRIATE FOR A PARTICULAR POINT
      SINCE THE DENSITY FUNCTION MAY BE TRUNCATED
      LAGRAGIAN INTERPOLATION MAY NOT ALWAYS BE THE BEST

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      IF( INOTZ .LE. 0) RETURN
      IF( INOTZ .NE. IDON) GO TO 7
      IF(XINT.LT. X(1).AND. XINT.LT. X(IDON).AND. Y(1) .LE. 0) RETURN
      IF(XINT.GT. X(1).AND. XINT.GT. X(IDON).AND. Y(IDON).LE.0.0)RETURN
      IF(XINT .LT. X(1).AND. XINT.LT. X(IDON)) GO TO 3
      IF(XINT .GT. X(1) .AND. XINT .GT. X(IDON)) GO TO 3
      DO 2 IRUN=2,IDON
      IF((XINT.GT. X(IRUN-1).AND. XINT .LT. X(IRUN)) .OR.
1(XINT.LT. X(IRUN-1) .AND. XINT .GT. X(IRUN))) INDEX=IRUN-1
      Y(IRUN)=ALOG(Y(IRUN))
2      CONTINUE
      Y(1)=ALOG(Y(1))
      YINT=SPLINEF11(X,Y,IDON,INDEX,XINT)
      IF( YINT .LT. -30.) RETURN
      YINT=EXP(YINT)
      RETURN
3      DINT=POLY(X,Y,XINT,IDON)
      IF( DINT .LE. 0.0) RETURN
      YINT=DINT
      RETURN
7      DO 8 IRUN=2,IDON
      IF((XINT .GT. X(IRUN-1) .AND. XINT .LT. X(IRUN)) .OR.
1(XINT .LT. X(IRUN-1) .AND. XINT .GT. X(IRUN))) GO TO 9
      GO TO 8
9      IF(Y(IRUN-1) .LE. 0.0 .AND. Y(IRUN) .LE. 0.0) RETURN
      INDEX=IRUN
      JCT=0
      IF(Y(IRUN-1) .LE. 0.0 .OR. Y(IRUN) .LE. 0.0) GO TO 25
      GO TO 10
8      CONTINUE
      RETURN
10     DO 15 JK=1,IDON
      IF(Y(JK) .LE. 0.0) GO TO 15
      JCT=JCT+1
      WH(JCT)=X(JK)
      EXT(JCT)=ALOG(Y(JK))
      IF(JK .EQ. INDEX) IDX=JK
15     CONTINUE
      IF(JCT .GE. 3) GO TO 20
      DINT=POLY(WH*EXT,XINT,JCT)
      IF( DINT .LE. -35.0) RETURN
      IF( DINT .GT. 0.0) GO TO 3
      YINT=EXP(DINT)
      RETURN
20     DINT=SPLINEF11(WH*EXT,JCT,IDX,XINT)
      IF(DINT .LE. -35.) RETURN
      IF( DINT .GT. 0.0) GO TO 3
      YINT=EXP(DINT)
      RETURN
25     IF(Y(IRUN-1) .GT. 0.0)FAC=ABS(IFIX(ALOG10(Y(IRUN-1))))
      IF(Y(IRUN) .GT. 0.0) FAC=ABS(IFIX(ALOG10(Y(IRUN))))
      DO 50 JK=1,IDON
      IF( Y(JK) .GT. 0.0) GO TO 30

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IF( JK .NE. INDEX .OR. JK .NE. (INDEX-1)) GO TO 50
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00151000

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30 JCT=JCT+1
   WH(JCT)=X(JK)
   EXT(JCT)=ALOG(1.+(10.**FAC)*Y(JK))
   IF(JK .EQ. INDEX) IDX=JK
50 CONTINUE
   IF( JCT .GE. 3) GO TO 60
   DINT=POLY(WH,EXT,XINT,JCT)
   GO TO 61
60 DINT=SPLINEFIT(WH,EXT,JCT,IDX,XINT)
61 IF(DINT .LT. 0.0) RETURN
   YINT=(EXP(DINT)-1.)/(10.**FAC)
   RETURN
END
```

00151100

00151200

00151300

00151400

00151500

00151600

00151700

00151800

00151900

00152000

00152100

00152200

00152300

SEGMENT

```
FUNCTION POLY(X,Y,XINT,INUM)
DIMENSION X(10),Y(10)
```

00156900

00157000

00157100

```
C
C THIS ROUTINE PERFORMS INTERPOLATION VIA
C GENERALIZED ONE DIMENSIONAL LAGRANGE
```

00157200

00157300

00157400

00157500

DSUM=0.0

DO 5 IK=1,INUM

00157600

TTERM=1.

00157700

BTERM=1.

00157800

DO 4 JK=1,INUM

00157900

IF( JK .EQ. IK) GO TO 4

00158000

TTERM=(XINT-X(JK))\*TTERM

00158100

BTERM=(X(1K)-X(JK))\*BTERM

00158200

4 CONTINUE

00158300

DSUM=DSUM+(TTERM/BTERM)\*Y(1K)

00158400

5 CONTINUE

00158500

POLY=DSUM

00158600

RETURN

00158700

END

00158800

SEGMENT

```
FUNCTION ECHECK(INUM,VAL)
COMMON/ERR/ IRP1,IRP2
GO TO (10,20
```

START OF SEGMENT

00158900

00159000

),INUM

00159100

00159200

C THIS IS A CHECK ON ZRANGE - ELLIPSE

10 IF(VAL .LT. 0.0 .AND. ABS(VAL) .GT. 1.E+06) IRP1=IRP1+1

00159300

VAL=AMAX1(0.0,VAL)

00159400

RETURN

00159500

C THIS IS A CHECK ON ZRANGE - CIRCLE

00159600

20 IF( VAL .LE. 0.0 .AND. ABS(VAL) .GT. 1.E+06) IRP2=IRP2+1

00159700

RETURN

00159800

END

00159900

SEGMENT

		START OF SEGMENT
	FUNCTION SPLINEFIT(X,Y,H,J,XINT)	00152400
	DIMENSION X(10),Y(10),D(10),P(10),E(10),C(4,10)	00152500
	DIMENSION A(10,3),B(10),Z(10)	00152600
C		00152700
C	SPLINEFIT PERFORMS INTERPOLATION BY FITTING	00152800
C	A CUBIC SPLINE FUNCTION TO THE POINTS	00152900
C		00153000
	MM=M-1	00153100
	DO 2 K=1,MM	00153200
	D(K)=X(K+1)-X(K)	00153300
	P(K)=D(K)/6.	00153400
2	E(K)=(Y(K+1)-Y(K))/D(K)	00153500
	DO 3 K=2,MM	00153600
3	B(K)=E(K)-E(K-1)	00153700
	A(1,2)=-1.-D(1)/D(2)	00153800
	A(1,3)=D(1)/D(2)	00153900
	A(2,3)=P(2)-P(1)*A(1,3)	00154000
	A(2,2)=2.*(P(1)+P(2))-P(1)*A(1,2)	00154100
	A(2,3)=A(2,3)/A(2,2)	00154200
	B(2)=H(2)/A(2,2)	00154300
	IF( M .EQ. 3) GO TO 5	00154400
	DO 4 K=3,MM	00154500
	A(K,2)=2.*(P(K-1)+P(K))-P(K-1)*A(K-1,3)	00154600
	B(K)=B(K)-P(K-1)*B(K-1)	00154700
	A(K,3)=P(K)/A(K,2)	00154800
4	B(K)=B(K)/A(K,2)	00154900
5	Q=D(M-2)/D(M-1)	00155000
	A(M,1)=1.+Q+A(M-2,3)	00155100
	A(M,2)=-J-A(M,1)*B(M-1)	00155200
	Z(M)=B(M)/A(M,2)	00155300
	MN=M-2	00155400
	DO 6 I=1,MN	00155500
	K=M-I	00155600
6	Z(K)=B(K)-A(K,3)*Z(K+1)	00155700
	Z(I)=-A(1,2)*Z(2)-A(1,3)*Z(3)	00155800
	DO 7 K=1,MM	00155900
	Q=1./(6.*D(K))	00155950
	C(1,K)=Z(K)*Q	00156000
	C(2,K)=Z(K+1)*Q	00156100
	C(3,K)=Y(K)/D(K)-Z(K+1)*P(K)	00156200
7	C(4,K)=Y(K+1)/D(K)-Z(K+1)*P(K)	00156300
	TINT=(X(J+1)-XINT)*(C(1,J)*(X(K+1)-XINT)**2.+C(3,J))	00156400
	TINT=TINT+ (XINT-X(J))*(C(2,J)*(XINT-X(J))**2.+C(4,J))	00156500
	SPLINEFIT=TINT	00156600
	RETURN	00156700
	END	00156800
		SEGMENT

SUBROUTINE RESUME(X1,X2,X3,\*)

C  
C  
C THIS SUBROUTINE ALLOWS THE PROGRAM TO BE  
C RUN FOR A PERIOD OF TIME AND TERMINATED  
C BY THE COMPUTER OPERATOR. THIS SUB INITIALIZES  
C ALL THE IMPORTANT VARIABLES BACK TO WHAT THEY WERE WHEN THE  
C PROGRAM WAS RUNNING

C  
C  
COMMON/CB7/ LSTP,ISUR  
COMMON /CB10/ CA,PA,CR,PR,A,B,C  
COMMON /CB8/ JOINT,ICAL  
COMMON/KESTAR/OC(30,2),ASN(30),NTESTS  
COMMON /KESTAR/ KTEST,NOC,NSTP,11,12,13,KREC,IRAC,NPF IAC,IRNR  
COMMON /KESTAR/ NPI INR,PROBAC,PROBNR,PRRAC,PRQAC,PRRNR,PRQNR  
COMMON /KESTAR/ RVALAC,RVALNR,RACBEG,SPRUAC,RNBEG,SPRUNR  
COMMON /KESTAR/ WN,QN,RN  
DAY=" / /"  
YEAR=" "  
DYM=TIME(5)  
DOFWK=TIME(6)  
TUD=TIME(1)/216000.0  
DAY=CONCAT(DAY,DYM,12,12,12)  
DAY=CONCAT(DAY,DYM,30,24,12)  
YEAR=CONCAT(YEAR,DYM,12,36,12)  
READ(10=1) NTRY5,KTEST,NOC,NSTP,JOINT,ICAL,11,12,13,KREC,IRAC,  
1 NPI IAC,IRNR,NPF INR,A,B,C,PROBAC,PROBNR,PRRAC,PRQAC,PRRNR,PRQNR,  
2 RVALAC,RVALNR,RACBEG,SPRUAC,RNBEG,SPRUNR,X1,X2,X3  
MTRY5=NTRY5+1  
WRITE(8,100) MTRY5,DOFWK,DAY,YEAR,TUD  
100 FORMAT(1H1,20X,"RESUMING PROCESSING",20X,"TRY",15,/,10X,A6,10X,  
1 2A6,25X,"AT",E15.7," HOURS")  
WRITE(8,101)  
101 FORMAT( 40X,"SUMMARY FROM LAST RUN")  
WRITE(8,\*/ ) NTRY5,KTEST,NOC,NSTP,JOINT,ICAL,11,12,13,KREC,IRAC,  
1 NPF IAC,IRNR,NPF INR,A,B,C,PROBAC,PROBNR,PRRAC,PRQAC,PRRNR,PRQNR,  
2 RVALAC,RVALNR,RACBEG,SPRUAC,RNBEG,SPRUNR,X1,X2,X3  
WRITE(8,102)  
102 FORMAT(///,40X,"SUMMARY FROM ALL PREVIOUS RUNS")  
DO 10 J1=1,KTEST  
DO 10 J2=1,NOC,9  
DO 10 J3=1,NSTP-1  
READ(11=(J3+((J2-1)\*NTESTS)+(J1-1)\*NTESTS\*10)) PACC,PREJ,PCUN,  
1 NSTEP,ALAM,NCASE  
WRITE(8,\*/ ) NCASE,ALAM,NSTEP,PACC,PREJ,PCUN  
IF( NSTP .LE. (ISUR+1)) GO TO 10  
IF( J1 .LT. KTEST .OR. J2 .LT. NOC .OR. J3 .LE. ISUR) GO TO 10  
OC(J3,1)=PACC  
OC(J3,2)=PREJ  
ASN(J3)=PCUN  
10 CONTINUE  
WN=A  
QN=B  
RN=C  
RETURN 1  
END

SEGMENT

Unclassified

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20. (continued)

The numerical approach is discussed, ~~in section (2.6).~~  
Appendix A gives the power calculation for a fixed sample  
ANOVA test; Appendix B shows how the Wald regions are found;  
Appendix C contains a computer program for the OC and ASN.

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